ILLINOIS STATE TOLL HIGHWAY AUTHORITY

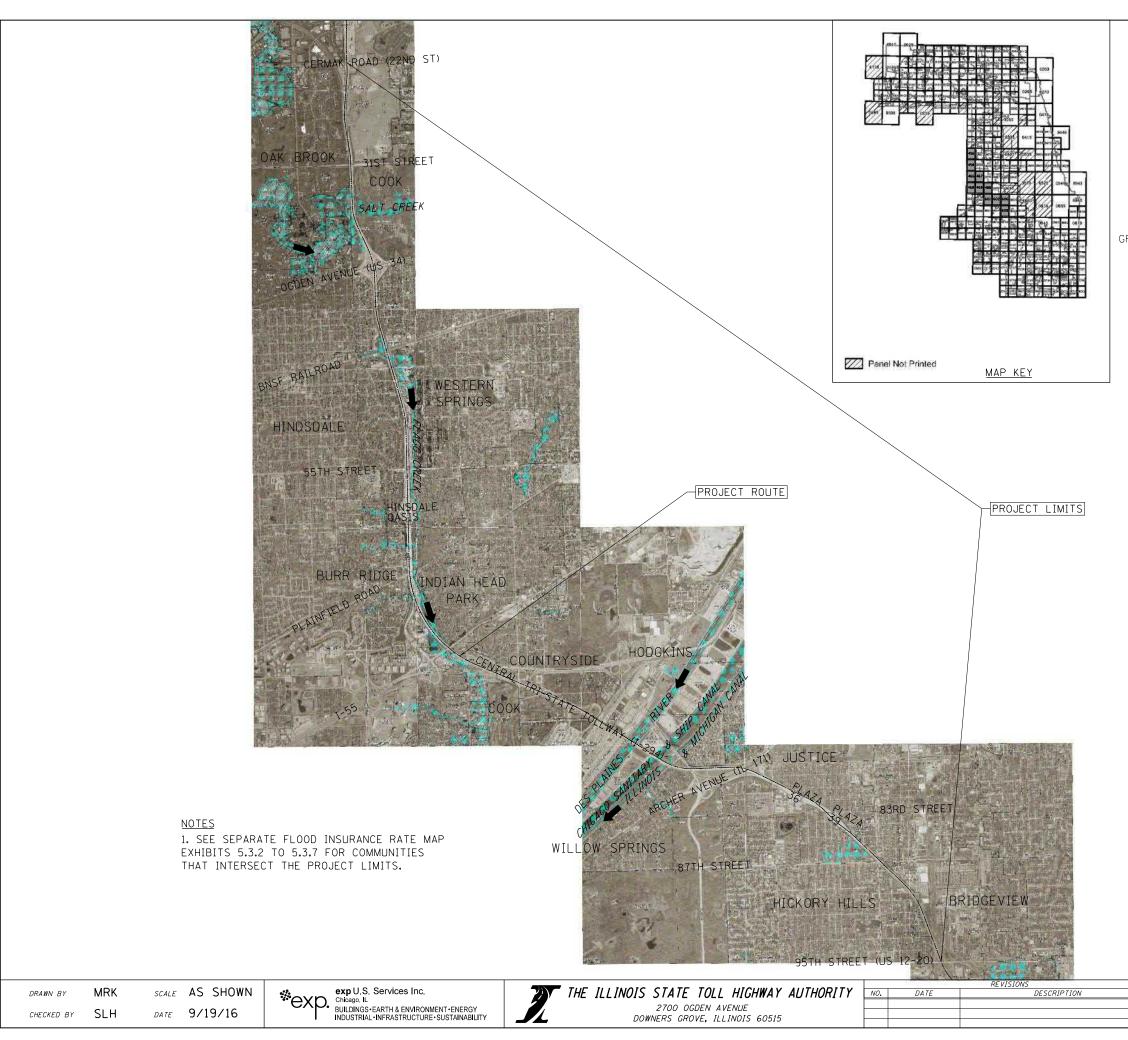


VOLUME 1 PART 2 CONCEPT DRAINAGE REPORT FOR CENTRAL TRI-STATE TOLLWAY (I-294) ROADWAY STUDY

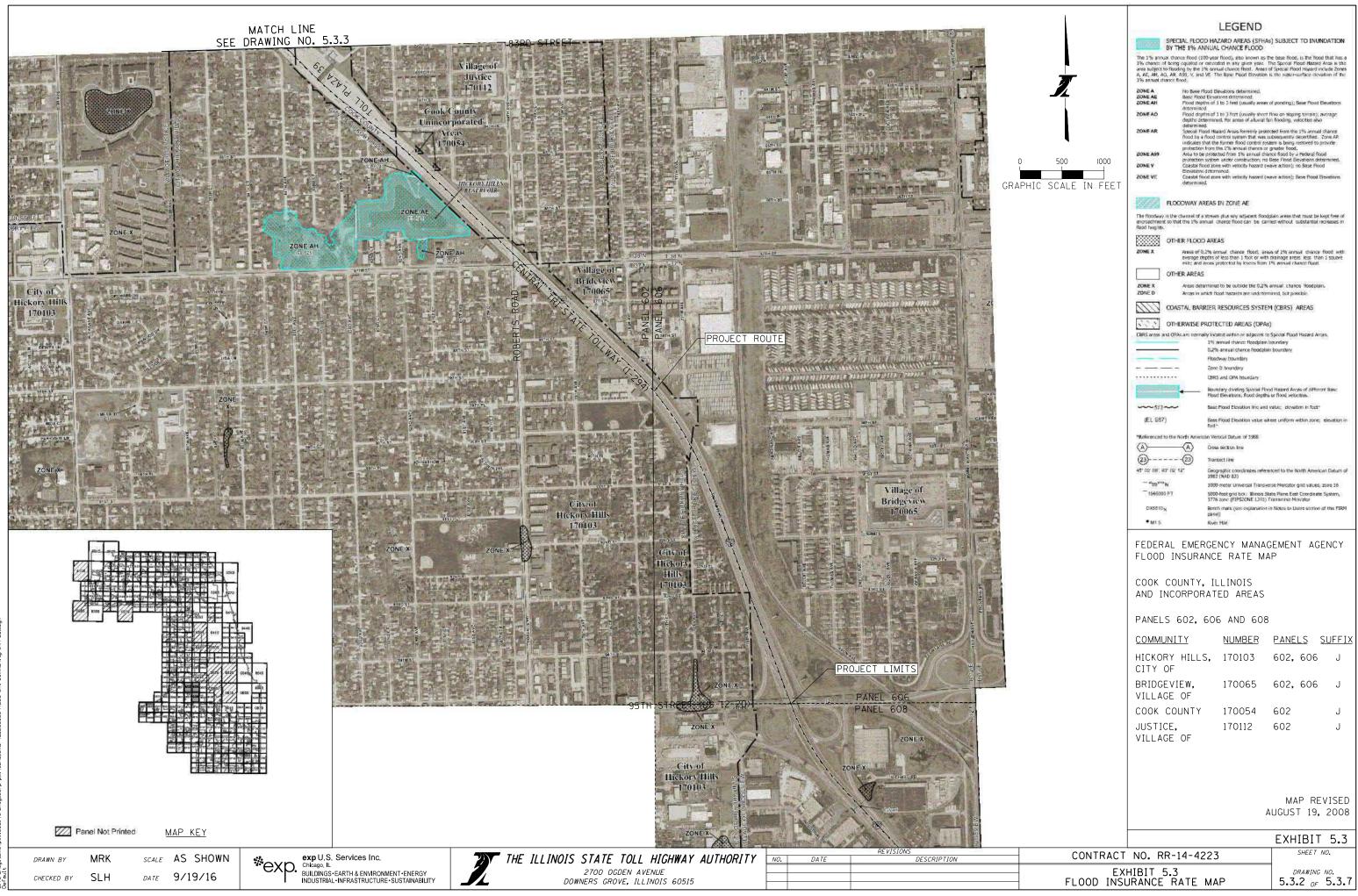
95TH STREET (M.P. 17.5) TO CERMAK ROAD (M.P. 29.5) CONTRACT RR-14-4223

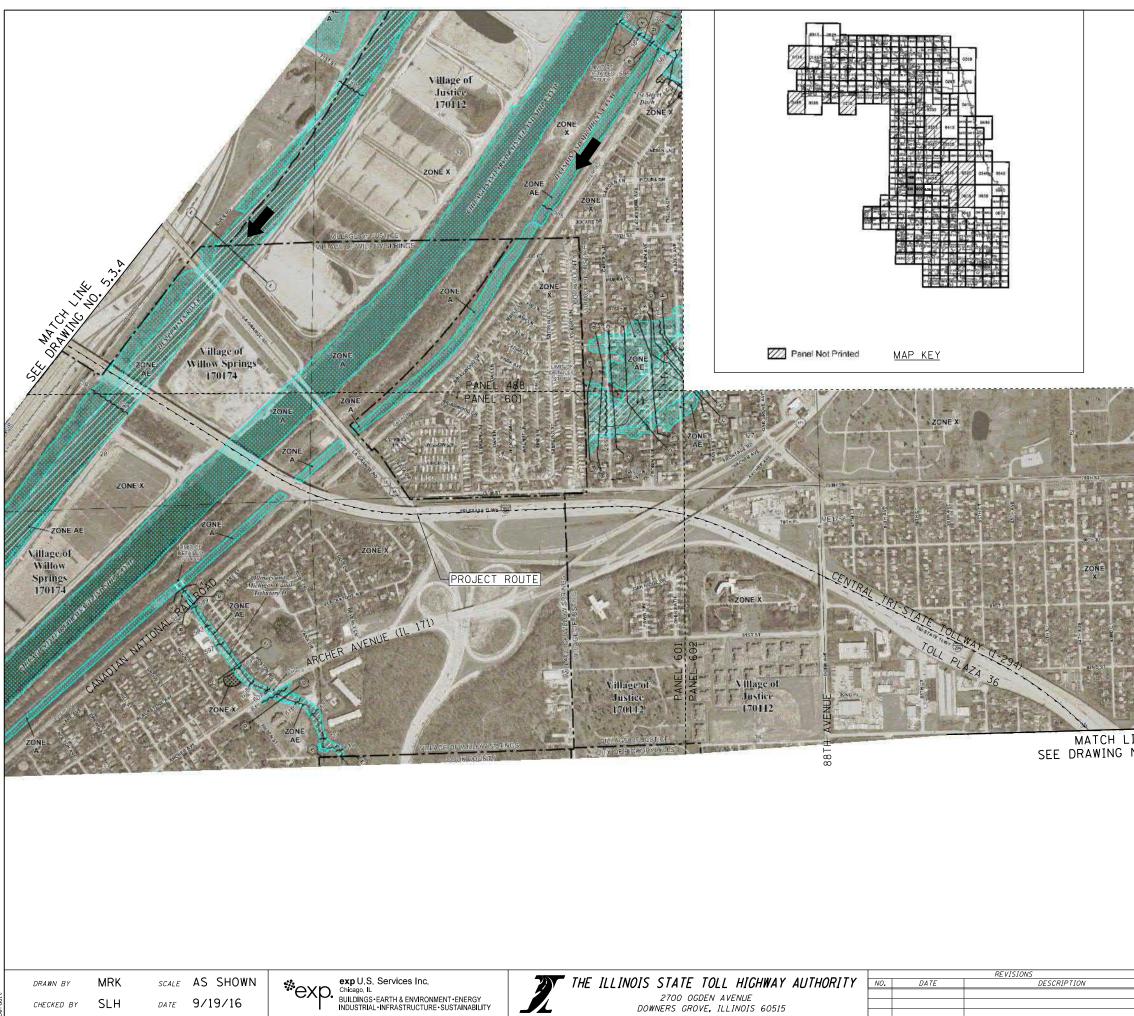
PREPARED BY: Exp / TranSystems / SE3 TEAM DATE: DECEMBER 22, 2017

5.3 IDENTIFIED BASE FLOODPLAIN MAPS



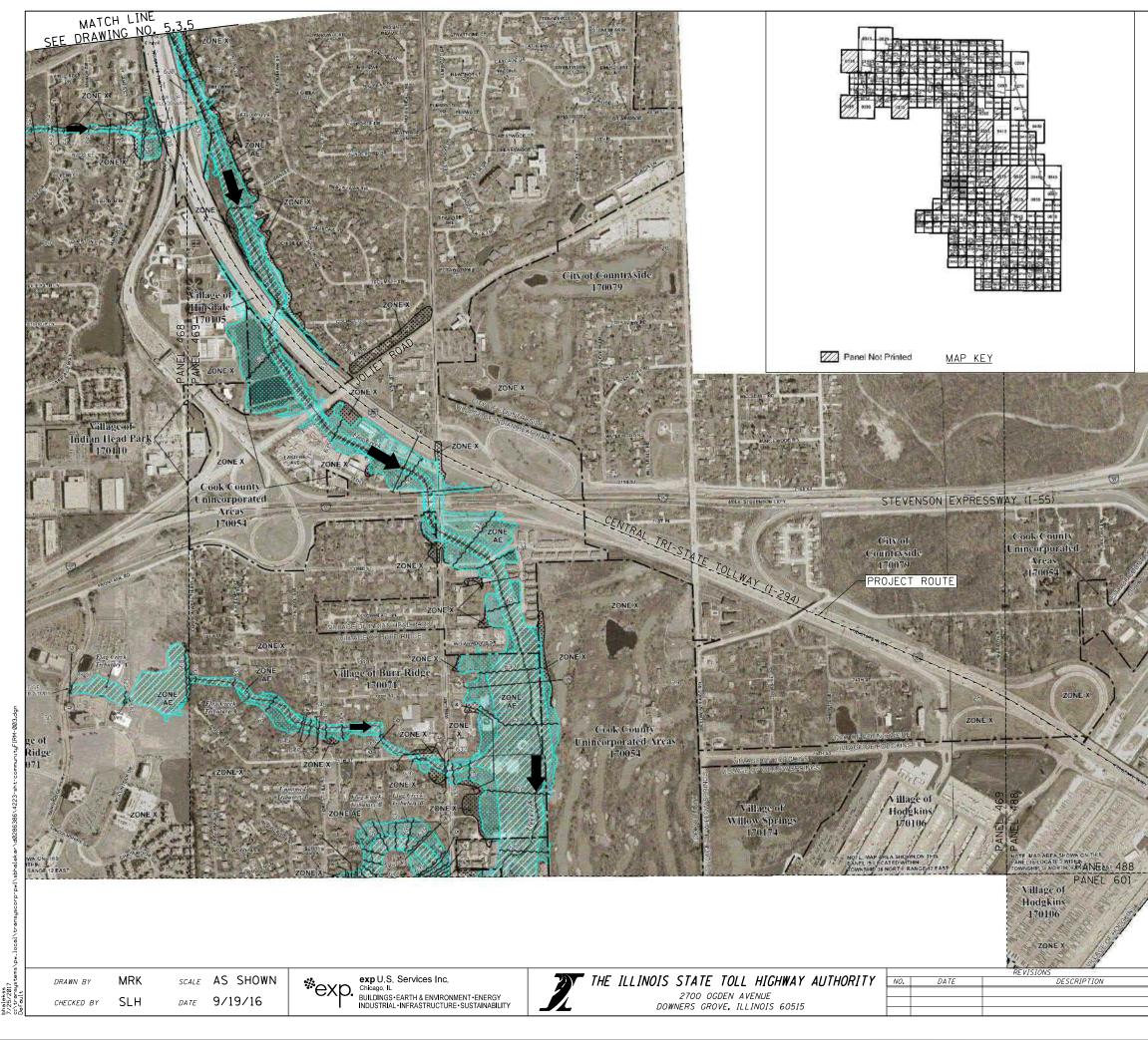
1	LEGEND					
		DD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION			
	The 1% annual chance flood (1 1% chance of being equaled o area subject to flooding by the	00-year flood), also known as th r exceeded in any given year. T 1% annual chance flood. Areas o	e base flood, is the flood that has a he Special Flood Hazard Arias is the f Special Flood Hazard include Zones 5 the water-surface elevation of the			
T	ZONE A No Base I ZONE AE Base Floo	Flood Bevations determined. In Elevations dotermined.				
	determin		of ponding); Sear Flood Bevetions			
	depths de determin ZONE AR Special FI	etermined, For areas of alluvial fa ed. lood Hazard Areas formerly protec	n flooding, velocities also ted from the 1% annual chance			
	indicates protection	a nood control system that was so that the former flood control syst in from the 1% annual chance or e protected from 1% annual chan	greater flood.			
	ZONE V Coastal fi	n system atten construction; no l opd zone with velocity hazard (wi	lase Flood Bevations determined.			
0 2500 5000		s determined. locd zone with velocity hazard (wi ed.	we action); Base Flood Elevations			
RAPHIC SCALE IN FEET	FLOODWAY A	REAS IN ZONE AE				
	The floodway is the channel of a encroadment so that the 1% a flood heights.	a stream plus ony adjacent floodp nnual chance flood can be carr	lain areas that must be kept free of en without substantial increases in			
	OTHER FLOOD	D AREAS				
	everage t	3.2% annual chance floot, area leptits of less than 1 foot or with areas protected by levers from 1	s of 1% annual chance flood with trainage areas less then 1 spuare % annual chance floor			
	OTHER AREA		TE ANTIGE CHARGE FIGURE			
		anninad to be outside the 0.2% which flood hazards are undeform				
	COASTAL BAR	RIER RESOURCES SYSTEM	(CBRS) AREAS			
	Contraction of the Contraction o	PROTECTED AREAS (OPAs)				
	CBRS areas and OPAs are norm	ally induted within or adjacent to 1% annual chance floodplain is	oundary			
		0.2% annual chance flood plair Floodway boundary	boundary			
	t: <u></u>	Zone D boundary CBRS and OPA boundary				
	-	Boundary dividing Special Pleo Flood Elevations, flood depths	d Hazard Arcas of different Base or flood velocities.			
		Base Flood Elevation line and	24 CHEED 10 20 C 20 A 20 HT FL 10 CHE 14 III			
	(EL 987)	Base Flood Elevation value with foot**	ere uniform within zone; elevation in			
	*Referenced to the North Ameri					
	(2)(2)	Gross section line Transect line				
	45" 02' 08', 83" 02' 12'	Geographic coordinates referen 1983 (NAD 83)	xed to the North American Datum of			
	- *55****N - 1565000 FT		se Mercator grid values, zone 16 ite Plane East Coordinate System.			
	DX5610 _X	3776 zone (FIPSZONE L201) T Benich mark (see explanation i				
	* M1 5	panel) River Mile				
	FEDERAL EMER FLOOD INSURA		EMENT AGENCY P			
	COOK AND DUI AND INCORPOF	PAGE COUNTIE RATED AREAS	S; ILLINOIS			
	PANELS					
		AGE COUNTY F	RELIMINARY)			
	456, 458, 466					
	468, 469, 488 602, 606, 60	,,	K COUNTY , AUG 19, 2008			
	<u>COMMUNITIES</u>					
		S, BRIDGEVIEW				
		, WILLOW SPR Indian head	INGS, HODGKINS, Park.			
		URR RIDGE, WE	ESTERN SPRINGS,			
	OAK BROOK					
			MAP REVISED			
		AUGUST	19, 2008 (COOK) TBD (DUPAGE)			
			EXHIBIT 5.3			
CONTRACT	NO. RR-14-42	223	SHEET NO.			
	HIBIT 5.3		DRAWING NO.			
	JRANCE RATE	MAP	5.3.1 _{OF} 5.3.7			

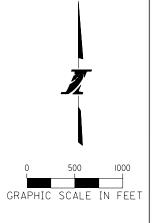


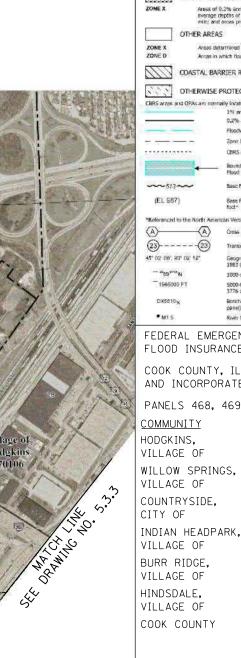


	II II II
	SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD The 1% annual chance flood (100-year flood), also income as the base flood, is the flood that has a
The second se	The shared state from (core-per nool), also when as the case in the shared state and a set of the shared state in the shared s
Ĵ,	ZONE A No Bere Flood Bevations determined, ZONE AE Basic Flood Elevations distermined, ZONE AH Flood Highfrix of 1 to 1 fert (usually averas of ponding); Base Flood Bevations
	ZONE An Those heppins of a to a tree (losuary areas or ponding); sever most detendeds detended. ZONE AO Phod doptins of a to 3 free (usually shoet flow on staping terrain); average deptins determined. The areas of alumina fan flooding, velocities also
	20NE AR detainined. Special Flood Hazard Arass formerly protocoled from the 1% annual chance flood by a flood control system that was subsequently decertified. Zone AR
•	indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. Area to be protected from 1% annual chance flood by a Federal flood
0 500 1000	20NE V Coastal flood zone with velocity hazard (wave action) no Base Flood Bevations determined. Elevations determined. Elevations determined.
GRAPHIC SCALE IN FEET	ZONE VE Coastal fixed zone with velocity hazard (wave action); Base Rood Elevations detarmined.
	FLOODWAY AREAS IN ZONE AE
	The flootkway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroadment so that the 1% annual chance flood can be carried without substantial increases in flood heights.
	OTHER FLOOD AREAS
	ZONE X Aross of 0.2% annual chance floot, areas of 1% annual chance flood with sverage depths of less than 1 foot or with riskinge areas, less than 1 square mility and areas protocold by leaves from 1% annual chance flood
	OTHER AREAS
	ZONE X Areas determined to be outside the 0.2% annual chance floodplan. ZONE 0 Areas in which flood heards are undetermined, but possible.
	COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS
	CIRES areas and OPAc are normally included within or adjacent. to Special Flood Heard Areas.
	1% annual chance fleodplain boundary 0,2% annual chance fleodplain boundary
Village of	Floodway foundary Zone D boundary
Justice 170112	CBRS and OPA Isoundary Boundary dividing Special Plood Hazard Arces of different Base
T(WITZ A CLAREN MARK	Hourtbary owning space in theor mapping should be the stress of anisotro bases Hourt Bevefores, fixed depths or flood the velocities. Salars Flood Elevation line and value, devation in fact*
	(EL S87) Base Flood Elevation value where uniform within zone; elevation in foct
	*Referenced to the North American Vertical Datum of 1988
	A Goss section line (23)(23) Transect line
	45° 02' 08° 83° 02' 12" Geographic coordinates referenced to the North American Datum of 1983 (NAD 63)

	3776 zone (FEPSZONE 1203) Transverse Mexcator DX6810 _X Bench mark (see explanation in Notes to Users section of this FIRM genetic
	M1 5 River Mile
Ser Ser French III	FEDERAL EMERGENCY MANAGEMENT AGENCY
THOMAS	FLOOD INSURANCE RATE MAP
	COOK COUNTY, ILLINOIS
	AND INCORPORATED AREAS
	PANELS 488, 601 AND 602
.INE	COMMUNITY NUMBER PANELS SUFFIX
NO. 5.3.2	JUSTICE, 170112 601, 602 J
	VILLAGE OF WILLOW SPRINGS,170174 601 J
	VILLAGE OF
	COOK COUNTY 170054 601 J
	MAP REVISED AUGUST 19, 2008
	AUGUST 19, 2008
	EXHIBIT 5.3
	NO. RR-14-4223 SHEET NO.
	HIBIT 5.3 JRANCE RATE MAP 5.3.3 OF 5.3.7



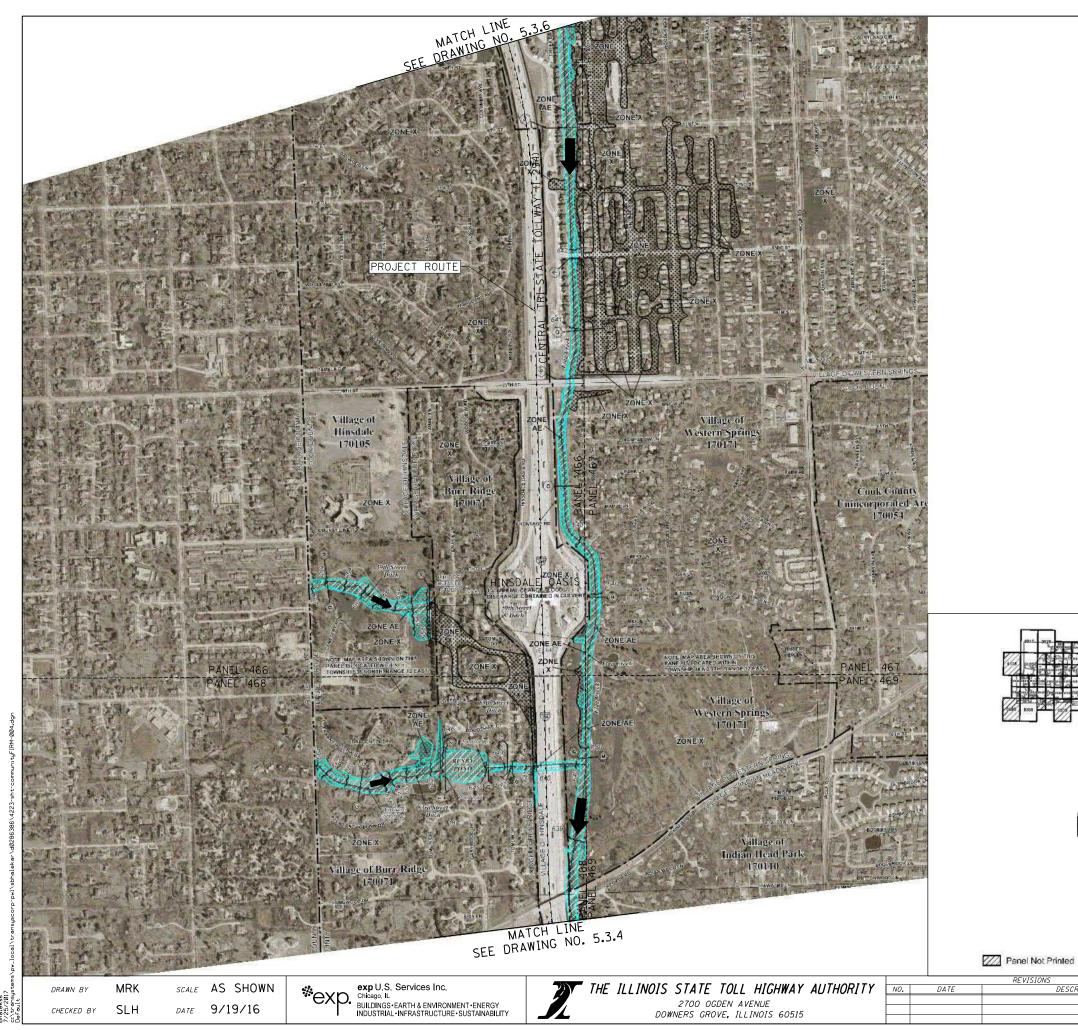




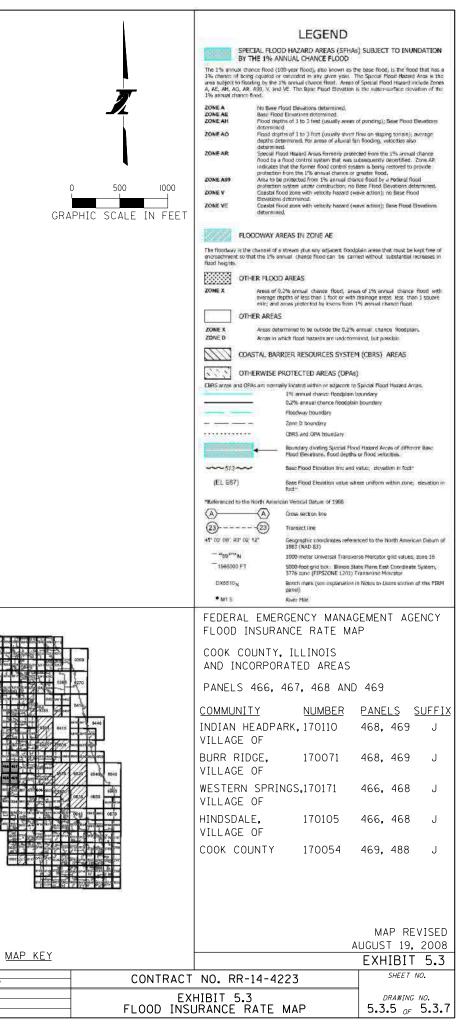
		LEGEND			
		ARD AREAS (SFHAS	s) SUBJECT	TO INUN	DATION
The 1% annual chance fi 1% chance of being equi area subject to flooding t A, AE, AH, AO, AR, A09, 1% annual chance flood.	alod or excend y the 1% annu V, and VE. Th	ficod), also known as th od in any given year. T al chance flood. Areas o e Bake Flood Elevation (the Special Flo	load Hazard od Hazard in	Arda is the clude Zones
ZONE AE Bat ZONE AH Flo	se Flood Elevati	vations determined. one dotermined. to 0 feet (usually areas	of ponding};	Sase Flood E	levetions
ZONE AO Flo dej	od depths of 1 aths determines	to 3 freet (usually sheet) I. For areas of alluvial fa	flow on slapi in flooding, v	ng tamain); a elocities also	Norage.
ZONEAR Sp no ind	licakes that the	and Areas formerly prote introl system that was si former flood control syst	terr is being i	restored to p	chance Zone AR rovide
ZONE A99 AN	a to be protect	e 1% annual chance or ed from 1% annual char ander construction; no l	nce flood by .	a Federal floo	
ZONE V Co Ele	astal flood zone Nations determ	with velocity hazard (w	ave action);	no Base Floo	d
	ermined.	Part of sector residence for	ave actually,		
FLOODW	AY AREAS I	N ZONE AE			
The floodway is the chain encroachment so that the flood heights.	nel of a stream 1% annual of	plus any adjacent flood; ance flood can be carr	plain areas th Netl without	et must be k substantial in	ept free of creases in
here and a second	LOOD AREA				
TVP	rade depths of	ual chance flood, area less than 1 foot or with atorted by levers frain 1	thainson are	as less that	flood with 1 square
		to be outside the 0.2%			3
		ad hazarda are undetorr			23
COASTAI	. BARRIER F	ESOURCES SYSTEM	(CBRS)	AREAS	
CBRS areas and OPAs are		TED AREAS (OPAs)		d Hazard Arc	35.
	1% av	inual chance fleodplain l annual chance fleodplair	ooundary		
	Floods	way boundary	1240030 *0340 * 0		
		D boundary and OPA boundary			
+	Bound Flood	ary dividing Special Floo Elevations, flood depths	of Hazard Arc or flood velo	as of difform cities.	w Base
		food Elevation line and			
(EL 987)	foct*	food Elevation value wh	ere uniform	within zone;	elevation in
*Referenced to the North		cal Datum of 1968 section line			
232	3) Transi	sctline			
45" 02" 08", 83" 02" 12"	Geogr 1983 (aphic coordinates refere NAD 83)	nced to the P	korth America	an Datum of
*59***N 1565000 FT	50004	neter Universal Transve foot grid tick: Illinois Str	ste Flane Eas	t Coordinate	
DX5510X	Bench	tone (FIPSZONE 1201) T mark (see explanation i			of this FIRM
• M1 5	pane) River				
FEDERAL E				T AGE	ENCY
COOK COUN					
AND INCOR			6.01		
PANELS 46					
<u>COMMUNITY</u> HODGKINS,		NUMBER			
VILLAGE OF		170106	469,	400	J
WILLOW SPF VILLAGE OF	RINGS,	170174	469		J
COUNTRYSID CITY OF	ε,	170079	469,	488	J
INDIAN HEAI VILLAGE OF		170110	468,	469	J
BURR RIDGE VILLAGE OF		170071	468,	469	J
HINDSDALE, VILLAGE OF		170105	468,	469	J
COOK COUN	ΓY	170054	469,	488	J

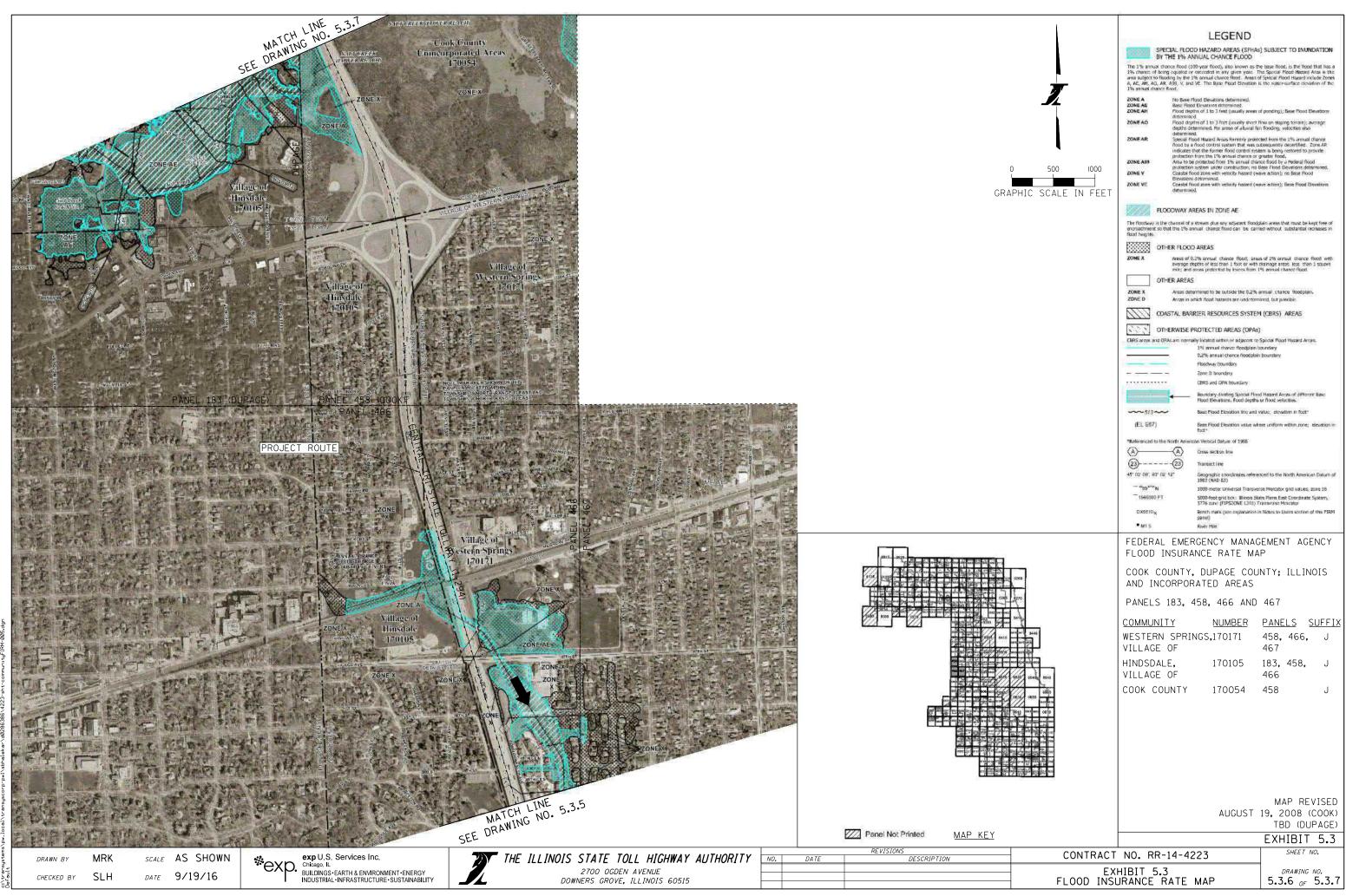
	EXHIBIT 5.3
CONTRACT NO. RR-14-4223	SHEET NO.
EXHIBIT 5.3 FLOOD INSURANCE RATE MAP	drawing no. 5.3.4 _{OF} 5.3.7

MAP REVISED AUGUST 19, 2008

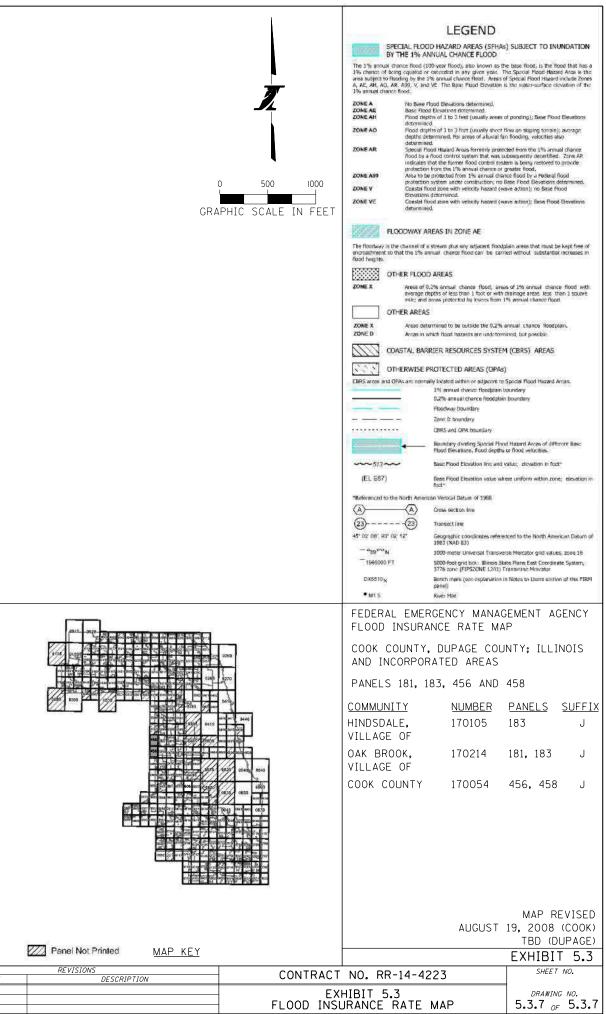


REVISION DESCRIPTION









bhalekss 7/25/2017

5.4 WATERWAY INFORMATION TABLE



MAJOR CULVERT (WC # 2) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCP 42"	Computed by: EL	Date:	7/20/2017
Section:	4223	S.N. Prop:	RCP 42"		_	
County:	Cook	Waterway:	Storm System East of I-294	Checked by: JC	Date:	7/21/2017
Station:	1007+20				_	

Drainage Area =	0.0079 sq.	mi	E	Existing Overtop	ping Elevation:	628.50	ft. @ Sta.	1010+65	
	5.07	' ac	Pr	oposed Overtop	ping Elevation:	627.71	ft. @ Sta.	1010+15	
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater E	lev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	15.10	7.70	7.70	624.09	0.00	0.00	624.09	624.09
Design	50	16.10	8.92	8.92	624.51	0.00	0.00	624.51	624.51
Base	100	17.00	9.49	9.49	624.67	0.00	0.00	624.67	624.67
OVT(E)	> 500 - Yr	-	-	-	-	-	-	-	-
OVT(P)	> 500 - Yr	-	-	-	-	-	-	-	-
Max. Calc.	500	18.00	10.47	10.47	624.79	0.00	0.00	624.79	624.79
					10-Year Velo	city through Ex	kisting Culvert =	1.68	fps

10-Year Velocity through Proposed Culvert =

1.68 fps 1.67 fps

OVT = Overtopping Event (E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A

SCOPE OF WORK:

EXISTING CULV	'ERT	
Bridge or Culvert Type:	42" RCP	
Cell Dimensions (W x H):		
# of span \ cells:	1	
Length:	224	
U/S Flowline:	621.31	
D/S Flowline:	620.62	
Skew:	0	
Low EOP:	628.5 @ 1010+65 SB SIDE	
EXISTING DROPE	BOX	

XISTING DROPE	BOX
Dimensions:	
Drop:	
Weir Elevation:	

PROPOSED CULVERT						
Culvert Type:	42" RCP					
Cell Dimensions (W x H):						
# of span \ cells:	1					
Length:	232					
U/S Flowline:	621.31					
D/S Flowline:	620.61					
Skew:	0					
Low EOP:	627.71 @ 1010+15 SB SIDE					
PROPOSED DRO Dimensions:	PBOX					
Drop:						
Weir Elevation:						

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS

Circular Culvert (42") under I-294 (@Station 1007+20)

Tran Sys	tems>			
Computed by:	EL	Date:	7/20/2017	
Checked by:	JC	Date:	7/21/2017	

Route:	Tri-State Tollway (I-294)	S.N. Exist: RCP 42"
Section:	4223	S.N. Prop: RCP 42"
County:	Cook	Waterway: Storm System East of I-294
Station:	1007+20	

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head (ft) @ Approach Section	
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed
	10	624.09	624.09	624.09	0.00	0.00
Design	50	624.51	624.51	624.51	0.00	0.00
Base	100	624.67	624.67	624.67	0.00	0.00
Max. Calc.	500	624.79	624.79	624.79	0.00	0.00

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
628.50	627.71			10	624.09	624.09	4.41	3.62		
Low Road S	station:	Low Beam Station:		50	624.51	624.51	3.99	3.20		
Existing	Proposed	Existing	Proposed	100	624.67	624.67	3.83	3.04		
1010+65	1010+15			500	624.79	624.79	3.71	2.92		

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50 year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50 year natural high water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	624.09	624.09	621.31	621.31	2.78	2.78			7.70	7.70
Design	50	624.51	624.51	621.31	621.31	3.20	3.20			8.92	8.92
Base	100	624.67	624.67	621.31	621.31	3.36	3.36			9.49	9.49
Max. Calc.	500	624.79	624.79	621.31	621.31	3.48	3.48			10.47	10.47

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.



MAJOR CULVERT (WC # 14) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	S.N. Exist:	CMP 54" (HDPE Lined Culvert Opening 40")	Computed by:	SB	Date:	6/27/2017
Section:		S.N. Prop:	RCP 54"				
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by:	KS	Date:	6/27/2017
Station:	1231+53.						

Drainage Area =	0.0671 sq. m	ni (42.97 acres)	E	xisting Overtopp	oing Elevation:	656.41	ft. @ Sta.	1233+09				
-			Pro	posed Overtop	ping Elevation:	658.15	ft. @ Sta.	1233+00				
Flood	Frequency	Discharge	Waterway O	Waterway Opening (sq. ft)		Hea	Head (ft)		lev. (ft)			
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed			
Ten-Year	10	17	2	1	631.1	1.0	0.9	632.1	632.0			
Design	50	35	9	12	633.2	0.6	0.2	633.9	633.5			
Base	100	43	9	16	634.1	1.0	0.3	635.1	634.4			
OVT(E)	> 500 - Yr											
OVT(P)	> 500 - Yr											
Max. Calc.	500	80	9	16	635.3	3.8	1.4	639.1	636.7			
	10-Year Velocity through Existing Culvert = 5.54 fps											

10-Year Velocity through Existing Cuivert = 10-Year Velocity through Proposed Culvert =

fps 5.18

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A

SCOPE OF WORK:

EXISTING CUL	VERT
Bridge or Culvert Type:	CMP Circular Culvert
Cell Dimensions (W x H):	Dia 54" (Lined Culvert Opening 40")
# of span \ cells:	1
Length:	305'
U/S Flowline:	630.15
D/S Flowline:	628.72
Skew:	5°
Low EOP:	656.41

EXISTING DROPBOX

	DOM
Dimensions:	N/A
Drop:	N/A
Weir Elevation:	N/A

PROPOSED CI	JLVERT
Culvert Type:	RCP Circular Culvert
Cell Dimensions (W x H):	Dia 54"
# of span \ cells:	1
Length:	321'
U/S Flowline:	630.23
D/S Flowline:	628.72
Skew:	5°
Low EOP:	658.15
PROPOSED DF	ROPBOX

Dimensions: N/A								
N/A								
N/A								
N/A								

NOTES:

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS (WC # 14) Circular Culvert (54") under I-294 (@Station 1231+53)

Route: Section:	Tri-State Tollway (I-294)	S.N. Exist: S.N. Prop;	54" CMP (HDPE Lined Culvert, Opening - 40") 54" RCP	Computed by:	SB	Date:	6/27/2017
County:	Cook	Waterway:	54 RCP Unnamed ditch tributary to Flagg Creek	Checked by:	KS	Date:	6/27/2017
Station:	1231+53.						

*exp

Created Head Calculations

Flood	Freq.			Proposed Headwater Elev. (ft)	Created Head Elev. (ft)		
	Year	U/S Face of structure/Approach section Sta. 835	U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	631.11	632.12	632.00	1.01	0.89	
Design	50	633.22	633.86	633.45	0.64	0.23	
Base	100	634.13	635.12	634.44	0.99	0.31	
Max. Calc.	500	635.29	639.05	636.72	3.76	1.43	

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	levation (ft) Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)		
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
656.41	658.15	NA	NA	10	632.12	632.00	24.29	26.15	NA	NA
Low Road S	tation:	Low Beam	Station:	50	633.86	633.45	22.55	24.70	NA	NA
Existing	Proposed	Existing	Proposed	100	635.12	634.44	21.29	23.71	NA	NA
1233+09	1233+00	NA	NA	500	639.05	636.72	17.36	21.43	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Circular Culvert Dia. (inch)		Opening Area (ft ²)	
	Year	Existing @ 835	Proposed @ 835	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	631.11	631.11	630.15	630.23	0.96	0.88	54" (Opening - 40")	54"	1.57	1.27
Design	50	633.22	633.22	630.15	630.23	3.07	2.99	54" (Opening - 40")	54"	8.70	12.40
Base	100	634.13	634.13	630.15	630.23	3.98	3.90	54" (Opening - 40")	54"	8.70	15.90
Max. Calc.	500	635.29	635.29	630.15	630.23	5.14	5.06	54" (Opening - 40")	54"	8.70	15.90

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.



MAJOR CULVERT (WC # 15) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	S.N. Exist:	CMP 54" (HDPE Lined Culvert Opening 40")	Computed by:	SB	Date:	6/27/2017
Section:		S.N. Prop:	RCP 54"				
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by:	KS	Date:	6/27/2017
Station:	1239+52.						

Drainage Area =	0.0253 sq. m	ii (16.2 acres)	Existing Overtopping Ele		oing Elevation:	653.50	ft. @ Sta.	1238+02	
-			Pro	posed Overtop	ping Elevation:	654.16	ft. @ Sta.	1238+00	
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	13	9	16	632.0	0.1	0.0	632.1	632.0
Design	50	22	9	16	633.9	0.2	0.1	634.2	634.0
Base	100	25	9	16	634.8	0.3	0.1	635.1	634.9
OVT(E)	> 500 - Yr								
OVT (P)	> 500 - Yr								
Max. Calc.	500	40	9	16	636.0	0.8	0.3	636.8	636.3
					10-Year Veloo	city through Ex	isting Culvert =	1.48	fps

10-Year Velocity through Proposed Culvert =

0.87 fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A

SCOPE OF WORK:

EXISTING CUL	/ERT							
Bridge or Culvert Type: CMP Circular Culvert								
Cell Dimensions (W x H):	Dia 54" (Lined Culvert Opening 40")							
# of span \ cells:	1							
Length:	233'							
U/S Flowline:	628.04							
D/S Flowline:	626.40							
Skew:	0°							
Low EOP:	653.5							

EXISTING DROPBOX

Dimensions:	N/A
Drop:	N/A
Weir Elevation:	N/A

PROPOSED CULVERT Culvert Type: <u>RCP Circular Culvert</u> Cell Dimensions (W x H): Dia 54" # of span \ cells: 1 Length: 266' U/S Flowline: 628.27 D/S Flowline: 626.4 Skew: 0° Low EOP: 654.16

PROPOSED DROPBOX

Dimensions:	N/A
Drop:	N/A
Weir Elevation:	N/A

NOTES:

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS (WC # 15) Circular Culvert (54") under I-294 (@Station 1239+52)

Route: Section:	Tri-State Tollway (I-294)	S.N. Exist: S.N. Prop:	54" CMP (HDPE Lined Culvert, Opening - 40") 54" RCP	Computed by:	SB	Date:	6/27/2017
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by:	KS	Date:	6/27/2017
Station:	1239+52.						

*ехр.

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	· Created Head Fley. (ff)	
	Year	U/S Face of structure/Approach section Sta. 453	U/S Face of Structure	U/S Face of Structure	Existing	Proposed
	10	631.99	632.07	632.02	0.08	0.03
Design	50	633.93	634.15	634.00	0.22	0.07
Base	100	634.76	635.06	634.86	0.30	0.10
Max. Calc.	500	636.01	636.80	636.27	0.79	0.26

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
653.50	654.16	NA	NA	10	632.07	632.02	21.43	22.14	NA	NA
Low Road S	tation:	Low Beam	Station:	50	634.15	634.00	19.35	20.16	NA	NA
Existing	Proposed	Existing	Proposed	100	635.06	634.86	18.44	19.30	NA	NA
1238+02	1238+00	NA	NA	500	636.80	636.27	16.70	17.89	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U	I/S Face of Structure	U/S Invert E	levation (ft)	Depth c	of Water	Circular Culv	ert Dia. (inch)	Opening	Area (ft ²)
	Year	Existing @ 453	Proposed @ 453	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	631.99	631.99	628.04	628.27	3.95	3.72	54" (Opening - 40")	54"	8.70	15.90
Design	50	633.93	633.93	628.04	628.27	5.89	5.66	54" (Opening - 40")	54"	8.70	15.90
Base	100	634.76	634.76	628.04	628.27	6.72	6.49	54" (Opening - 40")	54"	8.70	15.90
Max. Calc.	500	636.01	636.01	628.04	628.27	7.97	7.74	54" (Opening - 40")	54"	8.70	15.90

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.



BRIDGE (WC # 16) WATERWAY INFORMATION TABLE

exp

Route: Section: County: Station:

Tri-State Tollway (I-294) North of BNSF RR Cook 1257+00 S.N. Exist: BN 243 (NB) & BN 244 (SB) S.N. Prop: BN 243 (NB) & BN 244 (SB) Waterway: Flagg Creek

Computed by: KS	Date:	5/2/2017
Checked by: SH	Date:	5/2/2017

Drainage Area = 13.969 sq. mi Existing Overtoppi			opping Elevatio	n:		642.47	@ Sta.	1264+00	
			Proposed Overtopping Elevation: 642.33				642.33	@ Sta.	1264+00
Flood Event	Frequency	Discharge	Waterway Opening (sq. ft) Natural		Hea	Head (ft)		Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
	10	1073.1	600.53	621.40	633.48	0.41	0.35	633.89	633.83
Design	50	1833.1	845.98	872.51	635.72	0.45	0.38	636.17	636.10
Base	100	2236.5	920.88	949.27	636.34	0.46	0.40	636.80	636.74
Scour Design Check									
Overtop Existing	> 500 - Yr								
Overtop Proposed	> 500 - Yr								
Max. Calc.	500	3226.9	1064.60	1091.20	637.43	0.49	0.41	637.92	637.84
					10-Year Ve	elocity through E	xisting Bridge =	1.79	fps
					40.14			4 70	e

10-Year Velocity through Proposed Bridge =

1.73 fps

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: 637.41 (October 1954)

SCOPE OF WORK:

EXISTING STRUCTUR	E	PROPOSED STRUCTUR	E
TYPE:	2-span PCC girder bridge	TYPE: -	Single span PCC girder bridge
LENGTH:	163'-3" (Bk. To Bk. of Abutments)	LENGTH: -	123'-8" (Bk. To Bk. of Abutments)
# SPANS:	2	# SPANS: -	1
LOW BEAM:	642.91	LOW BEAM: -	640.61
SKEW:	30°	SKEW: -	30°
LOW EOP:	642.47	LOW EOP: -	642.33

NOTES: Existing and proposed bridge meet Tollway's freeboard and clearance criteria. Proposed Structure (Alternative 8R) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS

I-294 Bridge over the Flagg Creek (@Station 1257+00)

[%] exp.			
Computed by:	KS	Date:	5/2/2017
Checked by:	SH	Date:	5/2/2017

Created Head Calculations

BN 243 (NB) & BN 244 (SB)

BN 243 (NB) & BN 244 (SB)

Flagg Creek

Flood	Freq.	Natural H	1.W.E. (ft)	Existing	Existing Headwater Elev. (ft)		adwater Elev. (ft)	Created Head (ft) @ Approach Section		
	Year	U/S Face of Structure @ 23305.6	Approach section U/S @ 23365.6	U/S Face of Structure @ 23305.6	Approach section U/S @ 23365.6	U/S Face of Structure @ 23305.6	Approach section U/S @ 23365.6	Existing	Proposed	
	10	633.48	633.49	633.89	633.90	633.83	633.84	0.41	0.35	
Design	50	635.72	635.74	636.17	636.19	636.10	636.12	0.45	0.38	
Base	100	636.34	636.36	636.80	636.82	636.74	636.76	0.46	0.40	
Max. Calc.	500	637.43	637.46	637.92	637.95	637.84	637.87	0.49	0.41	

(1) The natural highwater elevation is the water surface elevation at the upstream end of the crossing, as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the approach section, and not at the U/S face of the bridge/culvert. The difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head.

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwater	Elev. (ft)	Freebo	ard (ft)	Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
642.47	642.33	642.91	640.61	10	633.89	633.83	8.58	8.50	9.02	6.78
Low Road S	station:	Low Beam	Station:	50	636.17	636.10	6.30	6.23	6.74	4.51
Existing	Proposed	Existing	Proposed	100	636.80	636.74	5.67	5.59	6.11	3.87
1264+00	1264+00	1257+00	1257+00	500	637.92	637.84	4.55	4.49	4.99	2.77

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

Tri-State Tollway (I-294)

North of BNSF RR

Cook

1257+00

Route:

Section:

County:

Station:

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

S.N. Exist:

S.N. Prop:

Waterway:

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E of Stru	. (ft) - U/S Face cture	Stream Bottom Elev.		Depth of Water		**Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	633.48	633.48	624.12	624.12	9.36	9.36	600.53	621.40
Design	50	635.72	635.72	624.12	624.12	11.60	11.60	845.98	872.51
Base	100	636.34	636.34	624.12	624.12	12.22	12.22	920.88	949.27
Max. Calc.	500	637.43	637.43	624.12	624.12	13.31	13.31	1064.60	1091.20

** 'Proposed structure waterway opening is larger than existing due to absense of pier.

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.

WSEL Summary Table - Created Head Calculations WC16 10-Year

	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - EX WSE
X-sect	WSE	WSE	WSE			
24186.93	633.85	634.21	634.15	0.36	0.30	-0.06
23915.05	633.69	634.07	634.01	0.38	0.32	-0.06
23864.58	633.69	634.07	634.01	0.38	0.32	-0.06
23606.53	633.58	633.98	633.92	0.40	0.34	-0.06
23476.6	633.55	633.95	633.88	0.40	0.33	-0.07
23365.6	633.49	633.90	633.84	0.41	0.35	-0.06
23305.6	633.48	633.89	633.82	0.41	0.34	-0.07
23201.92/Bridge						

			50-Year			
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - E
X-sect	WSE	WSE	WSE			
24186.93	636.17	636.55	636.49	0.38	0.32	-0.06
23915.05	636.01	636.42	636.36	0.41	0.35	-0.06
23864.58	636.00	636.41	636.34	0.41	0.34	-0.07
23606.53	635.86	636.30	636.23	0.44	0.37	-0.07
23476.6	635.80	636.25	636.18	0.45	0.38	-0.07
23365.6	635.74	636.19	636.12	0.45	0.38	-0.07
23305.6	635.72	636.18	636.11	0.46	0.39	-0.07
23201.92/Bridge						
			100-Year			
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - E WSE
X-sect	WSE	WSE	WSE			
24186.93	636.84	637.22	637.16	0.38	0.32	-0.06
23915.05	636.67	637.07	637.02	0.40	0.35	-0.05
23864.58	636.65	637.06	637.00	0.41	0.35	-0.06
23606.53	636.50	636.94	636.88	0.44	0.38	-0.06
23476.6	636.44	636.89	636.82	0.45	0.38	-0.07
23365.6	636.36	636.82	636.76	0.46	0.40	-0.06
23305.6	636.34	636.81	636.74	0.47	0.40	-0.07
23201.92/Bridge						
			500-Year			
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - E WSE
X-sect	WSE	WSE	WSE			
24186.93	638.06	638.44	638.38	0.38	0.32	-0.06
23915.05	637.86	638.28	638.21	0.42	0.35	-0.07
23864.58	637.85	638.27	638.20	0.42	0.35	-0.07
23606.53	637.65	638.11	638.03	0.46	0.38	-0.08
23476.6	637.57	638.04	637.96	0.47	0.39	-0.08
23365.6	637.46	637.95	637.87	0.49	0.41	-0.08
23305.6	637.43	637.92	637.84	0.49	0.41	-0.08
23201.92/Bridge						



MAJOR CULVERT (WC # 17) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 2-10' X 5'	Computed by: KS	Date:	12/14/2017
Section:		S.N. Prop:	RCBC 2-10' X 5'		_	
County:	Cook	Waterway:	Plainfield Road Ditch	Checked by: SLH	Date:	12/14/2017
Station:	1279+66				_	

Drainage Area =	1.69 sq. mi		Ex	isting Overtopp	oing Elevation:	643.64	ft. @ Sta.	1279+88	
-	-		Pro	posed Overtop	ping Elevation:	645.98	ft. @ Sta.	1279+00	
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater E	Elev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	197	30	37	637.8	0.2	0.0	638.0	637.8
Design	50	310	40	52	638.5	0.3	0.0	638.9	638.5
Base	100	367	44	58	638.9	0.4	0.0	639.3	638.9
OVT(E)	> 500 - Yr								
OVT (P)	> 500 - Yr								
Max. Calc.	500	510	57	74	639.6	0.7	0.0	640.3	639.7
					10-Year Veloo	city through Ex	isting Culvert =	6.8	fps

10-Year Velocity through Proposed Culvert =

6.8 fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: 639.7 (October 1954)

SCOPE OF WORK:

EXISTING CULVE	RT	PROPOSED CULV	ERT
Bridge or Culvert Type: C	oncrete Box Culvert	Culvert Type: Con	crete Box Culvert (extension)
Cell Dimensions (W x H): D	ouble 10' (W) x 5' (H)	Cell Dimensions (W x H): Dou	ole 10' (W) x 5' (H)
# of span \ cells:	2	# of span \ cells:	2
Length:	462.33'	Length:	491.33'
U/S Flowline:	635.65	U/S Flowline:	635.93
D/S Flowline:	631.18	D/S Flowline:	631.18
Skew:		Skew:	
Low EOP:	643.64	Low EOP:	645.98
EXISTING DROPB	X	PROPOSED DROPB	хс
Dimensions:	n/a	Dimensions:	n/a
Drop:	n/a	Drop:	n/a
Weir Elevation:	n/a	Weir Elevation:	n/a

NOTES: Proposed Structure (Alt 8R) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS



Double Box Culvert (10' x 5') under I-294 (@Station 1279+66)

RCBC 2-10' X 5'

RCBC 2-10' X 5'

Plainfield Road Ditch

Created Head Calculations

Flood	Freq.	Natural H.W.E. ⁽¹⁾ (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head Fley, (ff)		
	Year	U/S Face of structure Sta. 537.79	U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	637.76	637.97	637.81	0.21	0.05	
Design	50 638.51		638.85	638.54	0.34	0.03	
Base	100	638.85	639.25	638.87	0.40	0.02	
Max. Calc.	500	639.62	640.29	639.65	0.67	0.03	

S.N. Exist:

S.N. Prop:

Waterway:

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This metho d of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwate	er Elev. (ft)	Freebo	ard (ft)	Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
643.64	645.98	NA	NA	10	637.97	637.81	5.67	8.17	NA	NA
Low Road S	station:	Low Bean	n Station:	50	638.85	638.54	4.79	7.44	NA	NA
Existing	Proposed	Existing	Proposed	100	639.25	638.87	4.39	7.11	NA	NA
1279+88	1279+00	NA	NA	500	640.29	639.65	3.35	6.33	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

Route:

Section:

County:

Station:

Tri-State Tollway (I-294)

Cook

1279+66

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.		. (ft) - U/S Face of cture	U/S Invert Elevation (ft)		Depth of Water		Box Culve	ert Size (ft x ft)	Opening Area (ft ²)	
	Year	Existing @ 509	Proposed @ 537.79	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	637.16	637.76	635.65	635.93	1.51	1.83	2- 10' (W) x 5' (H)	2- 10' (W) x 5' (H)	30.20	36.60
Design	50	637.64	638.51	635.65	635.93	1.99	2.58	2- 10' (W) x 5' (H)	2- 10' (W) x 5' (H)	39.80	51.60
Base	100	637.87	638.85	635.65	635.93	2.22	2.92	2- 10' (W) x 5' (H)	2- 10' (W) x 5' (H)	44.40	58.40
Max. Calc.	500	638.51	639.62	635.65	635.93	2.86	3.69	2- 10' (W) x 5' (H)	2- 10' (W) x 5' (H)	57.20	73.80

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.

WSEL Summary Table - Created Head Calculations WC17

			10-Year				
	Natural	Exist	Prop	Evict Not	Bron Not		
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WSE	
739	642.51	642.51	642.51	0.00	0.00	0.00	
700	642.52	642.52	642.52	0.00	0.00	0.00	
675	642.52	642.52	642.52	0.00	0.00	0.00	
650	642.52	642.52	642.52	0.00	0.00	0.00	
625	642.52	642.52	642.52	0.00	0.00	0.00	
603.4	642.52	642.52	642.52	0.00	0.00	0.00	
598.75	638.53	638.53	638.53	0.00	0.00	0.00	
588.026*	638.25	638.25	638.25	0.00	0.00	0.00	
577.303*	638.19	638.19	638.19	0.00	0.00	0.00	
566.58	637.68	637.92	637.98	0.24	0.30	0.06	
556.983*	637.72	637.95	638.02	0.23	0.30	0.07	
547.386*	637.75	637.96	638.02	0.21	0.27	0.06	
537.79*	637.76	637.97	637.81	0.21	0.05	-0.16	
528.193	637.78	637.98		0.20			
518.596	637.78	637.99		0.21			
509	637.16	637.71		0.55			
385.75/culvert							

			50-Year			
	Natural	Exist	Prop	Exist - Nat	Prop - Nat	
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WSE
739	643.01	643.01	643.01	0.00	0.00	0.00
700	643.04	643.04	643.04	0.00	0.00	0.00
675	643.04	643.04	643.04	0.00	0.00	0.00
650	643.04	643.04	643.04	0.00	0.00	0.00
625	643.04	643.04	643.04	0.00	0.00	0.00
603.4	643.04	643.04	643.04	0.00	0.00	0.00
598.75	638.78	638.78	638.78	0.00	0.00	0.00
588.026*	638.77	638.77	638.77	0.00	0.00	0.00
577.303*	638.49	638.89	638.89	0.40	0.40	0.00
566.58	638.45	638.81	638.81	0.36	0.36	0.00
556.983*	638.48	638.83	638.84	0.35	0.36	0.01
547.386*	638.49	638.84	638.84	0.35	0.35	0.00
537.79*	638.51	638.85	638.54	0.34	0.03	-0.31
528.193	638.52	638.86		0.34		
518.596	638.53	638.86		0.33		
509	637.64	638.49		0.85		
385.75/culvert						
			100-Year		•	
	Natural	Exist	Prop	Exist - Nat	Dura Nat	1
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS
739	643.21	643.21	643.21	0.00	0.00	0.00
700	643.25	643.26	643.25	0.01	0.00	-0.01
675	643.25	643.26	643.25	0.01	0.00	-0.01
650	643.25	643.26	643.25	0.01	0.00	-0.01
625	643.25	643.25	643.25	0.00	0.00	0.00
603.4	643.25	643.25	643.25	0.00	0.00	0.00
598.75	638.97	638.97	638.97	0.00	0.00	0.00
588.026*	638.96	639.00	638.96	0.04	0.00	-0.04
577.303*	638.92	639.33	639.30	0.41	0.38	-0.03
566.58	638.79	639.22	639.19	0.43	0.40	-0.03
556.983*	638.82	639.23	639.22	0.41	0.40	-0.01
547.386*	638.83	639.24	639.22	0.41	0.39	-0.02
537.79*	638.85	639.25	638.87	0.40	0.02	-0.38
528.193	638.86	639.26		0.40		
	638.86	639.26		0.40		
518.596						
518.596	637.87	638.85		0.98		

	500-Year										
	Natural	Exist	Prop	Exist - Nat	Prop - Nat						
X-sect	WSE	WSE	WSE	EXIST - INdt	Prop - Nat	PR WSE - EX WSE					
739	643.51	643.54	643.53	0.03	0.02	-0.01					
700	643.59	643.62	643.61	0.03	0.02	-0.01					
675	643.59	643.62	643.61	0.03	0.02	-0.01					
650	643.59	643.62	643.61	0.03	0.02	-0.01					
625	643.59	643.62	643.60	0.03	0.01	-0.02					
603.4	643.58	643.61	643.60	0.03	0.02	-0.01					
598.75	639.48	640.25	640.04	0.77	0.56	-0.21					
588.026*	639.45	640.30	640.10	0.85	0.65	-0.20					
577.303*	639.78	640.39	640.22	0.61	0.44	-0.17					
566.58	639.58	640.27	640.09	0.69	0.51	-0.18					
556.983*	639.60	640.28	640.10	0.68	0.50	-0.18					
547.386*	639.61	640.29	640.1	0.68	0.49	-0.19					
537.79*	639.62	640.29	639.65	0.67	0.03	-0.64					
528.193	639.63	640.29		0.66							
518.596	639.64	640.30		0.66							
509	638.51	639.82		1.31							
385.75/culvert											







Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 3-15' X 5'	Computed by: KS	Date:	12/14/2017
Section:		S.N. Prop:	RCBC 3-15' X 5'			
County:	Cook	Waterway:	63rd St. Ditch	Checked by: <u>SLH</u>	Date:	12/14/2017
Station:	1306+54					

Drainage Area =	5.38 sq. mi		E	kisting Overtopp	oing Elevation:	644.91	ft. @ Sta.	1307+66	
-			Pro	posed Overtop	ping Elevation:	643.57	ft. @ Sta.	1312+00	
Flood	Frequency	Discharge	Waterway Opening (sq. ft) Natural		Hea	ad (ft)	Headwater E	Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	272	40	40	637.4	0.6	0.6	638.0	638.0
Design	50	447	91	90	638.5	0.3	0.3	638.8	638.8
Base	100	547	132	131	639.4	0.1	0.1	639.5	639.5
OVT (E)	> 500 - Yr								
OVT (P)	> 500 - Yr								
Max. Calc.	500	893	212	212	641.2	0.2	0.2	641.4	641.4
10-Year Velocity through					city through Ex	isting Culvert =	5.79	fps	

10-Year Velocity through Existing Culvert = 10-Year Velocity through Proposed Culvert =

5.79 fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: 641.5 (October 1954)

Weir Elevation:

SCOPE OF WORK:

EXISTING CULV	ERT	
Bridge or Culvert Type: (Concrete Box Culvert	
Cell Dimensions (W x H):	Triple 15' (W) x 5' (H)	
# of span \ cells:	3	
Length:	233.5'	
U/S Flowline:	636.5	
D/S Flowline:	635.51	
Skew:	no	
Low EOP:	644.91	
EXISTING DROPE	OX	
Dimensions:	n/a	
Drop:	n/a	

PROPOSED CL	JLVERT	
Culvert Type:	Concrete Box Culvert (extension	n)
Cell Dimensions (W x H):	Triple 15' (W) x 5' (H)	_
# of span \ cells:	3	-
Length:	291.92'	_
U/S Flowline:	636.52	_
D/S Flowline:	635.27	-
Skew:	no	_
Low EOP:	643.57	_
PROPOSED DR		
U/S Flowline: D/S Flowline: Skew:	636.52 635.27 no 643.57	-

Dimensions:	n/a
Drop:	n/a
Weir Elevation:	n/a

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

n/a

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS

Triple Box Culvert (15' x 5') under I-294 (@Station 1306+50)

[%]exp.

Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 3-15' X 5'	Computed by:	KS	Date:	12/14/2017
Section:		S.N. Prop:	RCBC 3-15' X 5'				
County:	Cook	Waterway:	63rd St. Ditch	Checked by:	SLH	Date:	12/14/2017
Station:	1306+54						

Calculated Created Head

Flood Freq.		Freq. Natural H.W.E. ⁽¹⁾ (ft)		Proposed Headwater Elev. (ft)	Created Head Elev. (ft)		
	Year U/S Face of struc Sta. 530		U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	637.40	637.95	637.97	0.55	0.57	
Design	50	638.52	638.78	638.80	0.26	0.28	
Base	100	639.44	639.54	639.54	0.10	0.10	
Max. Calc.	500	641.22	641.39	641.42	0.17	0.20	

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This met hod of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Eleva	ation (ft) ⁽³⁾	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
644.91	643.57	NA	NA	10	637.95	637.97	6.96	5.60	NA	NA
Low Road S	Station:	Low Beam Station:		50	638.78	638.80	6.13	4.77	NA	NA
Existing	Proposed	Existing	Proposed	100	639.54	639.54	5.37	4.03	NA	NA
1307+66	1312+00	NA	NA	500	641.39	641.42	3.52	2.15	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing @ 530	Proposed @ 530	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	637.40	637.40	636.50	636.52	0.90	0.88	3- 15' (W) x 5' (H)	3- 15' (W) x 5' (H)	40	40
Design	50	638.52	638.52	636.50	636.52	2.02	2.00	3- 15' (W) x 5' (H)	3- 15' (W) x 5' (H)	91	90
Base	100	639.44	639.44	636.50	636.52	2.94	2.92	3-15' (W) x 5' (H)	3- 15' (W) x 5' (H)	132	131
Max. Calc.	500	641.22	641.22	636.50	636.52	4.72	4.70	3-15' (W) x 5' (H)	3- 15' (W) x 5' (H)	212	212

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.

WSEL Summary Table - Created Head Calculations WC18 10-Year

	Natural	Exist	Prop			
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS
776	639.37	639.37	639.37	0.00	0.00	0.00
726.75	639.00	639.00	639.00	0.00	0.00	0.00
677.5	638.61	638.61	638.61	0.00	0.00	0.00
628.25	638.22	638.27	638.28	0.05	0.06	0.01
579	637.93	638.12	638.13	0.19	0.20	0.01
569	637.66	638.08	638.10	0.42	0.44	0.02
540	637.47	638.07	638.1	0.60	0.63	0.03
530	637.40	637.95	637.97	0.55	0.57	0.02
412/culvert						0.02
	1					
			50-Year			
	Natural	Exist	Prop	Exist - Nat	Prop - Nat	
X-sect	WSE	WSE	WSE	Exist - Nat	FTOP - Nat	PR WSE - EX WS
776	639.66	639.66	639.66	0.00	0.00	0.00
726.75	639.33	639.36	639.37	0.03	0.04	0.01
677.5	638.96	639.13	639.14	0.17	0.18	0.01
628.25	638.70	639.01	639.03	0.31	0.33	0.02
579	638.58	638.96	638.98	0.38	0.40	0.02
569	638.54	638.95	638.97	0.41	0.43	0.02
540	638.53	638.93	638.95	0.40	0.42	0.02
530	638.52	638.78	638.8	0.26	0.28	0.02
550	000.02					
412/culvert	000.02					
	000.02					
	000.02		100-Year			
	Natural	Exist	100-Year Prop			
				Exist - Nat	Prop - Nat	PR WSE - EX WS
412/culvert	Natural	Exist	Prop	Exist - Nat	Prop - Nat	PR WSE - EX WS 0.01
412/culvert X-sect	Natural WSE	Exist WSE	Prop WSE			0.01
412/culvert X-sect 776	Natural WSE 639.84	Exist WSE 639.92	Prop WSE 639.93	0.08	0.09	0.01 0.00
412/culvert X-sect 776 726.75	Natural WSE 639.84 639.69	Exist WSE 639.92 639.84	Prop WSE 639.93 639.84	0.08	0.09	0.01 0.00 0.00
412/culvert X-sect 776 726.75 677.5	Natural WSE 639.84 639.69 639.58	Exist WSE 639.92 639.84 639.77	Prop WSE 639.93 639.84 639.77	0.08 0.15 0.19	0.09 0.15 0.19	0.01 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25	Natural WSE 639.84 639.69 639.58 639.52	Exist WSE 639.92 639.84 639.77 639.73	Prop WSE 639.93 639.84 639.77 639.73	0.08 0.15 0.19 0.21	0.09 0.15 0.19 0.21	0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25 579	Natural WSE 639.84 639.69 639.58 639.52 639.49	Exist WSE 639.92 639.84 639.77 639.73 639.73	Prop WSE 639.93 639.84 639.77 639.73 639.71	0.08 0.15 0.19 0.21 0.22	0.09 0.15 0.19 0.21 0.22	0.01 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.48	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70	0.08 0.15 0.19 0.21 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22	0.01 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25 579 569 540	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.49 639.48 639.45	Exist WSE 639.92 639.84 639.77 639.73 639.73 639.71 639.70 639.67	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67	0.08 0.15 0.19 0.21 0.22 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22 0.22	0.01 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 540 530	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.49 639.48 639.45	Exist WSE 639.92 639.84 639.77 639.73 639.73 639.71 639.70 639.67	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67	0.08 0.15 0.19 0.21 0.22 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22 0.22	0.01 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 540 530	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.49 639.48 639.45	Exist WSE 639.92 639.84 639.77 639.73 639.73 639.71 639.70 639.67	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67	0.08 0.15 0.19 0.21 0.22 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22 0.22	0.01 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 540 530	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.49 639.48 639.45	Exist WSE 639.92 639.84 639.77 639.73 639.73 639.71 639.70 639.67	Prop WSE 639.93 639.77 639.71 639.71 639.71 639.71 639.70 639.67 639.54	0.08 0.15 0.21 0.22 0.22 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.22 0.10	0.01 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 540 530	Natural WSE 639.84 639.58 639.52 639.49 639.49 639.49 639.49 639.44 639.45 639.44	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.71 639.67 639.67 639.54	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67 639.67 639.54 500-Year	0.08 0.15 0.19 0.21 0.22 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22 0.22	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
X-sect 776 726.75 677.5 628.25 579 569 540 530 412/culvert	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.48 639.48 639.44 639.45 639.44	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70 639.67 639.67 639.54 Exist	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67 639.67 639.54 500-Year Prop	0.08 0.15 0.21 0.22 0.22 0.22 0.22	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.22 0.10	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25 579 569 540 530 412/culvert X-sect	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.48 639.45 639.45 639.44 Say.44 WSE	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70 639.67 639.54 Exist WSE	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67 639.54 500-Year Prop WSE	0.08 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Exist - Nat	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.10	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25 579 569 540 530 412/culvert X-sect 776	Natural WSE 639.84 639.69 639.52 639.52 639.49 639.45 639.45 639.45 639.45 639.45 639.45 639.45 639.44 WSE 641.27	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70 639.67 639.54 Exist WSE 641.57	Prop WSE 639.93 639.77 639.71 639.71 639.71 639.70 639.67 639.54 500-Year Prop WSE 641.60	0.08 0.15 0.21 0.22 0.22 0.22 0.10 Exist - Nat	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Prop - Nat	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25 579 569 540 530 412/culvert X-sect 776 726.75	Natural WSE 639.84 639.69 639.52 639.49 639.49 639.49 639.44 639.45 639.44 639.45 639.45 639.45 639.46 639.47 639.48 639.41 WSE 641.27 641.31	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70 639.67 639.54 Exist WSE 641.57 641.61	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67 639.54 500-Year Prop WSE 641.60 641.64	0.08 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Exist - Nat 0.30 0.30	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Prop - Nat 0.33 0.33	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 540 530 412/culvert X-sect 776 726.75 677.5	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.49 639.45 639.45 639.44 639.45 639.46 639.47 Matural WSE 641.27 641.29	Exist WSE 639.92 639.84 639.77 639.73 639.73 639.70 639.67 639.67 639.54 Exist WSE 641.67 641.61 641.60	Prop WSE 639.93 639.84 639.77 639.73 639.70 639.70 639.67 639.54 500-Year Prop WSE 641.60 641.63	0.08 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Exist - Nat 0.30 0.30	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Prop - Nat 0.33 0.33 0.34	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 540 530 412/culvert X-sect 776 726.75 628.25 530 530 530 530 530 530 530 53	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.48 639.44 639.45 639.46 639.47 639.48 639.44 0 Natural WSE 641.27 641.28	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70 639.70 639.67 639.54 Exist WSE 641.57 641.61 641.60 641.59	Prop WSE 639.93 639.84 639.77 639.73 639.71 639.70 639.67 639.54 500-Year Prop WSE 641.60 641.63 641.62	0.08 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Exist - Nat 0.30 0.30 0.31	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.22 0.10 Prop - Nat 0.33 0.33 0.34 0.34	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 628.25 579 569 530 412/culvert X-sect 776 726.75 677.5 677.5 677.5 677.5 677.5 677.5 628.25 579 569	Natural WSE 639.84 639.69 639.52 639.49 639.49 639.44 639.45 639.44 639.45 639.44 WSE 641.27 641.28 641.27 641.27	Exist WSE 639.92 639.84 639.77 639.73 639.71 639.70 639.67 639.54 Exist WSE 641.57 641.61 641.60 641.59 641.59 641.59	Prop WSE 639.93 639.77 639.73 639.71 639.70 639.71 639.70 639.71 639.73 639.74 500-Year Prop WSE 641.60 641.63 641.62 641.62 641.62 641.62	0.08 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Exist - Nat 0.30 0.30 0.31 0.31 0.31 0.32	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Prop - Nat 0.33 0.33 0.34 0.34 0.34 0.34	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00
412/culvert X-sect 776 726.75 677.5 628.25 579 569 540 530 412/culvert X-sect 776 726.75 628.25 579 530	Natural WSE 639.84 639.69 639.58 639.52 639.49 639.49 639.44 639.45 639.44 039.45 639.44 039.45 641.27 641.21 641.28 641.28	Exist WSE 639.92 639.84 639.77 639.73 639.73 639.71 639.70 639.67 639.54 Exist WSE 641.57 641.61 641.59 641.59	Prop WSE 639.93 639.77 639.71 639.71 639.71 639.71 639.71 639.71 639.71 639.73 639.74 500-Year Prop WSE 641.60 641.63 641.62	0.08 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Exist - Nat 0.30 0.30 0.31 0.31	0.09 0.15 0.19 0.21 0.22 0.22 0.22 0.10 Prop - Nat 0.33 0.33 0.34 0.34	0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00



MAJOR CULVERT (WC # 20) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 7' X 5'	Computed by: MRK	Date:	6/27/2017
Section:		S.N. Prop:	RCBC 7' X 5'			
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by: KS	Date:	6/27/2017
Station:	1338+54					

Drainage Area =	0.0235 sq. mi (150.43 acres)			kisting Overtopp	oing Elevation:	648.20	ft. @ Sta.	1336+92	
-			Pro	posed Overtop	ping Elevation:	649.1	ft. @ Sta.	1337+00	
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater E	Elev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	55	3	3	640.2	1.6	1.6	641.8	641.8
Design	50	83	4	4	640.4	1.6	1.6	642.1	642.1
Base	100	100	5	5	640.5	1.9	1.9	642.4	642.4
OVT(E)	> 500 - Yr								
OVT(P)	> 500 - Yr								
Max. Calc.	500	175	23	23	643.1	0.9	0.9	643.9	643.9
					10-Year Veloc	ity through Ex	isting Culvert =	6.31	fps

10-Year Velocity through Existing Cuivert = 10-Year Velocity through Proposed Cuivert =

6.31 fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: 643.3 (October 1954)

SCOPE OF WORK:

EXISTING CUL	/ERT	PROPOSED CU	_VERT
Bridge or Culvert Type:	Concrete Box Culvert	Culvert Type: C	concrete Box Culvert
Cell Dimensions (W x H):	7' (W) x 5' (H)	Cell Dimensions (W x H): 7	' (W) x 5' (H)
# of span \ cells:	1	# of span \ cells:	1
Length:	388'	Length:	388'
U/S Flowline:	639.83	U/S Flowline:	639.83
D/S Flowline:	637.50	D/S Flowline:	637.50
Skew:	no	Skew:	no
Low EOP:	648.20	Low EOP:	649.1
EXISTING DROPBOX		PROPOSED DR	OPBOX
Dimensions:	n/a	Dimensions:	n/a
Drop:	n/a	Drop:	n/a
Weir Elevation:	n/a	Weir Elevation:	n/a

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS

Box Culvert (7' x 5') under I-294 (@Station 1338+54)

MRK

KS

Computed by:

Checked by:

6/27/2017

6/27/2017

Date:

Date:

Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 7' X 5'	
Section:		S.N. Prop:	RCBC 7' X 5'	
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek	
Station	1338+54			

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head Elev. (ft)	
	Year	U/S Face of structure/Approach section Sta. 469		U/S Face of Structure	Existing Proposed	
	10	640.21	641.81	641.81	1.60	1.60
Design	50	640.40	642.05	642.05	1.65	1.65
Base	100	640.50	642.35	642.35	1.85	1.85
Max. Calc.	500	643.08	643.94	643.94	0.86	0.86

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This meth od of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	vation (ft)	Low Beam Ele	evation (ft)	Freq.	Headwate	er Elev. (ft)	Freebo	oard (ft)	Cleara	nce (ft)
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
648.20	649.1	NA	NA	10	641.81	641.81	6.39	7.29	NA	NA
Low Road S	Station:	Low Beam	Station:	50	642.05	642.05	6.15	7.05	NA	NA
Existing	Proposed	Existing	Proposed	100	642.35	642.35	5.85	6.75	NA	NA
1336+92	1337+00	NA	NA	500	643.94	643.94	4.26	5.16	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing @ 469	Proposed @ 469	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	640.21	640.21	639.83	639.83	0.38	0.38	7' (W) x 5' (H)	7' (W) x 5' (H)	2.66	2.66
Design	50	640.40	640.40	639.83	639.83	0.57	0.57	7' (W) x 5' (H)	7' (W) x 5' (H)	3.99	3.99
Base	100	640.50	640.50	639.83	639.83	0.67	0.67	7' (W) x 5' (H)	7' (W) x 5' (H)	4.69	4.69
Max. Calc.	500	643.08	643.08	639.83	639.83	3.25	3.25	7' (W) x 5' (H)	7' (W) x 5' (H)	22.75	22.75

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.



MAJOR CULVERT (WC # 21) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	
Section:		
County:	Cook	
Station:	1386+54	

S.N. Exist:	RCBC 8' X 8'	Computed by: MRK	Date:	6/27/2017
S.N. Prop:	RCBC 8' X 8'			
Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by: KS	Date:	6/27/2017

Drainage Area =	0.72 sq. mi		E>	isting Overtop	ping Elevation:	646.93	ft. @ Sta.	1388+00	
-			Pro	posed Overto	pping Elevation:	646.97	ft. @ Sta.	1385+50	
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater E	Elev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	157	44	44	639.7	0.0	0.0	639.4	639.4
Design	50	238	61	61	641.8	0.0	0.0	641.8	641.7
Base	100	284	64	64	642.8	0.4	0.4	643.2	643.2
OVT (E)	> 500 - Yr								
OVT (P)	> 500 - Yr								
Max. Calc.	500	486	64	64	644.9	1.2	1.2	646.1	646.1
					10-Year Veloc	ity through Ex	isting Culvert =	3.8	fps
					10-Year Velocit	y through Prop	osed Culvert =	3.8	fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: 644.1 (October 1954)

SCOPE OF WORK:

EXISTING CULVE	RT	PROPOSED CULV	/ERT
Bridge or Culvert Type: Co	oncrete Box Culvert	Culvert Type: Cor	ncrete Box Culvert (extension)
Cell Dimensions (W x H): 8'	(W) x 8' (H)	Cell Dimensions (W x H): 8' (W) x 8' (H)
# of span \ cells:	1	# of span \ cells:	1
Length:	287'	Length:	313'
U/S Flowline:	634.14	U/S Flowline:	634.20
D/S Flowline:	633.18	D/S Flowline:	633.18
Skew:	no	Skew:	no
Low EOP:	646.93	Low EOP:	646.97
EXISTING DROPBOX		PROPOSED DROPE	BOX
Dimensions:	n/a	Dimensions:	n/a
Drop:	n/a	Drop:	n/a
Weir Elevation:	n/a	Weir Elevation:	n/a

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS

Box Culvert (8' x 8') under I-294 (@Station 1386+54)

Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 8' X 8'
Section:		S.N. Prop:	RCBC 8' X 8'
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek
Station:	1386+54		

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head Elev. (ft)		
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	639.65	639.44	639.39	0.00	0.00	
Design	50	641.78	641.77	641.67	0.00	0.00	
Base	100	642.82	643.24	643.18	0.42	0.36	
Max. Calc.	500	644.91	646.07	646.11	1.16	1.20	

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This m ethod of calculating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Ele	evation (ft)	n (ft) Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
646.93	646.97	NA	NA	10	639.44	639.39	7.49	7.58	NA	NA
Low Road	Station:	Low Bear	n Station:	50	641.77	641.67	5.16	5.30	NA	NA
Existing	Proposed	Existing	Proposed	100	643.24	643.18	3.69	3.79	NA	NA
1388+00	1385+50	NA	NA	500	646.07	646.11	0.86	0.86	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing @ 802	Proposed @ 829	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	639.65	639.65	634.14	634.2	5.51	5.45	8' (W) x 8' (H)	8' (W) x 8' (H)	44.08	43.60
Design	50	641.78	641.78	634.14	634.2	7.64	7.58	8' (W) x 8' (H)	8' (W) x 8' (H)	61.12	60.64
Base	100	642.82	642.82	634.14	634.2	8.68	8.62	8' (W) x 8' (H)	8' (W) x 8' (H)	64.00	64.00
Max. Calc.	500	644.91	644.91	634.14	634.2	10.77	10.71	8' (W) x 8' (H)	8' (W) x 8' (H)	64.00	64.00

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.







MAJOR CULVERT (CREEK DRIVE CULVERT) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294
Section:	
County:	Cook
Station:	1386+54, 425' RT

S.N. Exist:	CMP_ARCH 7.33' X 11.6'	Computed by: <u>SB</u>	Date:	6/27/2017
S.N. Prop:	RCBC 12' X 6'			
Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by: KS	Date:	6/27/2017

Drainage Area =	0.72 sq. mi		Existing Overtopping Elevation:			641.78	ft. @ Sta.			
-			Proposed Overtopping Elevation:			641.78	ft. @ Sta.			
Flood	Frequency	Discharge	Waterway O	Waterway Opening (sq. ft) Natural		Head (ft)		Headwater E	Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed	
Ten-Year	10	157	50	50	639.2	0.2	0.1	639.3	639.2	
Design	50	238	66	70	641.3	0.4	0.3	641.7	641.5	
Base	100	284	66	72	642.4	0.3	0.3	642.7	642.6	
OVT(E)	> 500 - Yr									
OVT (P)	> 500 - Yr									
Max. Calc.	500	486	66	72	644.4	0.1	0.1	644.4	644.4	
10-Year Velocity through Existing Culvert =							2.6	fps		

10-Year Velocity through Proposed Culvert =

2.2 fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: 644.1 (October 1954)

SCOPE OF WORK:

EXISTING CUL	/ERT	
Bridge or Culvert Type:	CMP Arch Culvert	
Cell Dimensions (W x H):	11.6' (W) x 7.33' (H)	
# of span \ cells:	1	
Length:	50'	
U/S Flowline:	632.87	
D/S Flowline:	632.86	
Skew:	no	
Low EOP:	641.78	
EXISTING DROP	BOX	
Dimensions:	n/a	
Drop:	n/a	
Weir Elevation:	n/a	

PROPOSED C	ULVERT
Culvert Type:	Concrete Box Culvert
Cell Dimensions (W x H):	12' (W) x 6' (H)
# of span \ cells:	1
Length:	50'
U/S Flowline:	632.87
D/S Flowline:	632.86
Skew:	no
Low EOP:	641.78
PROPOSED DR	OPBOX
Dimensions:	n/a

Drop: n/a Weir Elevation: n/a

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS (WC @ Creek Drive)





Route:	Creek Drive	S.N. Exist:	CMP_ARCH 7.33' X 11.6'	Computed by:	SB	Date:	6/27/2017
Section:		S.N. Prop:	RCBC 12' X 6'				
County:	Cook	Waterway:	Unnamed ditch tributary to Flagg Creek	Checked by:	KS	Date:	6/27/2017
Station:	1386+54, 425' RT						

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head Flev	
	Year	U/S Face of structure/Approach section Sta. 302	U/S Face of Structure	U/S Face of Structure	Existing	Proposed
	10	639.15	639.31	639.24	0.16	0.09
Design	50	641.29	641.65	641.54	0.36	0.25
Base	100	642.37	642.70	642.63	0.33	0.26
Max. Calc.	500	644.37	644.44	644.44	0.07	0.07

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This meth od of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Ele	levation (ft) Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeb	oard (ft)	Clearance (ft)		
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
641.78	641.78	NA	NA	10	639.31	639.24	2.47	2.54	NA	NA
Low Road	Station:	Low Bear	n Station:	50	641.65	641.54	0.13	0.24	NA	NA
Existing	Proposed	Existing	Proposed	100	642.70	642.63	-0.92	-0.85	NA	NA
-	-	NA	NA	500	644.44	644.44	-2.66	-2.66	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing @ 302	Proposed @ 302	Existing	Proposed	Existing	Proposed	Existing (Arch)	Proposed (Box)	Existing	Proposed
	10	639.15	639.18	632.87	632.87	6.28	6.31	11.6' (W) x 7.33' (H)	12' (W) x 6' (H)	50.24	50.48
Design	50	641.29	641.58	632.87	632.87	8.42	8.71	11.6' (W) x 7.33' (H)	12' (W) x 6' (H)	66.20	69.68
Base	100	642.37	642.62	632.87	632.87	9.50	9.75	11.6' (W) x 7.33' (H)	12' (W) x 6' (H)	66.20	72.00
Max. Calc.	500	644.37	644.41	632.87	632.87	11.50	11.54	11.6' (W) x 7.33' (H)	12' (W) x 6' (H)	66.20	72.00

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.

			10-Year			
	Natural	Exist	Prop	Exist - Nat	Prop - Nat	
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS
497	639.24	639.30	639.24	0.06	0.00	-0.06
412	639.27	639.34	639.28	0.07	0.01	-0.06
357	639.23	639.31	639.24	0.08	0.01	-0.07
302	639.15	639.23	639.16	0.08	0.01	-0.07
261/culvert						
			50-Year			
	Natural	Exist	Prop	Exist - Nat	Data Nat	
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS
497	641.33	641.59	641.48	0.26	0.15	-0.11
412	641.42	641.67	641.56	0.25	0.14	-0.11
357	641.39	641.65	641.54	0.26	0.15	-0.11
302	641.29	641.55	641.44	0.26	0.15	-0.11
261/culvert						
			100-Year	-		
	Natural	Exist	Prop	Eviat Nat	Dava Net	
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS
497	642.29	642.62	642.54	0.33	0.25	-0.08
412	642.40	642.72	642.64	0.32	0.24	-0.08
357	642.38	642.70	642.62	0.32	0.24	-0.08
302	642.37	642.70	642.62	0.33	0.25	-0.08
261/culvert						
			500-Year	-		
	Natural	Exist	Prop	Exist - Nat	Data Nat	
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS
497	644.17	644.22	644.22	0.05	0.05	0.00
412	644.40	644.45	644.45	0.05	0.05	0.00
357	644.38	644.44	644.43	0.06	0.05	-0.01
302	644.37	644.42	644.42	0.05	0.05	0.00
261/culvert						

WSEL Summary Table - Created Head Calculations- Creek Drive Culvert



BRIDGE (WC # 22) WATERWAY INFORMATION TABLE



fps

12/20/2017 12/20/2017

Route:	Tri-State Tollway (I-294)	S.N. Exist: BN 259 & BN 260	Computed by: KS	Date:
Section:		S.N. Prop: BN 259 & BN 260		
County:	Cook	Waterway: Flagg Creek	Checked by: SH	Date:
Station:	1405+00			

Drainage Area =	3.536 sq. mi		Existing Overto	opping Elevation	1:		646.48	@ Sta.	1407+50	
-			Proposed Ove	rtopping Elevati	on:		645.94	@ Sta.	1401+00	
Flood Event	Frequency	Discharge	Waterway Op	pening (sq. ft)	Natural	Hea	Head (ft)		Headwater Elev. (ft)	
	Year	(cfs)	Existing	Existing Proposed H.W.E.		Existing	Proposed	Existing	Proposed	
	10	302.0	281.28	279.51	639.06	0.03	0.00	639.09	639.06	
Design	50	520.0	454.09	445.71	641.51	0.02	0.03	641.53	641.54	
Base	100	640.0	550.09	519.20	642.59	0.09	0.02	642.68	642.61	
Scour Design Check										
Overtop Existing	> 500 - Yr									
Overtop Proposed	> 500 - Yr									
Max. Calc.	500	945.0	745.86	649.47	644.50	0.01	0.03	644.51	644.53	
10-Year Velocity through Existing Bridge =						1.15	fps			

10-Year Velocity through Proposed Bridge = 1.08

DATUM:	NAVD 88
ALL-TIME H.W.E. & DATE:	645.51 (October 1954)

SCOPE OF WORK:

EXISTING STRUCTU	RE	PROPOSED STRUCTU	JRE
TYPE:	3-span 36" PCC girder bridge	TYPE: -	Single-span 27" PCC girder bridge
LENGTH:	121' (face to face abutments along the girder)	LENGTH: -	70' (face to face abutments along the girder)
# SPANS:	3	# SPANS: -	1
LOW BEAM:	642.50	LOW BEAM: -	643.79
SKEW:	45°	SKEW: -	45°
LOW EOP:	646.48	LOW EOP: -	645.94

NOTES:

- Existing bridge does meet Tollway's freeboard critera but not the clearance criteria.

- Proposed bridge does meet Tollway's freeboard and clearance criteria.

- Proposed Structure (Alternative 8R) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS I-294 Bridge over the Flagg Creek (@Station 1405+00)



Route:	Tri-State Tollway (I-294)	S.N. Exist:	BN 259 (IDOT SN 016-9813) & BN 260 (IDOT SN 016-9812)	Computed by
Section:		S.N. Prop:	BN 259 (IDOT SN 016-9813) & BN 260 (IDOT SN 016-9812)	
County:	Cook	Waterway:	Flagg Creek	Checked by:
Station:	1405+00			

Created Head Calculations

Flood	Freq.	Natural	H.W.E. (ft)	Existing H	leadwater Elev. (ft)	Proposed Headwater Elev. (ft)		Created Head (ft) @ Approach Section	
	Year	U/S Face of Structure @ 38526	Approach section U/S @ 38642.07	U/S Face of Structure @ 38526	Approach section U/S @ 38642.07	U/S Face of Structure @ 38526	Approach section U/S @ 38642.07	Existing	Proposed
	10	639.06	639.02	639.09	639.05	639.06	639.02	0.03	0.00
Design	50	641.51	641.49	641.53	641.51	641.54	641.52	0.02	0.03
Base	100	642.59	642.57	642.68	642.66	642.61	642.59	0.09	0.02
Max. Calc.	500	644.50	644.47	644.51	644.48	644.53	644.50	0.01	0.03

(1) The natural highwater elevation is the water surface elevation at the upstream end of the crossing, as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the approach section, and not at the U/S face of the bridge/culvert. The difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head.

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freebo	ard (ft)	Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
646.48	645.94	642.50	643.68	10	639.09	639.06	7.39	6.88	3.44	4.62
Low Road S	Low Road Station: Low Beam Station:		50	641.53	641.54	4.95	4.40	0.99	2.17	
Existing	Proposed	Existing	Proposed	100	642.68	642.61	3.80	3.33	-0.09	1.09
1407+50	1401+00	1405+00	1405+00	500	644.51	644.53	1.97	1.41	-2.00	-0.82

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) @ U/S Face of Structure		Stream Bottom Elev.		Depth of Water		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	639.06	639.06	632.00	632.00	7.06	7.06	281.28	279.51
Design	50	641.51	641.51	632.00	632.00	9.51	9.51	454.09	445.71
Base	100	642.59	642.59	632.00	632.00	10.59	10.59	550.09	519.20
Max. Calc.	500	644.50	644.50	632.00	632.00	12.50	12.50	745.86	649.47

Bottom width (ft) 45 Full flow (sq ft) 745 (Existing Bridge Open Area) Full flow (sq ft)

649 (Proposed Bridge Open Area)

(6) The waterway opening area is computed using the NHWE at the U/S face of the culvert, and not the headwater elevation. The maximum opening area should be less or equal to the cross sectional area of the box culvert or circular/elliptical pipe. If the culvert is embedded to meet permit requirements, the embedded depth should not be included in the opening area calculations.

WSEL Summary Table - Created Head Calculations WC22

	10-Year											
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - EX						
X-sect	WSE	WSE	WSE			WSE						
38785.00	639.20	639.22	639.16	0.02	-0.04	-0.06						
38726.00	639.19	639.21	639.18	0.02	-0.01	-0.03						
38689.80	639.18	639.20	639.18	0.02	0.00	-0.02						
38642.07	639.02	639.05	639.02	0.03	0.00	-0.03						
38526.00	639.06	639.08	639.05	0.02	-0.01	-0.03						
38355/Bridge												

	50-Year											
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - EX						
X-sect	WSE	WSE	WSE			WSE						
38785.00	641.62	641.64	641.55	0.02	-0.07	-0.09						
38726.00	641.61	641.63	641.59	0.02	-0.02	-0.04						
38689.80	641.60	641.62	641.59	0.02	-0.01	-0.03						
38642.07	641.49	641.51	641.52	0.02	0.03	0.01						
38526.00	641.51	641.54	641.52	0.03	0.01	-0.02						
38355/Bridge												

100-Year									
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - EX			
X-sect	WSE	WSE	WSE			WSE			
38785.00	642.69	642.77	642.60	0.08	-0.09	-0.17			
38726.00	642.68	642.76	642.65	0.08	-0.03	-0.11			
38689.80	642.67	642.76	642.65	0.09	-0.02	-0.11			
38642.07	642.57	642.66	642.59	0.09	0.02	-0.07			
38526.00	642.59	642.68	642.59	0.09	0.00	-0.09			
38355/Bridge									

500-Year									
	Natural	Exist	Prop (No Pier, Single Span)	Exist - Nat	Prop - Nat	PR WSE - EX			
X-sect	WSE	WSE	WSE			WSE			
38785.00	644.59	644.61	644.45	0.02	-0.14	-0.16			
38726.00	644.58	644.60	644.54	0.02	-0.04	-0.06			
38689.80	644.57	644.59	644.54	0.02	-0.03	-0.05			
38642.07	644.47	644.48	644.50	0.01	0.03	0.02			
38526.00	644.50	644.51	644.49	0.01	-0.01	-0.02			
38355/Bridge									



MAJOR CULVERT (WC # 23) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)
Section:	
County:	Cook
Station:	1410+80

S.N. Exist:	RCBC 6' W X 5' H
S.N. Prop:	RCBC 14' W X 6' H (with 1' of Embedment)
Waterway:	Western Spring Ditch (Tributary to Flagg Creek)

	Computed by:	KS	Date:	12/14/2017
)				
reek)	Checked by:	SH	Date:	12/14/2017

Drainage Area =	0.251 sq. mi	(160.6 acres)	(160.6 acres) Existing Overtopping Elevation:		646.62	ft. @ Sta.	1410+85			
-			Pro	posed Overtop	ping Elevation:	645.59	ft. @ Sta.	1409+94		
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	Head (ft)		Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed	
Ten-Year	10	145	15	51	640.4	0.2	0.0	640.5	639.9	
Design	50	265	28	70	642.5	0.3	0.0	642.8	642.2	
Base	100	317	30	70	643.6	0.9	0.0	644.5	643.4	
OVT(E)	> 500 - Yr									
OVT(P)	< 500 - Yr									
Max. Calc.	500	540	30	70	646.1	1.0	0.0	647.1	645.4	
	10-Year Velocity through Existing Culvert =					6.4	fps			

10-Year Velocity through Proposed Culvert =

6.4 fps 2.1 fps

OVT = Overtopping Event

(E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: TBD

SCOPE OF WORK:

EXISTING CULVERT							
Bridge or Culvert Type: Reinforced Concrete Box Culvert							
Cell Dimensions (W x H):	6' (W) x 5' (H)						
# of span \ cells:	1						
Length:	165'						
U/S Flowline:	637.22						
D/S Flowline:	636.63						
Skew:	no						
Low EOP:	646.62						

EXISTING	DROPBOX

Dimensions:	n/a
Drop:	n/a
Weir Elevation:	n/a

PROPOSED CU	JLVERI		
Culvert Type:	Reinforc	ed Concrete Box Culvert	
Cell Dimensions (W x H):	14' (W) >	(6' (H) with 1.0' of Embed	ment
# of span \ cells:		1	
Length:		225'	
U/S Flowline:	636.72	(Invert = 635.72)	
D/S Flowline:	635.96	(Invert = 634.96)	
Skew:		no	
Low EOP:	6	645.59	
PROPOSED DR	ROPBOX	<	
Dimensions:		n/a	

Dimensions:	n/a
Drop:	n/a
Weir Elevation:	n/a

NOTES: Proposed Structure (Alt 8R) Details are preliminary. Subject to Refinement in TSL stage.

WATERWAY INFORMATION TABLE BACK-UP CACULATIONS (WC # 23) Box Culvert (6' x 5') under I-294 (@Station 1410+80)

*exp				
I	Computed by:	KS	Date:	12/14/2017
	Checked by:	SH	Date:	12/14/2017

Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCBC 6' W X 5' H
Section:		S.N. Prop:	RCBC 14' W X 6' H (with 1' of Embedment)
County:	Cook	Waterway:	Western Spring Ditch (Tributary to Flagg Creek)
Station:	1410+80		

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head Elev. (ft)	
	Year	U/S Face of structure/Approach section Sta. 5000	U/S Face of Structure	U/S Face of Structure	Existing	Proposed
	10	640.35	640.51	639.87	0.16	0.00
Design	50	642.49	642.83	642.19	0.34	0.00
Base	100	643.59	644.46	643.42	0.87	0.00
Max. Calc.	500	646.09	647.07	645.36	0.98	0.00

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	vation (ft)	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
646.62	645.59	NA	NA	10	640.51	639.87	6.11	5.72	NA	NA
Low Road S	Station:	Low B	eam Station:	50	642.83	642.19	3.79	3.40	NA	NA
Existing	Proposed	Existing	Proposed	100	644.46	643.42	2.16	2.17	NA	NA
1410+85	1409+94	NA	NA	500	647.07	645.36	-0.45	0.23	NA	NA

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50-year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50-year natural high-water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing @ 4969	Proposed @ 5000	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	639.72	640.35	637.22	636.72	2.50	3.63	6' (W) x 5' (H)	14' (W) x 6' (H)	15.00	50.82
Design	50	641.85	642.49	637.22	636.72	4.63	5.77	6' (W) x 5' (H)	14' (W) x 6' (H)	27.78	70.00
Base	100	642.99	643.59	637.22	636.72	5.77	6.87	6' (W) x 5' (H)	14' (W) x 6' (H)	30.00	70.00
Max. Calc.	500	646.12	646.09	637.22	636.72	8.90	9.37	6' (W) x 5' (H)	14' (W) x 6' (H)	30.00	70.00

WSEL Summary Table - Created Head Calculations WC23

			10-Year				
	Natural	Exist	Prop	Exist - Nat	Prop - Nat	PR WSE - EX WSE	
X-sect	WSE	WSE	WSE	Exist - Nat	riop - Nat		
5039	640.72	640.72	640.72	0.00	0.00	0.00	
5000	640.35	640.51	639.87	0.16	-0.48	-0.64	
4959/culvert							
		·	50-Year		-	•	
	Natural	Exist	Prop	Exist - Nat	Duen Net		
X-sect	WSE	WSE	WSE	EXIST - INAL	Prop - Nat	PR WSE - EX WS	
5039	642.47	642.81	642.12	0.34	-0.35	-0.69	
5000	642.49	642.83	642.19	0.34	-0.30	-0.64	
4959/culvert							
			100-Year				
	Natural	Exist	Prop	Exist - Nat	Dueu Net		
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS	
5039	643.59	644.46	643.42	0.87	-0.17	-1.04	
5000	643.59	644.46	643.42	0.87	-0.17	-1.04	
4959/culvert							
			500-Year				
	Natural	Exist	Prop	Eviat Nat	Duen Net		
X-sect	WSE	WSE	WSE	Exist - Nat	Prop - Nat	PR WSE - EX WS	
5039	646.09	647.06	645.44	0.97	-0.65	-1.62	
5000	646.09	647.07	645.36	0.98	-0.73	-1.71	
4959/culvert							



BRIDGE (WC # 25) WATERWAY INFORMATION TABLE

Route: Section: County: Station:

Tri-State Tollway (I-294) 4223 Dupage 1492+50

BN 267 & BN 268 S.N. Exist: S.N. Prop: TBD Salt Creek Waterway:

Computed by:

Checked by:

Drainage Area =	114 sq. mi		E	xisting Overtopp	ing Elevation:	645.36	ft @ Sta.	1471+00	
			Pre	oposed Overtop	ping Elevation:	647.84	ft @ Sta.	1476+50.51	
Flood Event	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	d (ft)	Headwater	Elev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
	10	2903	634.40	755.40	640.17	0.22	0.09	640.39	640.26
Design	50	4193	777.00	901.50	641.32	0.46	0.40	641.78	641.72
Base	100	4782	804.50	929.40	641.54	0.60	0.55	642.14	642.09
Scour Design Check	200								
Overtop Existing	> 500 - Yr	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
Overtop Proposed	> 500 - Yr	n/a	n/a	n/a	n/a	n/a	n/a	n/a	n/a
Max. Calc.	500	6230	915.90	1038.60	642.40	0.91	0.88	643.31	643.28
					10-Year Vel	ocity through E	xisting Bridge =	3.00	fps
					10-Year Veloo	city through Pro	posed Bridge =	3.00	fps

DATUM: ALL-TIME H.W.E. & DATE:

SCOPE OF WORK:

)RK:					
	EXISTING STRUC	TURE			
	TYPE: 3	-Span PCC (Girder Bridge		
	LENGTH:	155'	-		
	# SPANS:	3			
	LOW BEAM:	645.56			
	SKEW: 0	(relative to r	oad)		
	LOW EOP:	645.15			

NOTES: Proposed structure are preliminary; subject to refinement in TSL stage. Model From 2IM Group

From 2IM Group

Date:	11/17/2017

Date: 11/17/2014

PROPOSED STRUCTURE TYPE: Single Span LENGTH: 130' # SPANS: 1 LOW BEAM: 645.20 SKEW: 0 (relative to road) LOW EOP: 647.84



MAJOR CULVERT (WC # 24) WATERWAY INFORMATION TABLE



EXPERIENCE | Transportation

12/21/2017

12/21/2017

Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCP 60"	Computed by:	EL	Date:
Section:	4223	S.N. Prop:	RCP 60"			-
County:	Cook	Waterway:	Tributary Ditch to Salt Creek	Checked by:	JC	Date:
Station:	1464+55					-

Drainage Area =	0.490 sq. r	ni	E	Existing Overtop	ping Elevation:	644.40	ft. @ Sta.	1476+72	
-	-		Pi	oposed Overtop	ping Elevation:	644.42	ft. @ Sta.	1479+00	
Flood	Frequency	Discharge	Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater E	lev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.*	Existing	Proposed	Existing	Proposed
Ten-Year	10	100.0	19.63	19.63	644.98	0.00	0.00	644.98	644.98
Design	50	139.0	19.63	19.63	644.98	0.33	0.33	645.31	645.31
Base	100	155.0	19.63	19.63	644.98	0.82	0.82	645.80	645.80
OVT(E)	10	100.0	19.63	19.63	644.98	0.00	-	644.98	-
OVT(P)	> 500 - Yr	-	-	-	-	-	-	-	-
Max. Calc.	500	190.0	19.63	19.63	644.98	1.33	2.10	646.31	647.08
					10-Year Velo	city through Ex	kisting Culvert =	5.12	fps
					10 Veer Velee	ity through Droy	accord Culvert	E 10	fnc

10-Year Velocity through Proposed Culvert =

5.12 fps

OVT = Overtopping Event (E) Existing (P) Proposed

*Natural HWE = 643.26+0.006*287 = 644.98 (where 643.26=10YR WSE in Salt Creek

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A

SCOPE OF WORK: EXISTING CULVI	ERT				
Bridge or Culvert Type: 60" RCP					
Cell Dimensions (W x H):					
# of span \ cells:	1				
Length:	287				
U/S Flowline:	635.77				
D/S Flowline:	634.06				
Skew:	30 degrees				
Low EOP: 6	644.40 @ 1476+72 (NB Side)				
EXISTING DROPB	OX				
Dimensions:					
Drop:					
Weir Elevation:					

PROPOSED CL	JLVERT
Culvert Type:	60" RCP
Cell Dimensions (W x H):	
# of span \ cells:	1
Length:	287
U/S Flowline:	635.77
D/S Flowline:	634.06
Skew:	30 degrees
Low EOP:	647.71 @ 1458+86 (SB Side)
PROPOSED DRO Dimensions:	DPBOX
Dimensions: Drop:	
Weir Elevation:	

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

Circular Culvert (60") under I-294 (@Station 1464+55)

Tran Sys	tems>			
EXPERIENCE Tra	sportation			
Computed by:	EL	Date:	12/21/2017	
Checked by:	JC	Date:	12/21/2017	

Route:	Tri-State Tollway (I-294)	S.N. Exist: RCP 60"
Section:	4223	S.N. Prop: RCP 60"
County:	Cook	Waterway: Tributary Ditch to Salt Creek
Station:	1464+55	

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head (ft) Section	
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed
	10	644.98	644.98	644.98	0.00	0.00
Design	50	644.98	645.31	645.31	0.33	0.33
Base	100	644.98	645.80	645.80	0.82	0.82
Max. Calc.	500	644.98	646.31	647.08	1.33	2.10

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam I	Elevation (ft)	Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
644.40	647.71			10	644.98	644.98	-0.58	2.73		
Low Road S	Station:	Low Bear	n Station:	50	645.31	645.31	-0.91	2.40		
Existing	Proposed	Existing	Proposed	100	645.80	645.80	-1.40	1.91		
1476+72	1458+86			500	646.31	647.08	-1.91	0.63		

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50 year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50 year natural high water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	644.98	644.98	635.77	635.77	9.21	9.21			19.63	19.63
Design	50	644.98	644.98	635.77	635.77	9.21	9.21			19.63	19.63
Base	100	644.98	644.98	635.77	635.77	9.21	9.21			19.63	19.63
Max. Calc.	500	644.98	644.98	635.77	635.77	9.21	9.21			19.63	19.63



MAJOR CULVERT (WC # 26) WATERWAY INFORMATION TABLE



EXPERIENCE | Transportation

Date:

Date:

7/15/2017

7/18/2017

Route:	Tri-State Tollway (I-294)	S.N. Exist:	CMP 54"/BCCMP 44" Liner
Section:	4223	S.N. Prop:	RCP 54"
County:	Cook	Waterway:	Box Culvert that drains to Outlet 28A-2
Station:	1532+05		

Drainage Area =	0.0773 sq.	mi	E	Existing Overtopping Elevation:			ft. @ Sta.	1526+00	
-	49.46	ac	Pi	roposed Overtop	pping Elevation:	670.49	ft. @ Sta.	1526+00	
Flood	Frequency Discharge		Waterway O	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.	Existing	Proposed	Existing	Proposed
Ten-Year	10	17.9	2.17	2.45	662.85	0.81	0.68	663.66	663.53
Design	50	41.3	3.96	4.51	663.37	1.40	1.15	664.77	664.52
Base	100	56.4	4.94	5.68	663.64	1.80	1.44	665.44	665.08
OVT(E)	> 500 - Yr	-	-	-	-	-	-	-	-
OVT(P)	> 500 - Yr	-	-	-	-	-	-	-	-
Max. Calc.	500	65.5	5.53	6.38	663.80	2.06	1.59	665.86	665.39
					10-Year Velo	city through Ex	kisting Culvert =	6.03	fps
					10-Year Veloc	ity through Prop	bosed Culvert =	5.92	fps

OVT = Overtopping Event (E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A

*Shorter length in proposed conditions as it will tie-in to proposed box culvert on NB side.

Computed by: EL

Checked by: JC

SCOPE OF WORK:

EXISTING CUL	/ERT	PROPOSED CU	LVERT
Bridge or Culvert Type:	CMP 54"/ 44" BCCMP Liner	Culvert Type:	54" RCP
Cell Dimensions (W x H):		Cell Dimensions (W x H):	
# of span \ cells:	1	# of span \ cells:	1
Length:	250	Length:	225*
U/S Flowline:	661.90	U/S Flowline:	661.90
D/S Flowline:	660.06	D/S Flowline:	660.24
Skew:	0	Skew:	0
Low EOP:	671.44 @ 1526+00 (NB Side)	Low EOP:	670.49 @ 1526+00 (NB Side)
EXISTING DROP	BOX	PROPOSED DRO	PBOX
Dimensions:		Dimensions:	
Drop:		Drop:	
Weir Elevation:		Weir Elevation:	

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

Circular Culvert (44") under I-294 (@Station 1532+05)

TranSys	tems>
EXPERIENCE Tran	sportation
Computed by:	EL

Date: 7/15/2017

Checked by:

Date:

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Proposed Elev. (ft) Headwater Elev. (ft)		Created Head (ft) @ Approach Section		
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	662.85	663.66	663.53	0.81	0.68	
Design	50	663.37	664.77	664.52	1.40	1.15	
Base	100	663.64	665.44	665.08	1.80	1.44	
Max. Calc.	500	663.80	665.86	665.39	2.06	1.59	

S.N. Prop: RCP 54"

S.N. Exist: CMP 54"/ BCCMP 44" Liner

Waterway: Box Culvert that drains to Outlet 28A-2

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam I	Elevation (ft)	Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
671.44	670.49			10	663.66	663.53	7.78	6.96		
Low Road S	station:	Low Bear	m Station:	50	664.77	664.52	6.67	5.97		
Existing	Proposed	Existing	Proposed	100	665.44	665.08	6.00	5.41		
1526+00	1526+00			500	665.86	665.39	5.58	5.10		

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

Tri-State Tollway (I-294)

4223

Cook

1532+05

Route:

Section:

County:

Station:

(4) Freeboard is calculated from the 50 year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50 year natural high water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	662.85	662.85	661.90	661.90	0.95	0.95			2.17	2.45
Design	50	663.37	663.37	661.90	661.90	1.47	1.47			3.96	4.51
Base	100	663.64	663.64	661.90	661.90	1.74	1.74			4.94	5.68
Max. Calc.	500	663.80	663.80	661.90	661.90	1.90	1.90			5.53	6.38







1.70 fps

Route:	Tri-State Tollway (I-294)	S.N. Exist:	RCP 42"	Computed by: E	L Date:	7/19/2017
Section:	4223	S.N. Prop:	RCP 42"			
County:	Cook	Waterway:	Box Culvert that Drains to 28A-2	Checked by:	C Date:	7/20/2017
Station:	1553+70					

Drainage Area =	0.0307 sq.	mi	E	xisting Overtop	oing Elevation:	668.50	ft. @ Sta.	1557+00	
	19.64 ac		Pro	oposed Overtop	ping Elevation:	668.50	ft. @ Sta.	1557+00	
Flood	Frequency Discharge		Waterway Op	pening (sq. ft)	Natural	Hea	ad (ft)	Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.*	Existing	Proposed	Existing	Proposed
Ten-Year	10	1.11	0.20	0.20	660.69	3.52	0.12	664.21	660.81
Design	50	13.84	0.92	0.92	661.03	5.89	1.39	666.92	662.42
Base	100	23.26	3.59	3.59	661.90	5.39	1.13	667.29	663.03
OVT(E)	> 500 - Yr	-	-	-	-	-	-	-	-
OVT(P)	> 500 - Yr	-	-	-	-	-	-	-	-
Max. Calc.	500 32.11 9.62 9.62		9.62	664.46	3.16	0.14	667.62	664.60	
					10-Year Velo	city through Ex	isting Culvert =	0.12	fps

10-Year Velocity through Existing Culvert =

10-Year Velocity through Proposed Culvert =

OVT = Overtopping Event (E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A

*For WC #27, natural headwater taken as WSE at node 159+02_42infromWestPond from SWMM model projected up slope of WC # 27 pipe (proposed model from Cermak Interchange Flood Impact Reduction project - tailwater condition relieved with proposed model). The existing condition tailwater was taken from Node 7R in the existing conditions SWMM model. The 9'x4' and 10'x4' culverts from the Cermak Interchange Flood Impact Reduction project are shown on the Proposed Drainage Plan and are to be constructed with this project and lowers the created head at WC # 27. Existing pipes to remain are to be televised to determine condition during Phase 2.

SCOPE OF WORK:			
EXISTING CUL	/ERT	PROPOSED CU	LVERT
Bridge or Culvert Type:	42" RCP	Culvert Type:	42" RCP
Cell Dimensions (W x H):		Cell Dimensions (W x H):	
# of span \ cells:	1	# of span \ cells:	1
Length:	214	Length:	217 (extend to prop box culvert)
U/S Flowline:	660.50	U/S Flowline:	660.50
D/S Flowline:	660.07	D/S Flowline:	660.06
Skew:	0	Skew:	0
Low EOP:	668.50 @ 1557+00 SB Side	Low EOP:	668.50 @ 1557+00 SB Side
EXISTING DROP	BOX	PROPOSED DRO	PBOX
Dimensions:		Dimensions:	
Drop:		Drop:	
Weir Elevation:		Weir Elevation:	

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

Circular Culvert (42") under I-294 (@Station 1553+70)

Tran Sys	tems>			
EXPERIENCE Tran Computed by:	sportation	Date:	7/19/2017	
Checked by:	JC	Date:	7/20/2017	

Route:	Tri-State Tollway (I-294)	S.N. Exist: RCP 42"
Section:	4223	S.N. Prop: RCP 42"
County:	Cook	Waterway: Box Culvert that Drains to 28A-2
Station:	1553+70	

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	.,	Created Head (ft) @ Approach Section	
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	660.69	664.21	660.81	3.52	0.12	
Design	50	661.03	666.92	662.42	5.89	1.39	
Base	100	661.90	667.29	663.03	5.39	1.13	
Max. Calc.	500	664.46	667.62	664.60	3.16	0.14	

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam I	Elevation (ft)	Freq.	Headwater	Elev. (ft)	Freebo	oard (ft)	Cleara	nce (ft)
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
668.50	668.5			10	664.21	660.81	4.29	7.69		
Low Road S	station:	Low Bear	n Station:	50	666.92	662.42	1.58	6.08		
Existing	Proposed	Existing	Proposed	100	667.29	663.03	1.21	5.47		
1557+00	1557+00			500	667.62	664.60	0.88	3.90		

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50 year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50 year natural high water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	660.69	660.69	660.50	660.50	0.19	0.19			0.20	0.20
Design	50	661.03	661.03	660.50	660.50	0.53	0.53			0.92	0.92
Base	100	661.90	661.90	660.50	660.50	1.40	1.40			3.59	3.59
Max. Calc.	500	664.46	664.46	660.50	660.50	3.96	3.96			9.62	9.62



MAJOR CULVERT (WC # 28) WATERWAY INFORMATION TABLE



Route:	Tri-State Tollway (I-294)	S.N. Exist:	_2-RCP 60"	Computed by: <u>EL</u>
Section:	4223	S.N. Prop:		
County:	Cook	Waterway:	NB I-294 Ditch	Checked by: JC
Station:	1563+63			

Drainage Area =	0.1224 sq. m	ni	Existing Overtopping Eleva			671.35	ft. @ Sta.	1562+84	
_	78.36	ac	Pro	posed Overto	oping Elevation:		ft. @ Sta.		
Flood	Frequency	Discharge	Waterway Op	pening (sq. ft)	Natural	Hea	id (ft)	Headwater E	lev. (ft)
	Year	(cfs)	Existing	Proposed	H.W.E.*	Existing	Proposed	Existing	Proposed
Ten-Year	10	83.3	23.47	-	666.39	0.03	-	666.42	-
Design	50	134.4	35.89	-	667.31	0.52	-	667.83	-
Base	100	174.9	39.27	-	667.90	1.27	-	669.17	-
OVT(E)	< 500 - Yr	-	-	-	-	-	-	-	-
OVT (P)	> 500 - Yr	-	-	-	-	-	-	-	-
Max. Calc.	500	218.4	39.27	-	668.37	2.22	-	670.59	-
					10-Year Velo	city through Ex	isting Culvert =	3.51	fps
					10-Year Velocit	y through Prop	osed Culvert =		fps

OVT = Overtopping Event (E) Existing (P) Proposed

DATUM:	NAVD 88	
ALL-TIME	H.W.E. & DATE:	N/A

*For WC #28 and #29, natural headwater taken as WSE at node J11 from SWMM model projected up slope of WC # 29 pipe. WC#28 natural headwater calculated by continuing natural headwater from WC#29 up slope of WC#28 pipe. The existing condition assumes that the 9' x 4' box culvert from the Cermak Interchange Flood Impact Reduction project downstream is in place. The 9'x4' and 10'x4' culverts from the Cermak Interchange Flood Impact Reduction project are shown on the Proposed Drainage Plan and are to be constructed with this project. Existing pipes to remain are to be televised to determine condition during Phase 2.

SCOPE OF WORK:						
EXISTING CULVERT						
Bridge or Culvert Type:	2-60" RCP					
Cell Dimensions (W x H):						
# of span \ cells:	2					
Length:	268					
U/S Flowline:	663.54, 663.53					
D/S Flowline:	663.05, 662.88					
Skew:	0					
Low EOP:	671.35 @ 1562+84					
EXISTING DROP Dimensions: Drop: Weir Elevation:	30X					

PROPOSED CULVERT Culvert Type: Cell Dimensions (W x H): # of span \ cells: Length: U/S Flowline: D/S Flowline: Skew: Low EOP:

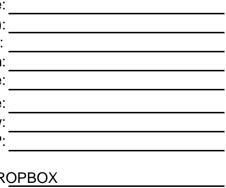
> PROPOSED DROPBOX Dimensions: Drop: Weir Elevation:

NOTES:

Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.



Date:	7/16/2017
Date:	7/18/2017



Circular Culvert (2 - 60") under I-294 (@Station 1563+63)

Route:	Tri-State Tollway (I-294)	S.N. Exist: RCP 2-60"
Section:	4223	S.N. Prop: RCP 2-60"
County:	Cook	Waterway: NB I-294 Ditch
Station:	1563+63	

Tran Sys	tems>		
EXPERIENCE Tran Computed by:	sportation	Date:	7/17/2017
Checked by:	JC	Date:	7/18/2017

Created Head Calculations

Flood	Freq. Natural H.W.E. (ft)		Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head (ft) @ Approach Section		
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed	
	10	666.39	666.42		0.03		
Design	50	667.31	667.83		0.52		
Base	100	667.90	669.17		1.27		
Max. Calc.	500	668.37	670.59		2.22		

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freeboard (ft)		Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
671.35				10	666.42		4.93			
Low Road S	station:	Low Bear	Low Beam Station:		667.83		3.52			
Existing	Proposed	Existing	Proposed	100	669.17		2.18			
1562+84				500	670.59		0.76			

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50 year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50 year natural high water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	666.39		663.53		2.86				23.47	
Design	50	667.31		663.53		3.78				35.89	
Base	100	667.90		663.53		4.37				39.27	
Max. Calc.	500	668.37		663.53		4.84				39.27	



MAJOR CULVERT (WC # 29) WATERWAY INFORMATION TABLE



fps

Route:	Tri-State Tollway (I-294)	S.N. Exist:	60" Lined 24", 60" Lined 38", & 48" RCP	Computed by: EL	Date:	7/17/2017
Section:	4223	S.N. Prop:				
County:	Cook	Waterway:	NB-I294 Ditch	Checked by: JC	Date:	7/18/2017
Station [.]	1562+30					

Drainage Area =	0.1668 sq.	. mi	E	xisting Overtop	oing Elevation:	671.60	ft. @ Sta.	1559+29	
	106.75	ac	Pre	Proposed Overtopping Elevation:			ft. @ Sta.		
Flood	Frequency	Discharge	Waterway O	Waterway Opening (sq. ft)		Head (ft)		Headwater Elev. (ft)	
	Year	(cfs)	Existing	Proposed	H.W.E.*	Existing	Proposed	Existing	Proposed
Ten-Year	10	116.6	22.86	-	666.05	0.21	-	666.26	-
Design	50	175.2	23.58	-	666.97	0.58	-	667.55	-
Base	100	212.0	23.58	-	667.56	1.12	-	668.68	-
OVT(E)	< 500 - Yr	-	-	-	-	-	-	-	-
OVT(P)	> 500 - Yr	-	-	-	-	-	-	-	-
Max. Calc.	500	250.2	23.58	-	667.46	2.41	-	669.87	-
	5.24	fps							

10-Year Velocity through Existing Culvert = 10-Year Velocity through Proposed Culvert =

OVT = Overtopping Event (E) Existing (P) Proposed

DATUM: NAVD 88 ALL-TIME H.W.E. & DATE: N/A *For WC #28 and #29, natural headwater taken as WSE at node J11 from SWMM model projected up slope of WC # 29 pipe. WC#28 natural headwater calculated by continuing natural headwater from WC#29 up slope of WC#28 pipe. The existing condition assumes that the 9' x 4' box culvert from the Cermak Interchange Flood Impact Reduction project downstream is in place. The 9'x4' and 10'x4' culverts from the Cermak Interchange Flood Impact Reduction project are shown on the Proposed Drainage Plan and are to be constructed with this project. Existing pipes to remain are to be televised to determine condition during Phase 2.

SCOPE OF WORK:

EXISTING CUL	/ERT	PROPOSED CULVERT	
Bridge or Culvert Type:	60" lined to 24", 60" lined to 38", 48"	Culvert Type:	
Cell Dimensions (W x H):		Cell Dimensions (W x H):	
# of span \ cells:	3	# of span \ cells:	
Length:	195	Length:	
U/S Flowline:	663.15, 663.17, 662.67	U/S Flowline:	_
D/S Flowline:	662.15, 661.84, 662.11	D/S Flowline:	
Skew	0	Skew:	
Low EOP:	671.60 @ 1559+29 ON RAMP B	Low EOP:	_
EXISTING DROP	BOX	PROPOSED DROPBOX	
Dimensions:		Dimensions:	
Drop:		Drop:	
Weir Elevation:		Weir Elevation:	

NOTES: Proposed Structure (Alt 8) Details are preliminary. Subject to Refinement in TSL stage.

Circular Culvert (24"/38"/48") under I-294 (@Station 1562+30)

Tran Sys	tems>			
EXPERIENCE Trav Computed by:	sportation EL	Date:	7/17/2017	
Checked by:	JC	Date:	7/18/2017	

Route:	Tri-State Tollway (I-294)	S.N. Exist: CMP 60" with 24" Liner/CMP 60" with 38" Liner/RCP 48"
Section:	4223	S.N. Prop: RCP 2-54"/RCP 48"
County:	Cook	Waterway: NB I-294 Ditch
Station:	1562+30	

Created Head Calculations

Flood	Freq.	Natural H.W.E. (ft)	Existing Headwater Elev. (ft)	Proposed Headwater Elev. (ft)	Created Head (ft) Section	
	Year	U/S Face of structure/Approach section	U/S Face of Structure	U/S Face of Structure	Existing	Proposed
	10	666.05	666.26	-	0.21	-
Design	50	666.97	667.55	-	0.58	-
Base	100	667.56	668.68	-	1.12	-
Max. Calc.	500	667.46	669.87	-	2.41	-

(1) The natural highwater elevation is the water surface elevation at the upstream side of the crossing as modeled in the stream natural condition, without the structure.

(2) The created head is calculated at the cross section upstream of the bridge/culvert which has the greatest difference between the natural and proposed conditions. This difference in elevation is then added to the Natural H.W.E. at the U/S face of the structure. This method of calcuating created head is only required for bridges and some major culvert crossings. Also, the preferred created head should never be negative. Headwater elevations = The natural highwater elevation + the created head

Freeboard and Clearance Calculations

Low EOP Elev	ation (ft)	Low Beam Elevation (ft)		Freq.	Headwater Elev. (ft)		Freebo	oard (ft)	Clearance (ft)	
Existing	Proposed	Existing	Proposed	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed
671.60				10	666.26	-	5.34	-		
Low Road S	tation:	Low Beam Station:		50	667.55	-	4.05	-		
Existing	Proposed	Existing	Proposed	100	668.68	-	2.92	-		
1559+29 (on Ramp B)				500	669.87	-	1.73	-		

(3) Low road elevation is calculated at the edge of pavement, and on the low side of the roadway.

(4) Freeboard is calculated from the 50 year design headwater elevation to the proposed low road elevation in the floodplain.

(5) Vertical clearance is calculated from the 50 year natural high water elevation to the proposed low chord (beam) bridge elevation (2 ft minimum requirement)

Waterway Opening Area Calculations

Flood	Freq.	Natural H.W.E. (ft) - U/S Face of Structure		U/S Invert Elevation (ft)		Depth of Water		Box Culvert Size (ft x ft)		Opening Area (ft ²)	
	Year	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
	10	666.05		662.67		3.38				22.86	
Design	50	666.97		662.67		4.30				23.58	
Base	100	667.56		662.67		4.89				23.58	
Max. Calc.	500	667.46		662.67		4.79				23.58	

5.5 DRAINAGE DESIGN CRITERIA

3 DRAINAGE DESIGN CRITERIA

The Drainage Criteria is based upon the criteria established in the Tollway Drainage Design Manual dated March 2016. Within the Tollway's right-of-way, the Tollway criteria will govern over the MWRD criteria per coordination with the Tollway and MWRD.

	Task	Description		
A - HYDROLOGY				
A-1	Rainfall Intensity and Distribution	ISWS Bulletin 70 (Isohyetal Values) with Huff Distributions will be used for bridges, culverts, channels, and detention basin design. ISWS Bulletin 70 (Sectional Values) will be used for storm sewers and roadway ditch design.		
		If a hydrograph method is used, rainfall should be distributed using the appropriate ISWS Circular 173 Huff rainfall distribution (Huff, 1990) and a critical duration analysis must be utilized.		
A-2	Peak Discharge for Major Waterway Crossings	FIS and MWRD discharge will be used for major waterway structures when available. If storm gage data are available, they may be used for design purposes. Otherwise, a hydrograph method shall be used to calculate peak flows. Regression equations may be used for watersheds \geq 450-ac in urban area.		
A-3	Peak Discharge for Storm Sewers, Ditches, and Minor Culverts	Rational Method for watersheds less than 200-ac. However, a hydrograph method is preferred for complex facilities and larger watersheds.		
A-4	Runoff coefficients C	C = 0.95 (impervious), $C = 0.30$ (pervious)		
A-5	Runoff curve numbers CN	CN = 74 (open spaces with grass cover on 75% - lawns, parks, golf courses, cemeteries, for hydrologic soil group C)		
	B - HYDRAULICS			
B-1	Bridge	Design frequency is 50-yr storm; the calculated design headwater elevation (HW) shall be minimum 3 ft. below the low edge of pavement.		
		The low chord shall be at least 2 ft. above the 50-yr natural highwater surface elevation and also above recorded high water at site.		
		Check for the 500-yr storm, HW shall not encroach onto the roadway edge of pavement on the low side of the roadway.		
		If the structure is located in designated floodway or floodplain, see item B-2 below for additional design criteria.		
B-2	Major Waterway Crossings Located in Designated Floodway or Floodplains	Required for all designated floodways and floodplains with greater than 1 sq.mile (640-ac) watershed area. For structures in designated floodways, the structure shall meet the 17 ILL. ADM. CODE-Part 3708 rules for Bridge and Culvert Reconstruction or Modification, which may involve determining the feasibility of reducing the created head to 0.1 ft.		

Drainage Design Criteria

October 2016

	Task	Description
		over natural for events up to and including the 100-yr storm, if the structure is a source of flood damage. If the structure is not a source of flood damage, minimum design criteria is to not increase the flood profile by more than 0.1 ft. over existing, for flood profiles up to and including the 100-yr storm.
		When no designated floodway exists, the proposed structure shall meet the Part 3700 rules for Bridge and Culvert Reconstruction. In general, replacement structures should reduce created head to 0.5 ft. for floods up to and including the 100-yr event.
		See also App. K to the Tollway's Drainage Manual Dated March 2016.
В-3	Storm Sewers	Design frequency is 50-yr storm; the maximum highwater elevation shall be kept at least 2 ft. below the manhole/inlet rim elevation.
		Zero encroachment on traveled way and no closer than 3 ft. from the edge of the traveled way. Maximum water depth on pavement of 0.35 ft.
		Minimum size shall be 15" dia. RCP under traveled way, or 12" dia. RCP outside of traveled way. Minimum 6-in cover between bottom of subbase and crest of the pipe.
		Maximum structure spacing is 350 ft. (15" to 24" dia.), 400 ft. (27" to 36" dia.), 500 ft. (42" to 54" dia.) and 1,000 ft. (over 60" dia.).
		Maximum inlet spacing is 1,000 ft. The first inlet spacing may be as great as 1,200 ft. from crest vertical curve. Minimum three structures at sag locations.
B-4	Cross Road Culvert	Design frequency is 50-yr storm; the calculated design headwater shall be minimum 3 ft. below the low edge of pavement, $HW/D \le 1$ ratio or maximum 0.5 ft. of created head.
		Check for 100-yr storm, no encroachment on any adjacent properties. Check for 500-yr storm, no overtopping of roadway.
		Minimum size for roadway or ramp crossings is 24" dia. RCP for lengths less than 200 ft. and 30" dia. RCP for longer than 200 ft.
		Minimum size for ditch culverts is 18" dia. RCP.
		No CMP will be allowed.
		Use HY-8 for non floodplain areas and HECRAS for floodplain areas.
B-5	Ditch Design Requirements	Design frequency is 50-yr storm. The ditch depth shall be a minimum of 3 ft., or the water surface elevation (WSEL) in the ditch shall be 2 ft. below the edge of pavement, or 1 ft. below the adjacent right-of-way, whichever is controlling.
		The minimal longitudinal slope shall be 0.3% (with 0.5% preferred by IDOT District One). Longitudinal slope less than 0.3% is allowable with the approval of the Tollway, if special consideration is provided.
		The velocities shall be generally between 3 to 5 fps. Ditches with more than 5-fps will need to be lined. Ditch lining recommendations will

Drainage Design Criteria

	Task	Description
		consider velocity and soil types. Check for 100-yr storm, the WSEL shall not encroach onto the roadway.
B-6	Ditch Cross Section Requirements	For new ditches, 6:1 foreslopes, 4–ft. bottom and 4:1 backslopes are desirable, but 4:1 foreslopes, 2-ft bottom and 3:1 backslopes are acceptable. When existing ditches are to remain or to be re-established, use 4:1 foreslopes, 2-ft bottom, and 3:1 backslopes.
		The ditch check crest must be a minimum of 1 ft. above grated inlets and 2 ft. below the edge of pavement.
B-7	Pump Station	Design frequency is 50-yr storm; the design hydraulic gradeline shall have a 2 ft. freeboard below the top of the inlet. Check for 100-yr, the hydraulic gradeline shall not be above the top of the inlet.
B-8	Interchange and Expressway	The proposed interchange and expressway in the floodplain shall have a minimum of 3 ft. of freeboard against the 50-yr storm WSEL, or 2 ft. of freeboard against the 100-yr WSEL, whichever is higher.
	C - FLOODPLAIN	
C-1	Compensatory Storage	For fill in the regulatory floodplain, 17 ILL. ADM. CODE-Part 3708 rules will need to be followed.
		The Compensatory Storage Volume, for any fill due to roadway widening and structures in the regulatory floodplain, shall be provided incrementally between the normal elevation and the 10-yr flood elevation and between the 10-yr flood elevation and the base flood elevation (BFE) (100-yr flood elevation) as follows: (i) at a 1:1.0 ratio for Cook County (ii) at a 1:1.0 or 1:1.5 ratio for DuPage County. For details, see DuPage County Countywide Stormwater and Flood Plain Ordinance, dated April 2013, section 15-81.D
	D - DETENTION	
D-1	General Considerations	Detention volume shall be provided to compensate for the effect of increased peak discharges resulting from the additional impervious areas. The proposed construction shall not increase the existing peak runoff from Tollway property and shall comply with the maximum allowable release rate criteria (see section D3). Offsite drainage shall be bypassed rather than detained.
		Detention in ditches can be provided if it does not cause a hazard to traffic. Detention in pipes is acceptable only if no other alternate is feasible. A 2-fps cleansing velocity must be provided for upsized pipes used for conveyance and storage purpose.
		Detention facilities and floodplain compensatory storage site shall be provided separately.
D-2	Design Storm	100-yr storm event for the critical storm duration (Cook County facilities) and for the 24-hr storm duration (DuPage County facilities), using the ISWS Bulletin 70 rainfall depth.

Drainage Design Criteria

	Task	Description
D-3	Maximum Allowable Release Rates	The maximum allowable release rates are estimated, for the added impervious area only, as follows:
		 (i) 0.04-cfs/acre, for the 2-yr storm and for the critical storm duration (Cook County facilities) and for the 24-hr storm duration (DuPage County facilities). (ii) 0.10-cfs/acre, for the 100-yr storm and 24-hr storm duration (DuPage County facilities). (iii) 0.15-cfs/acre, for the 100-yr storm and for the critical storm duration (Cook County facilities).
		The offsite post-development release rates shall be less than or equal to the pre-developed condition release rates, for the 2-yr and 100-yr storm events, for the critical storm duration (Cook County facilities) and for the 24-hr storm duration (DuPage County facilities). The above release rates should be estimated using an appropriate hydrograph routing method such as HEC-HMS, xpSWMM, Win TR-20, or Pond-Pack.
D-4	Required Volume	The volume of required detention storage (acre-feet) can be initially estimated using the maximum allowable release rates (see section D-3) and as shown in Appendix G1 (for Cook County facilities) and Appendix G2 (for DuPage County facilities).
		The final detention volumes and the outlet control structure (restrictor) will be designed according to section D-5 and section D-6.
D-5	Water Quality Volume	The required volume control shall include the capture of the first flush, a runoff volume equal to 1.00" (Cook County), or 1.25" (DuPage County) of rainfall times the added impervious area.
		The runoff from the first flush rainfall shall be stored below the elevation of the primary gravity outlet of detention facility, or within roadside ditches located upstream of the proposed detention facility. A control structure or underdrain may be used, provided that the draw down time is between 48 and 96 hours.
		According to USACOE (Oct 2016), the applicants for Regional Permit 3 shall be required to make a reasonable attempt to retain the runoff from the 1.00" rainfall event. Where project constraints make it impracticable to fully met the stormwater performance standard, applicants shall be allowed to implement practices according with the following hierarchy: (i) retention facilities, (ii) use of bioswales, (iii) detention facilities, (iv) use of catch basins with sumps or other inlet controls, and (v) runoff design practices for bridge deck runoff crossing waters to minimize stormwater impacts.
D-6	Methodology	Detention shall be designed using an appropriate hydrograph routing method such as HEC-HMS, xpSWMM, Win TR-20, or Pond-Pack.
		Proposed condition release rates, at the main outfall (outlet), must be less than or equal to existing condition release rates, for the 2-yr and 100-yr storm events for the critical storm duration.
		Within the same watershed, some shifting of required detention between

Drainage Design Criteria

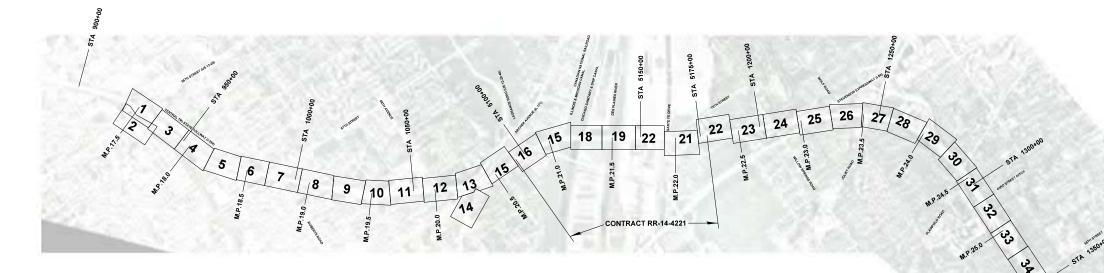
October 2016

	Task	Description
		outfalls (outlets) is allowable (regional detention). The proposed release rates, at the main outfalls (outlets) included in the regional detention analysis, must be less than or equal to existing release rates, for the 2-yr and 100-yr storm events for the critical storm durations.
D-7	Detention Basin	Dry detention basins are preferred. Wet basins are allowed for water quality, if they are not a hazard or are shielded by guardrail, and only with the Tollway approval.
		A minimum of 2 ft. freeboard above the maximum water surface elevation (100-yr) to the top of berm and a minimum of 3 inches above the maximum water surface elevation (100-yr) over emergency spillway to the top of berm shall be provided.
		The control structure in and out pipes should have the same size. The minimum restrictor plate orifice size is 4" dia.
D-8	Detention in Ditches	Maximum water surface elevation (100-yr) shall be at least 2 ft. below the edge of pavement.
		A maximum detention depth of 4 ft. is recommended.
		Minimum ditch check outlet pipe shall be 12" dia. and a minimum 4" dia. restrictor plate orifice.
		A minimum of 1 ft. freeboard shall be provided between the maximum water surface elevation (100-yr) and the existing right-of-way ground elevation.
D-9	Detention in Infield Areas	Maximum water surface elevation (100-yr) shall be at least 2 ft. below the edge of pavement.

For flex lane drainage requirements (previously referred to as Lane 0), the criteria for allowable storm water spread within the flex lane is still in progress. For the proposed drainage plans included in this report, we have assumed that the flex lane is treated similar to a shoulder where spread requirements must be met for Lane 1, not the flex lane, which were the criteria that were followed on the Jane Addams I-90 Projects for Lane 0. For reference, please see Appendix B, Section 6.7 for the technical memorandum submitted to the Tollway in draft form.

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5.6 PROPOSED DRAINAGE PLAN



<u>drainage legend</u>				
BOUNDARY LINES/SYMBOLS	Existin	<u>g drainage</u>	PROPOS	ED DRAINAGE
SLOTTED DRAIN	0	MANHOLE	Θ	MANHOLE
●● ● USGS DRAINAGE DIVIDE	0	CATCH BASIN	٠	CATCH BASIN
	•	INLET	-	INLET
STREAM		HEADWALL		HEADWALL/END SECTION
FLOODPLAIN BOUNDARY	٩	FLARED END SECTION	$\leftrightarrow \rightarrow$	SUMMIT
FLOODWAY BOUNDARY	\leftrightarrow	SUMMIT	~~>	DITCH FLOW
WATER OF US - WOUS /	~~>	DITCH FLOW	-+-	SWALE
WETLAND / STORMWATER CONVEYANCE	-+-	SWALE	bb	STORM SEWER
		STORM SEWER		CULVERT
		CULVERT	POND-PR-19A	DETENTION POND- ID
	POND-19A	DETENTION POND- ID	188:00.89	RIPRAP
		RIPRAP		CONCRETE REVETMENT MAT
		CONCRETE REVETMENT MAT		

NOTE: EXISTING SYSTEM TO REMAIN IN PLACE SHALL BE CLEANED AND TELEVISED

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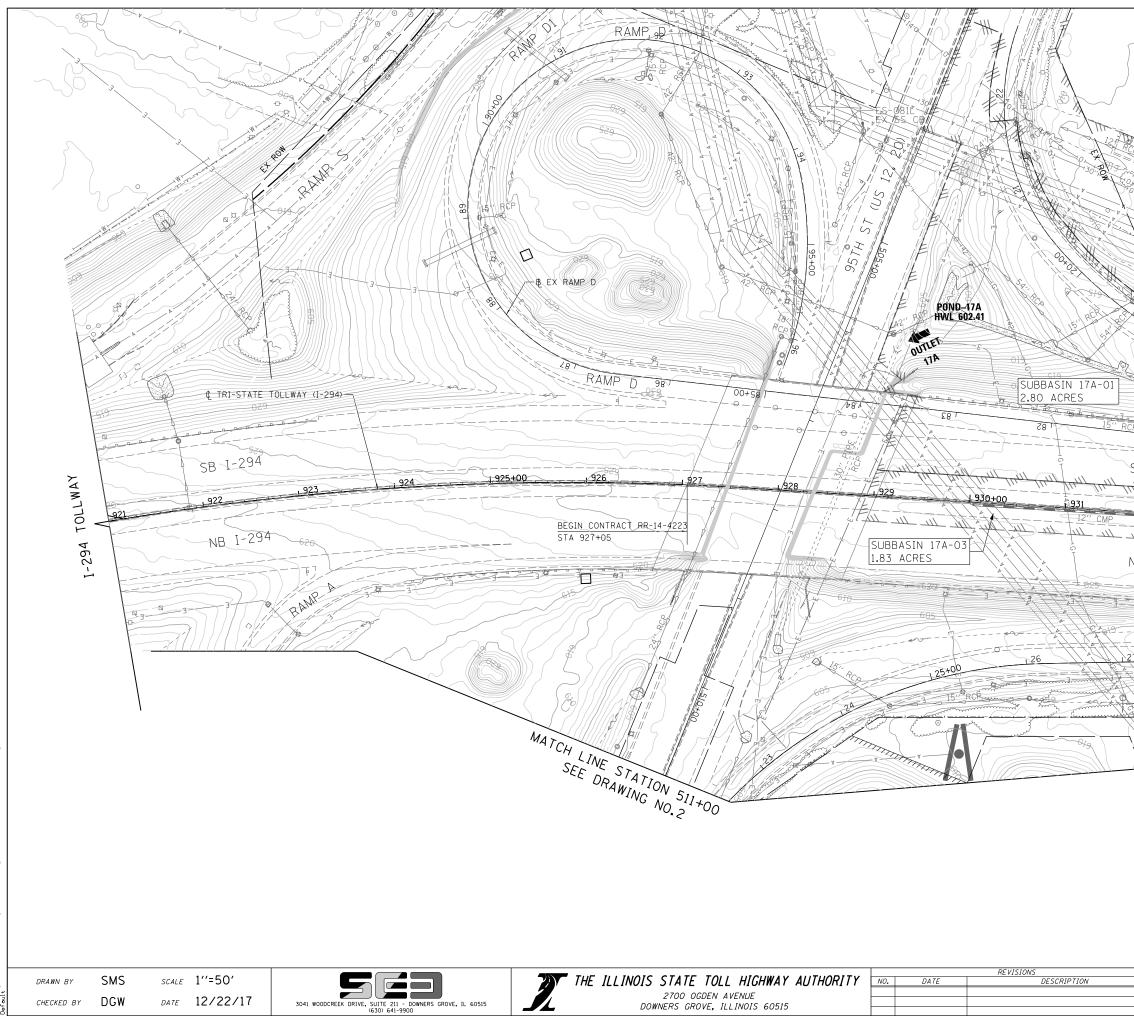
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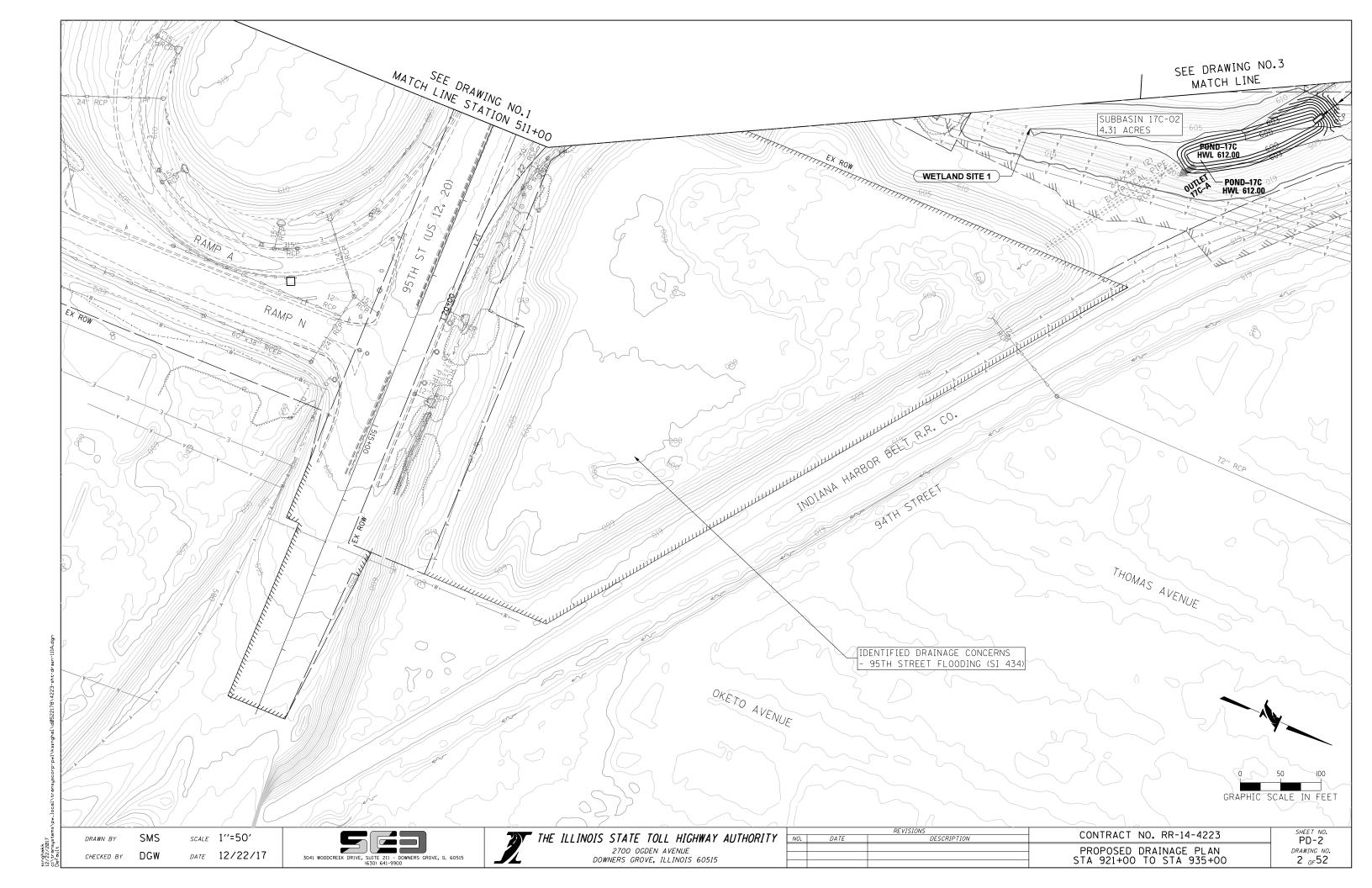
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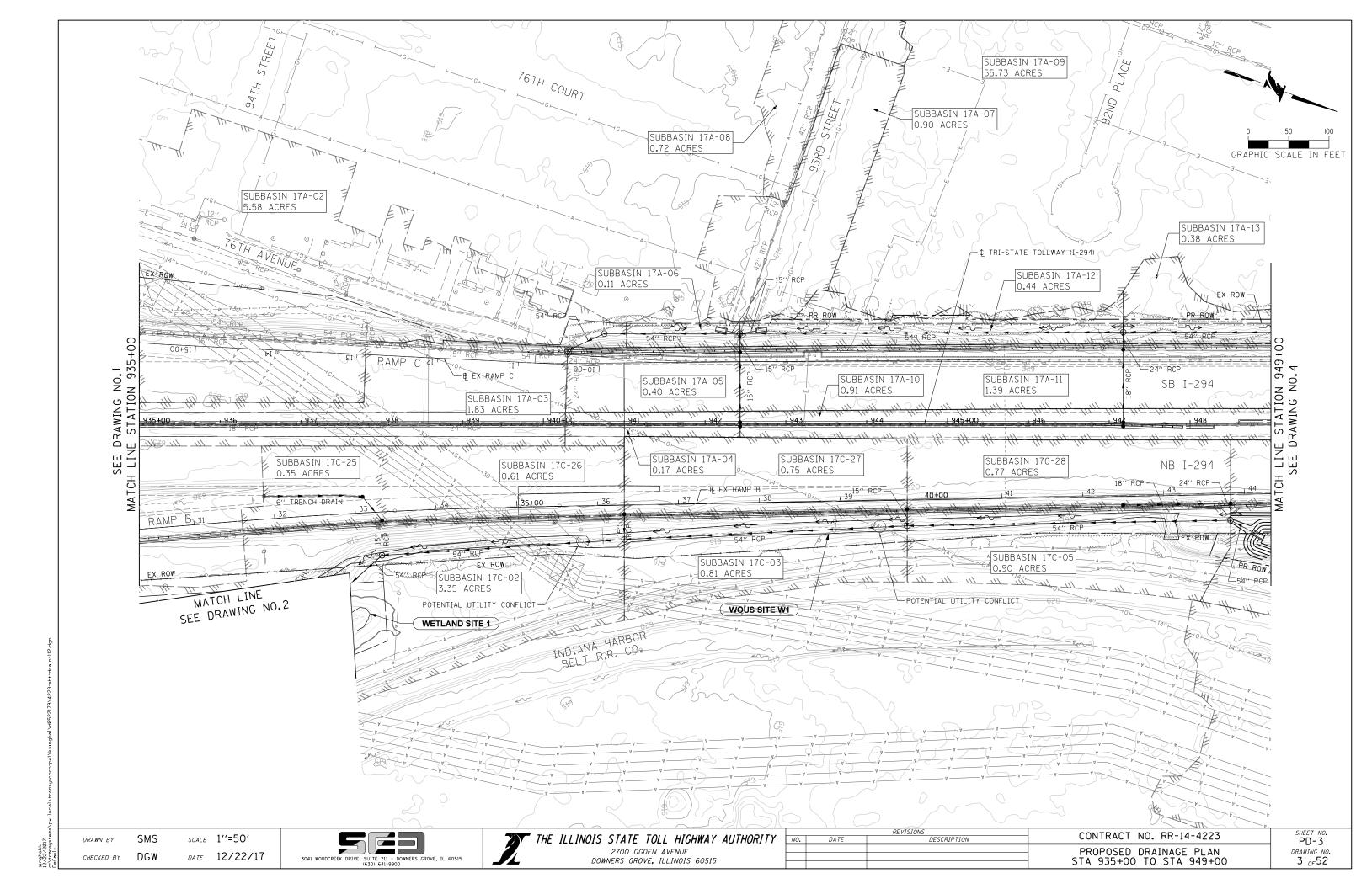
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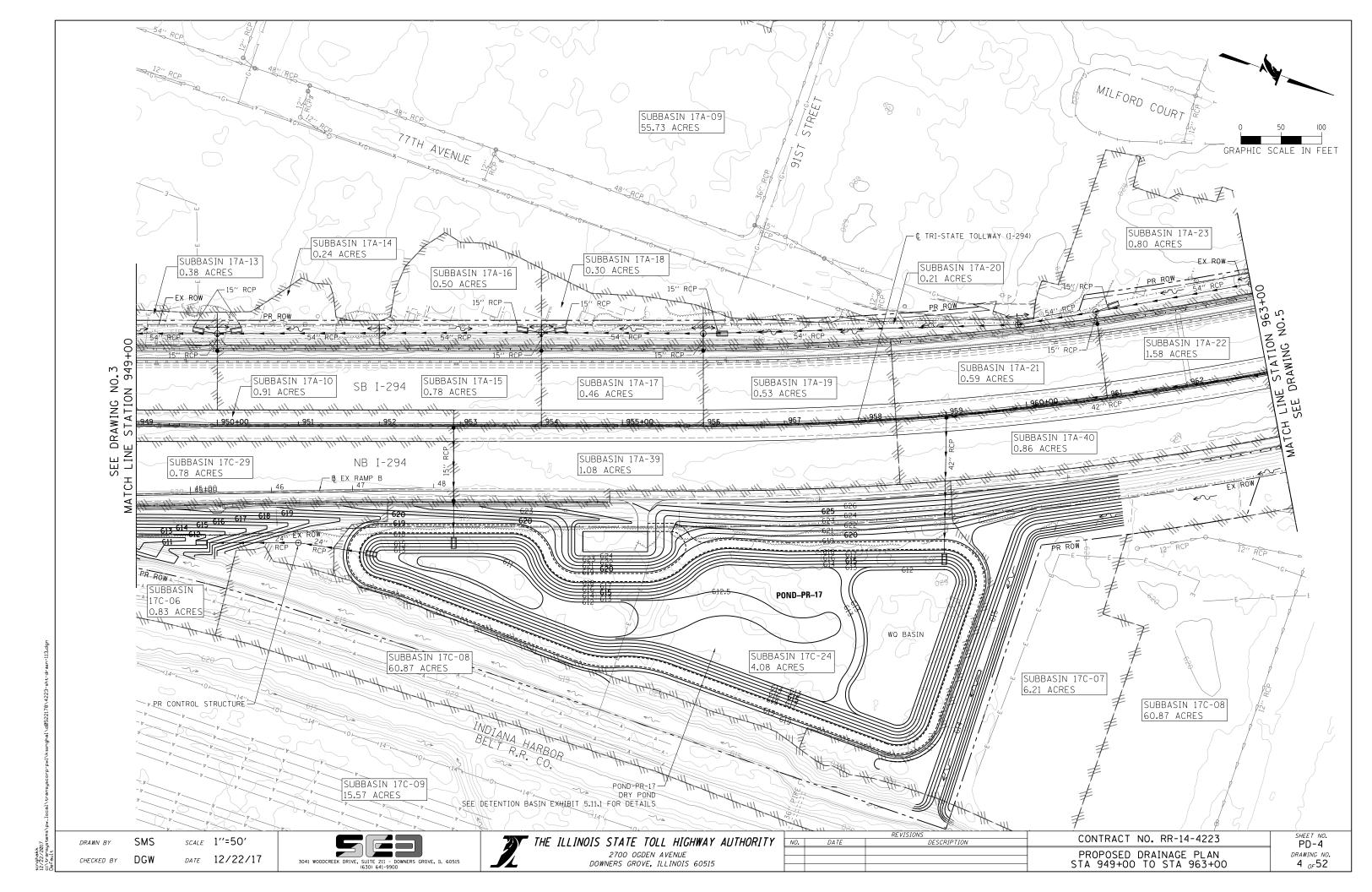
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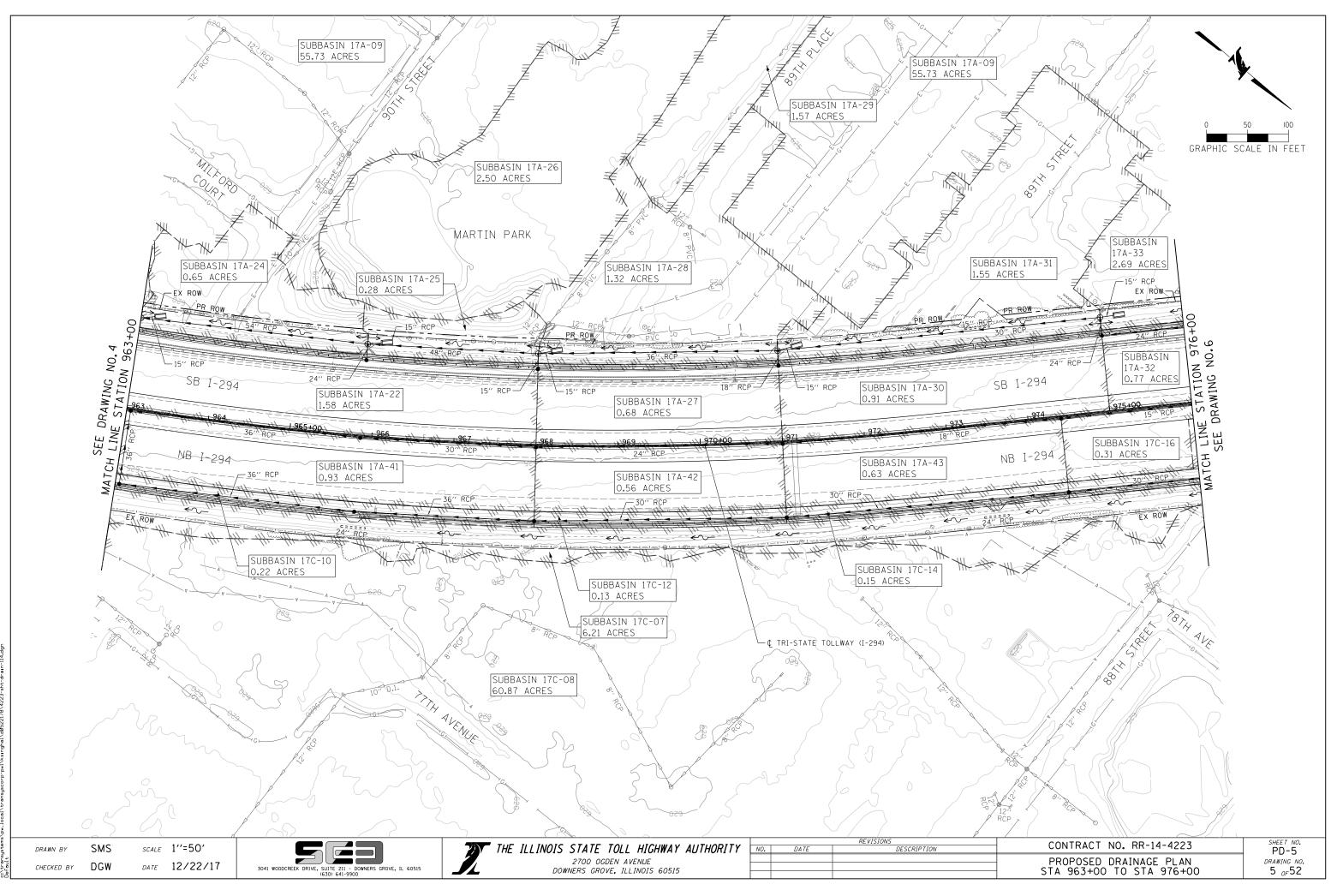


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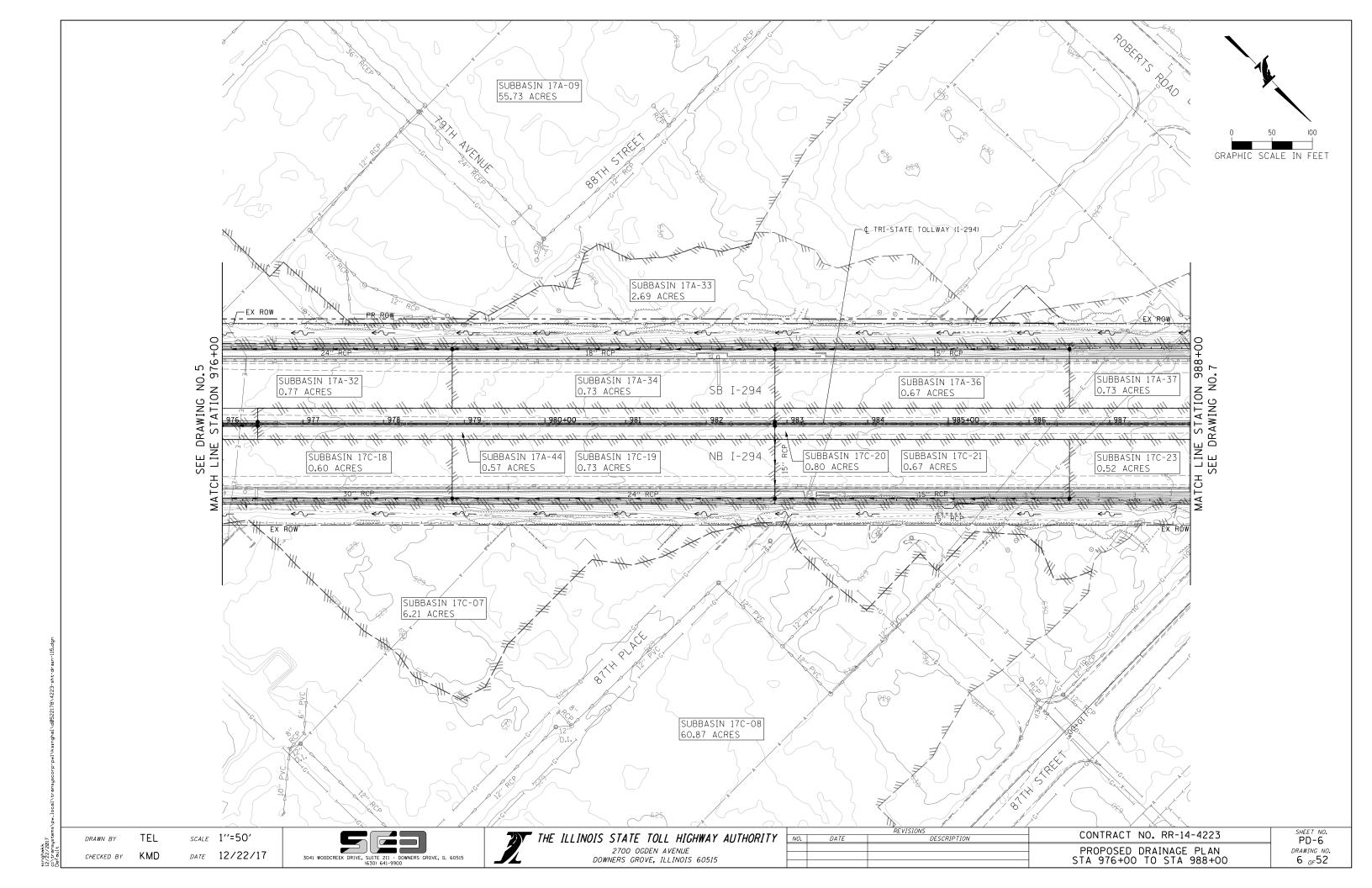


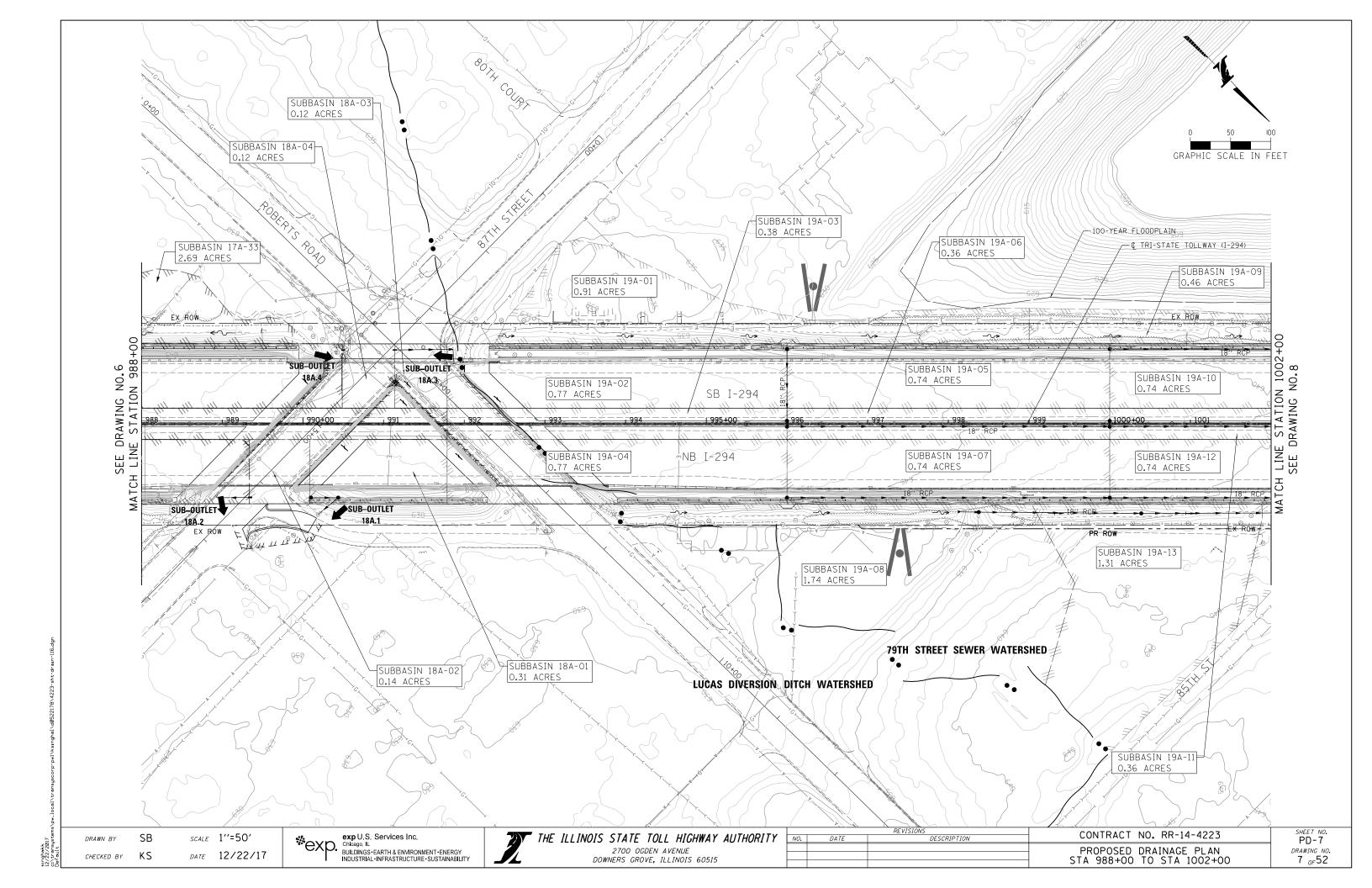


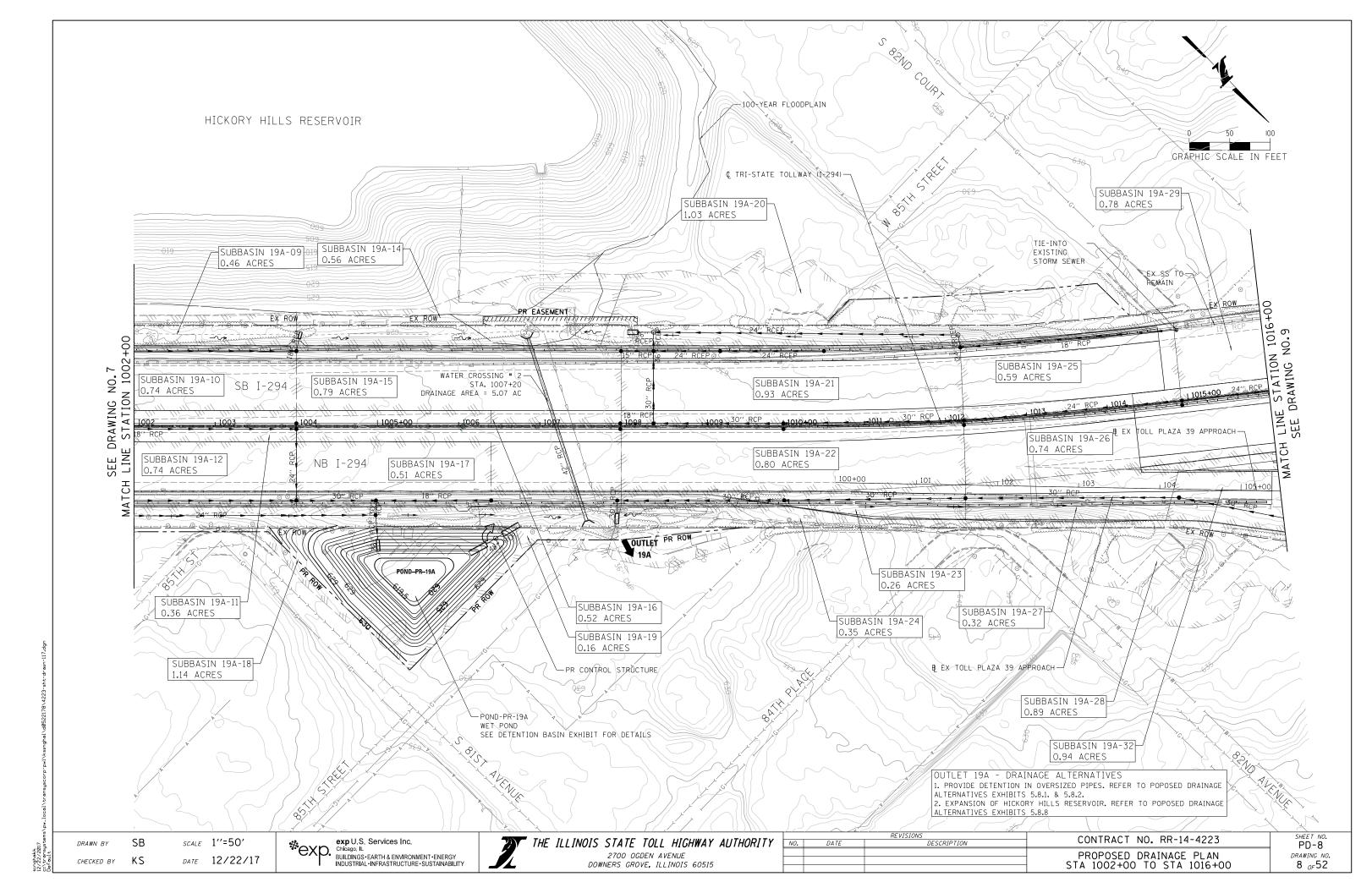


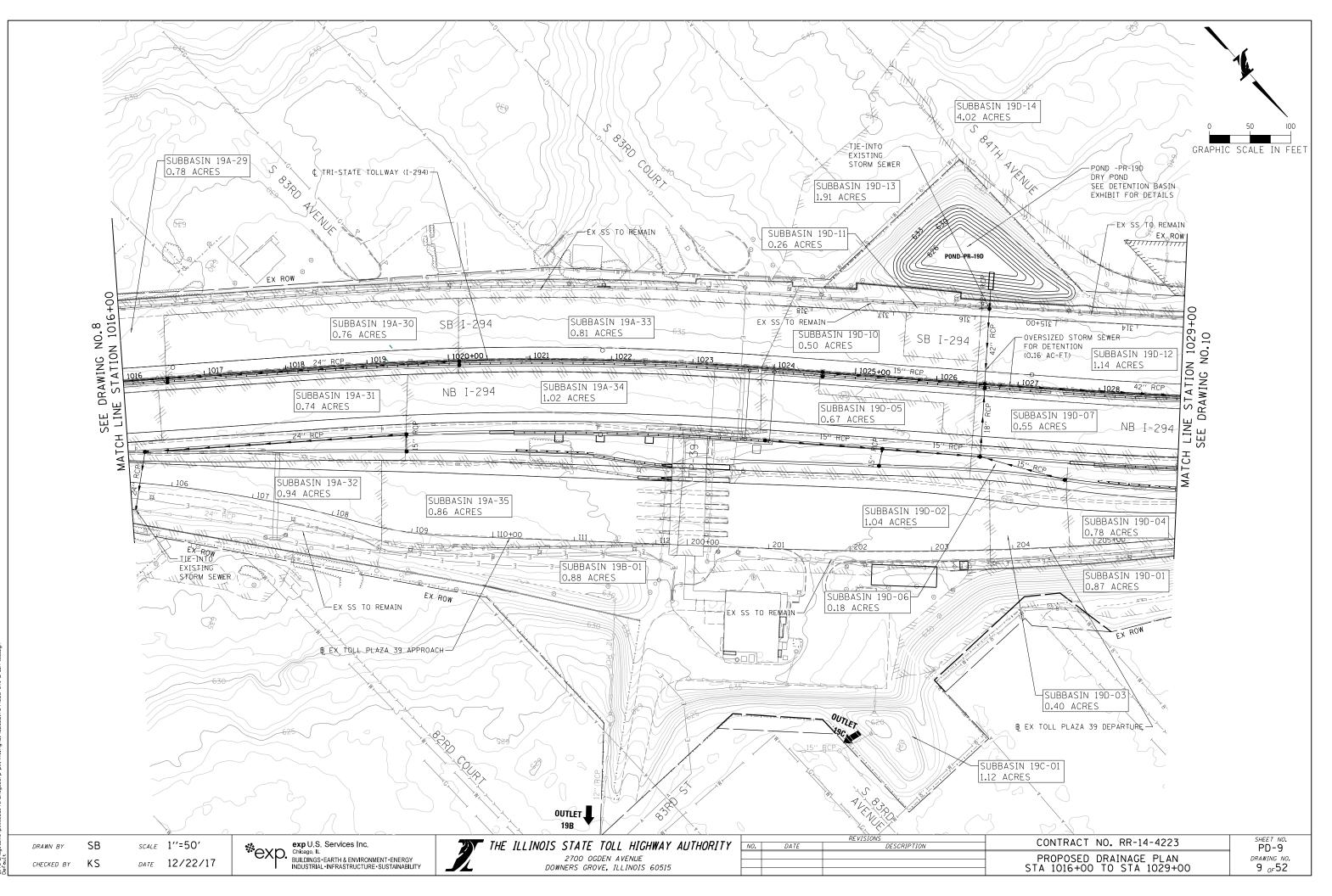


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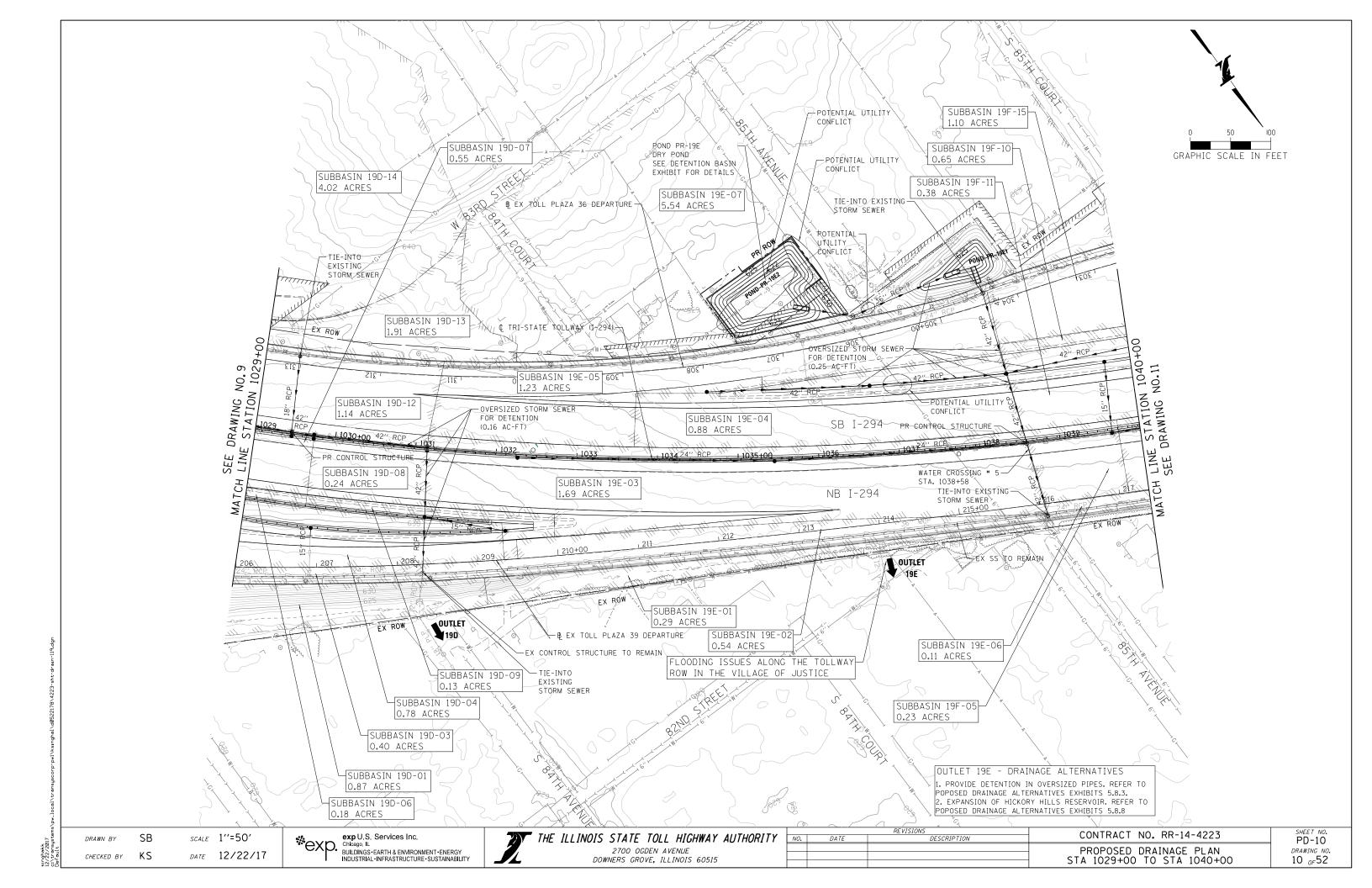


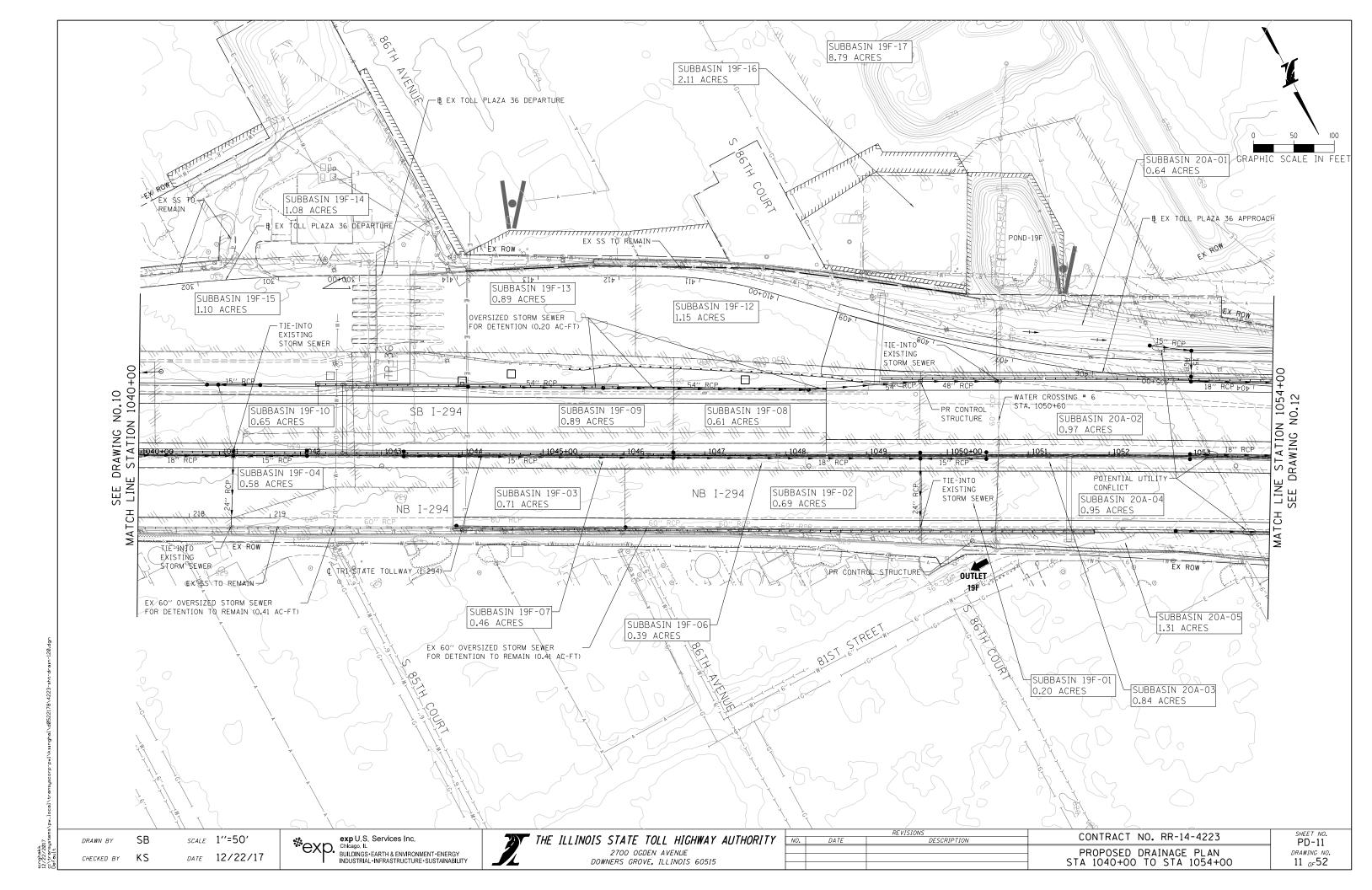


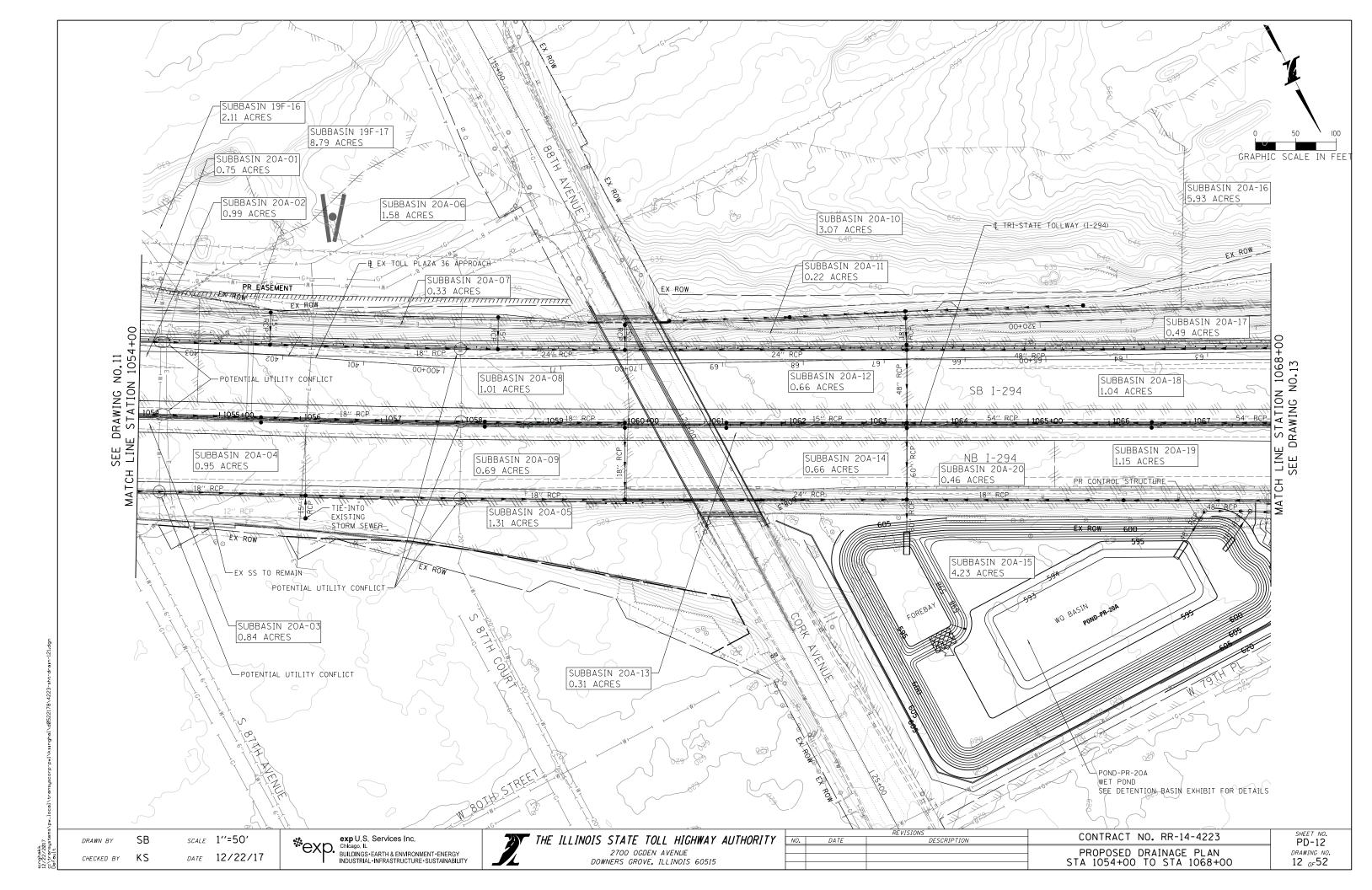


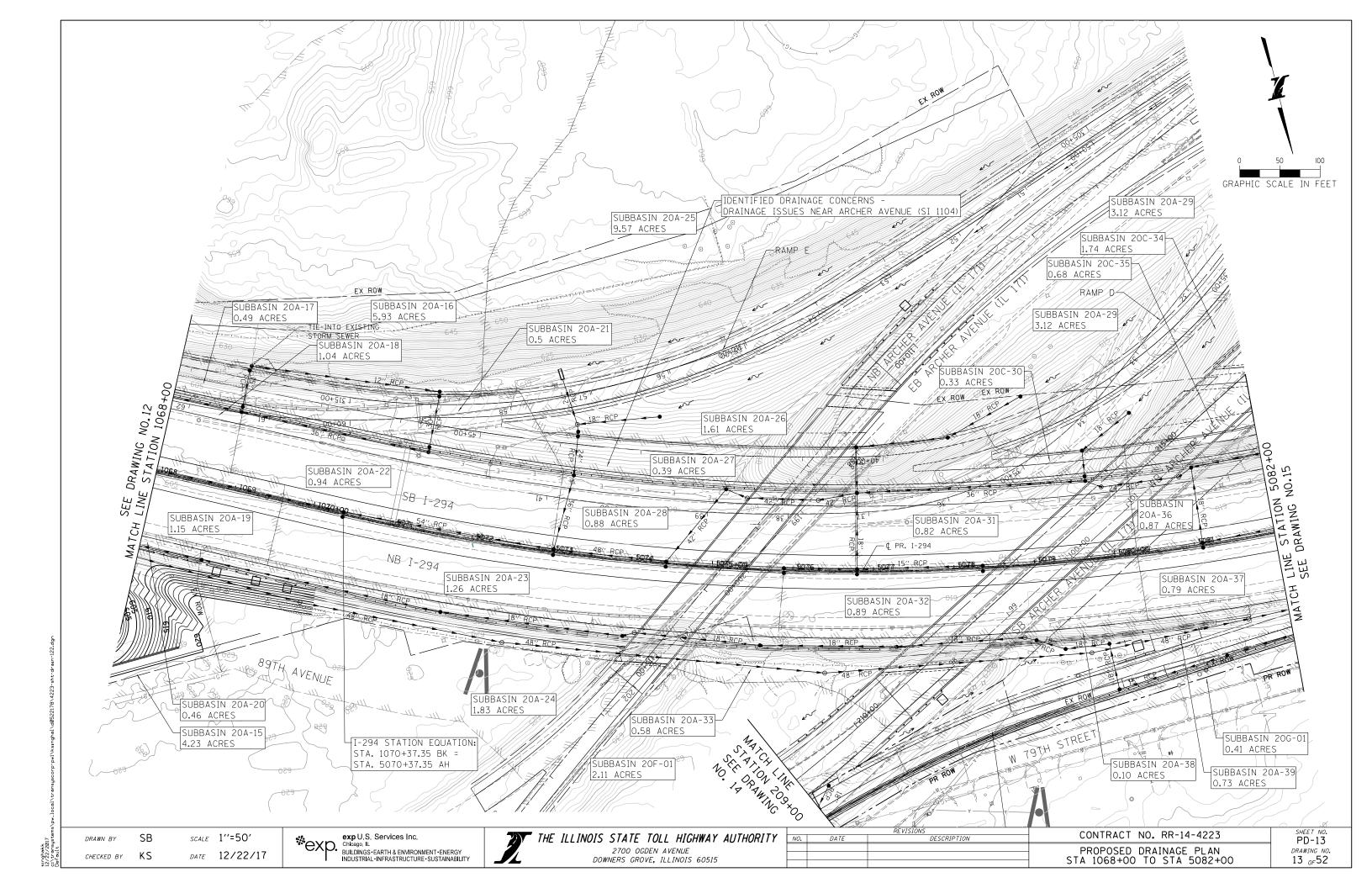


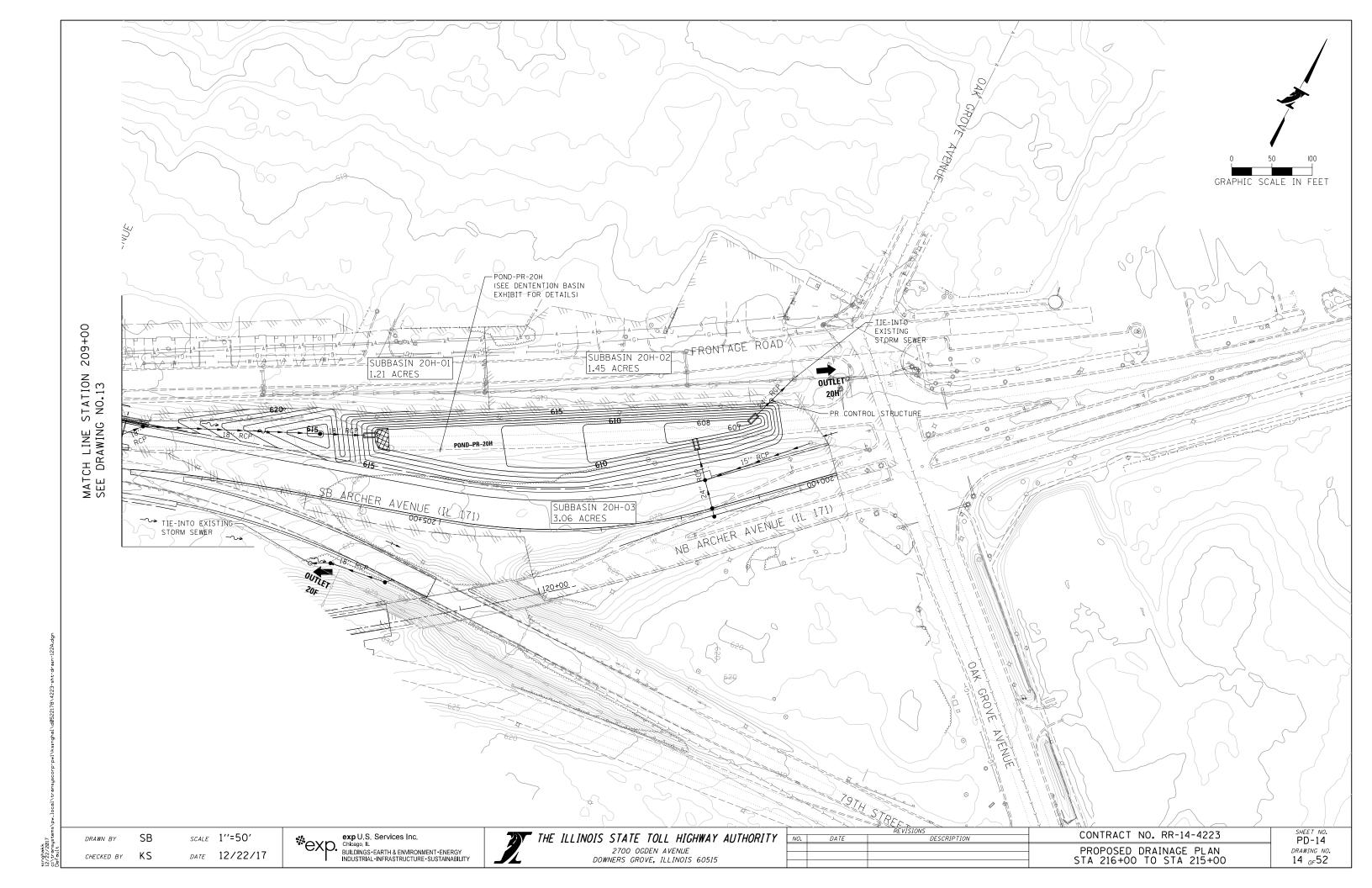
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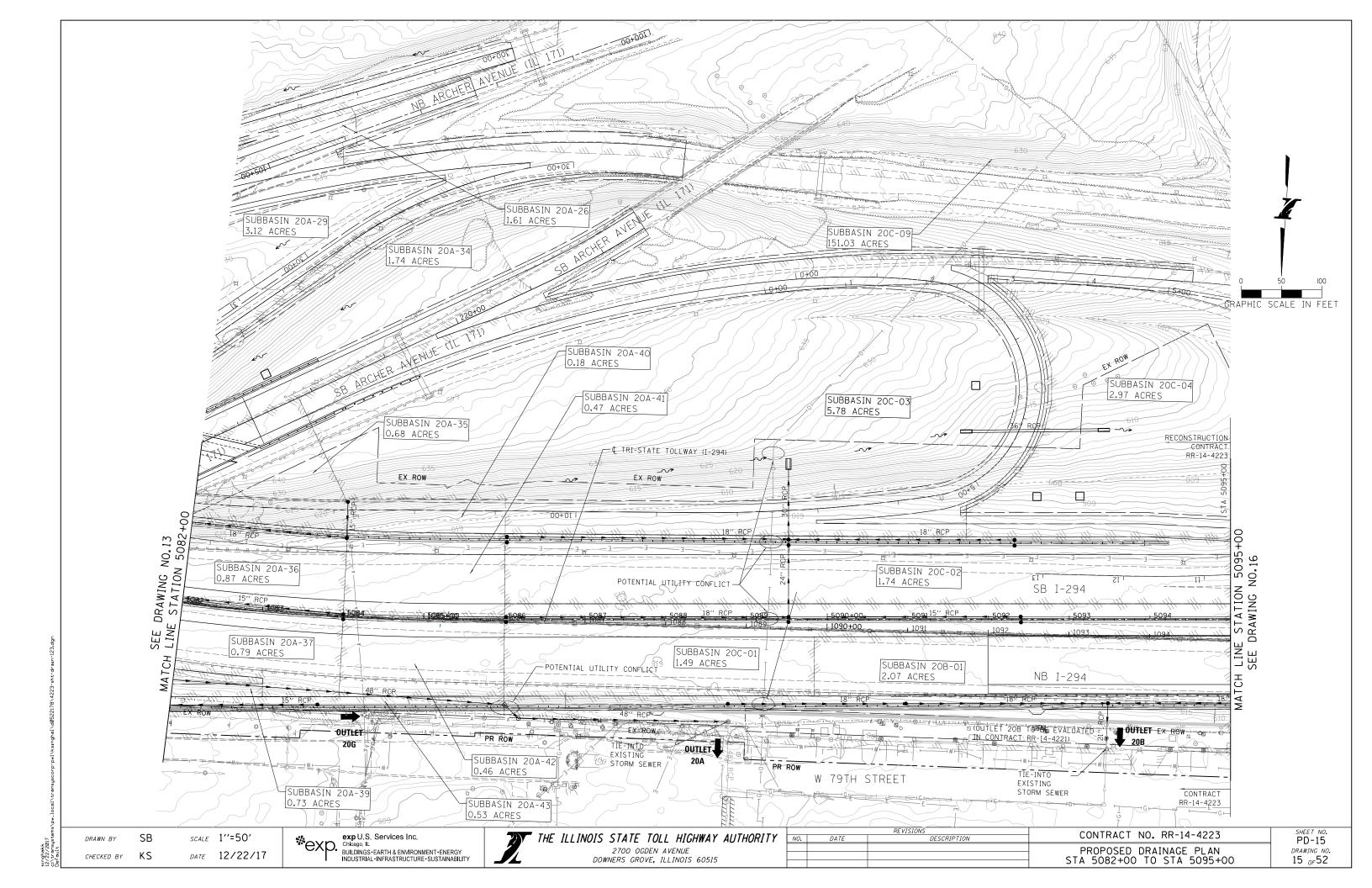


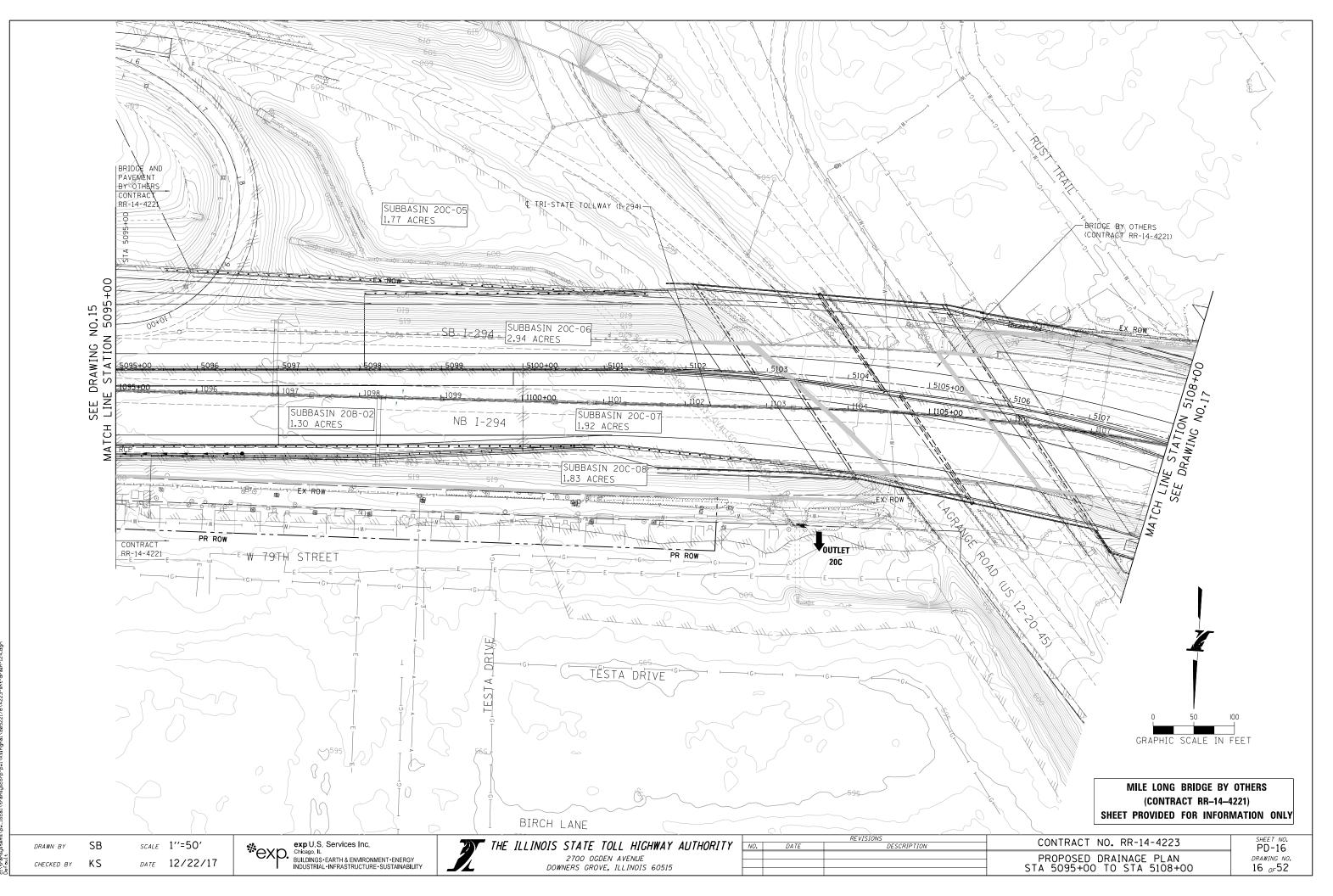




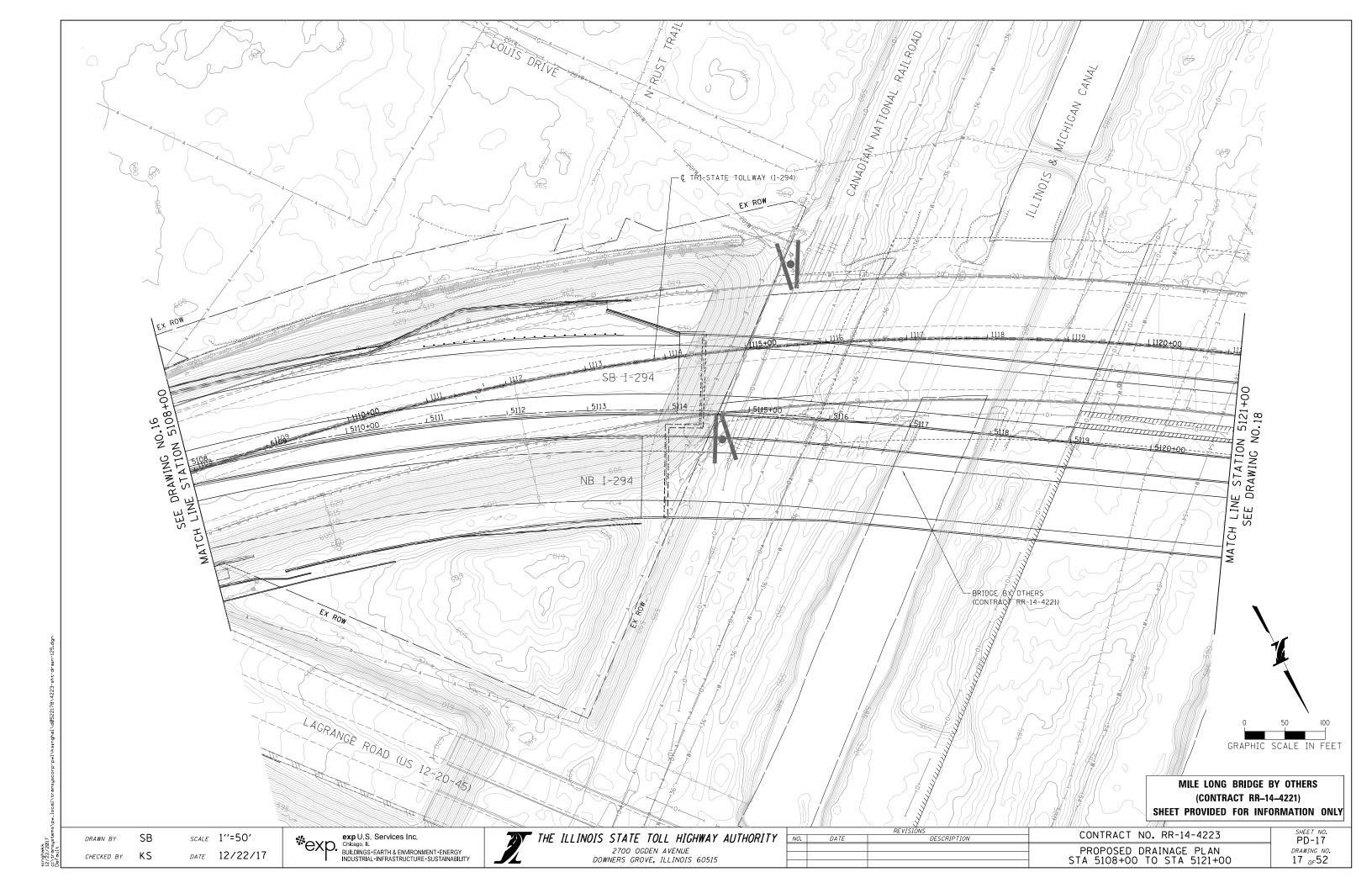


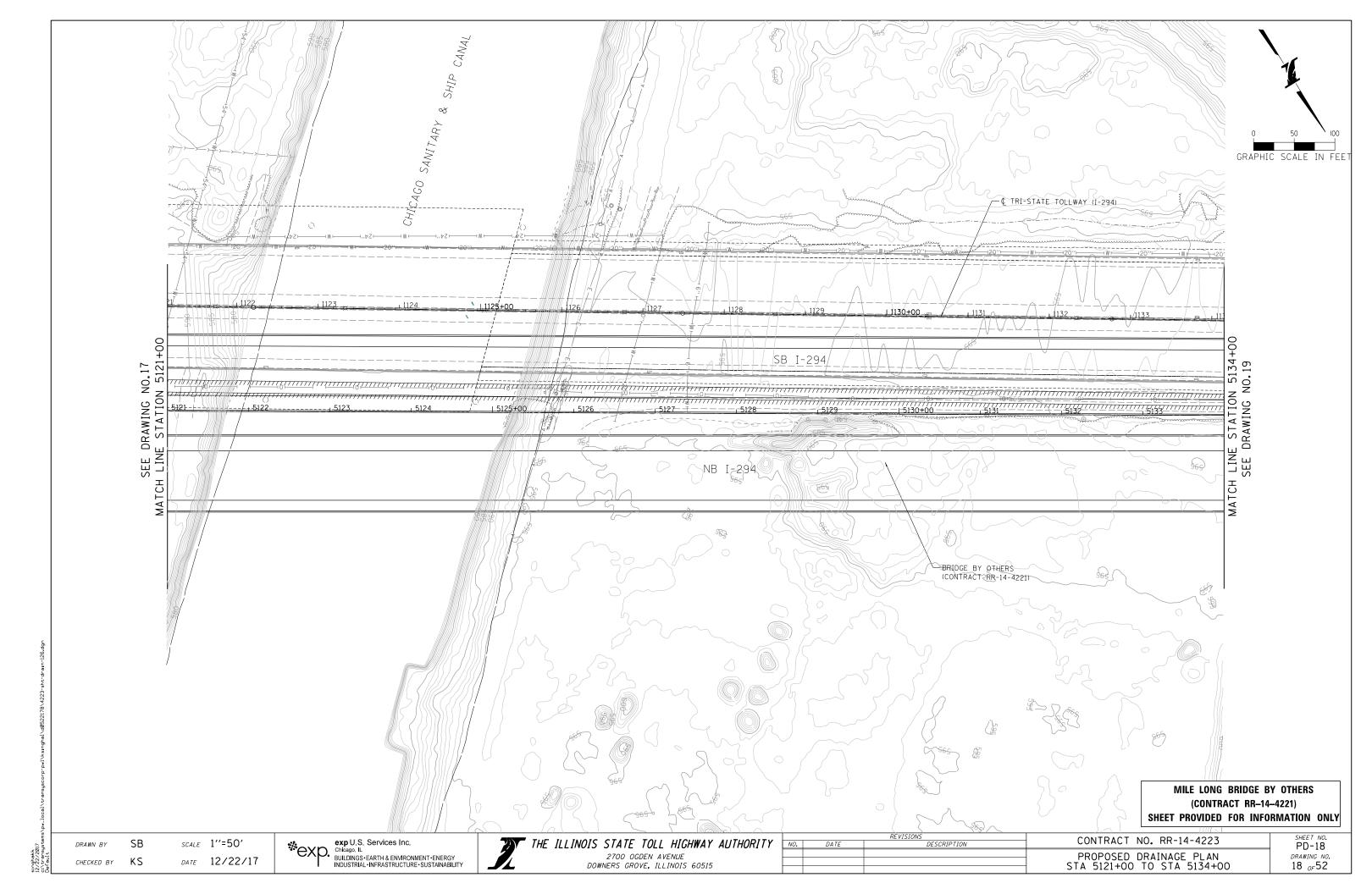


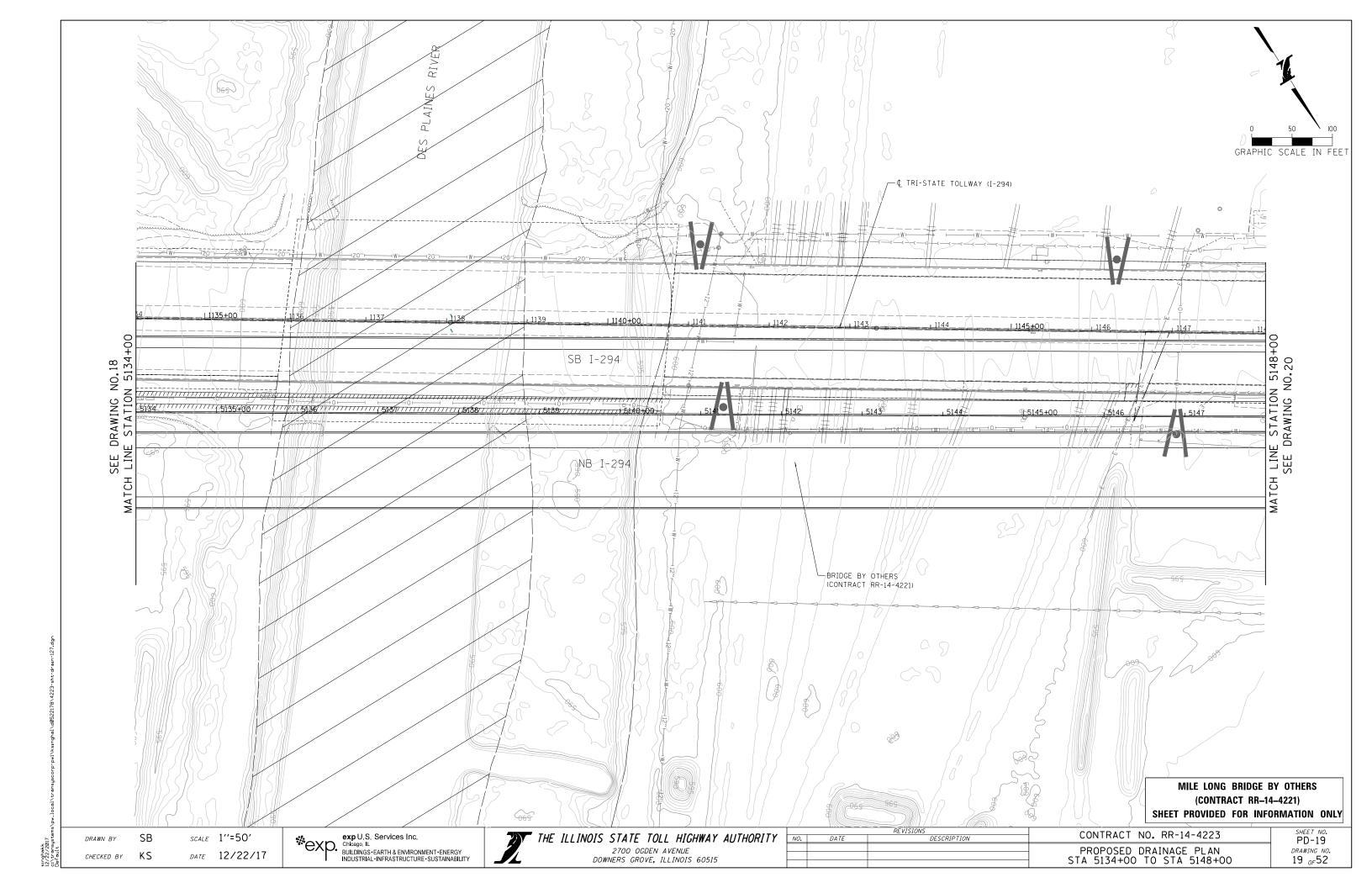


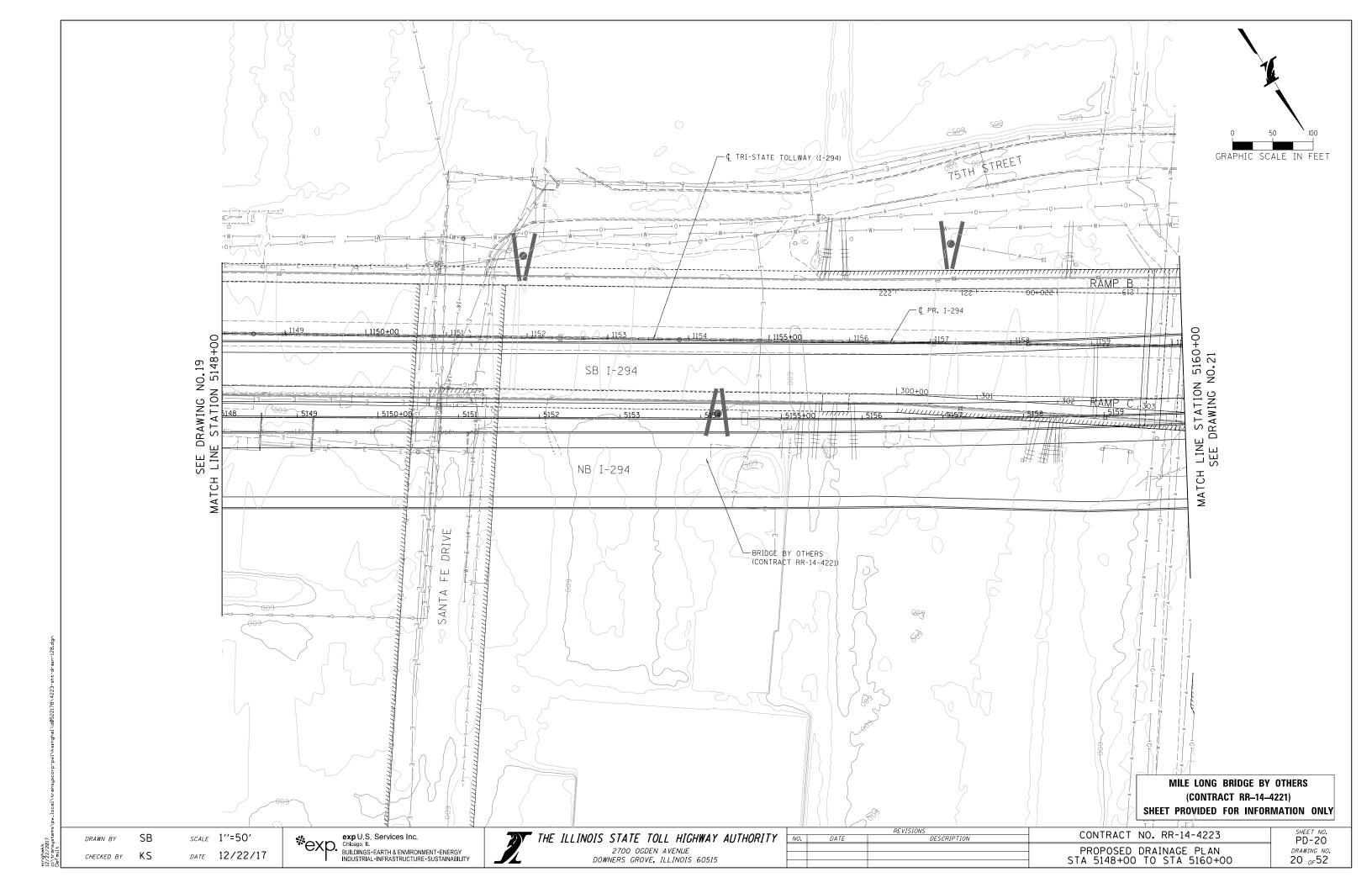


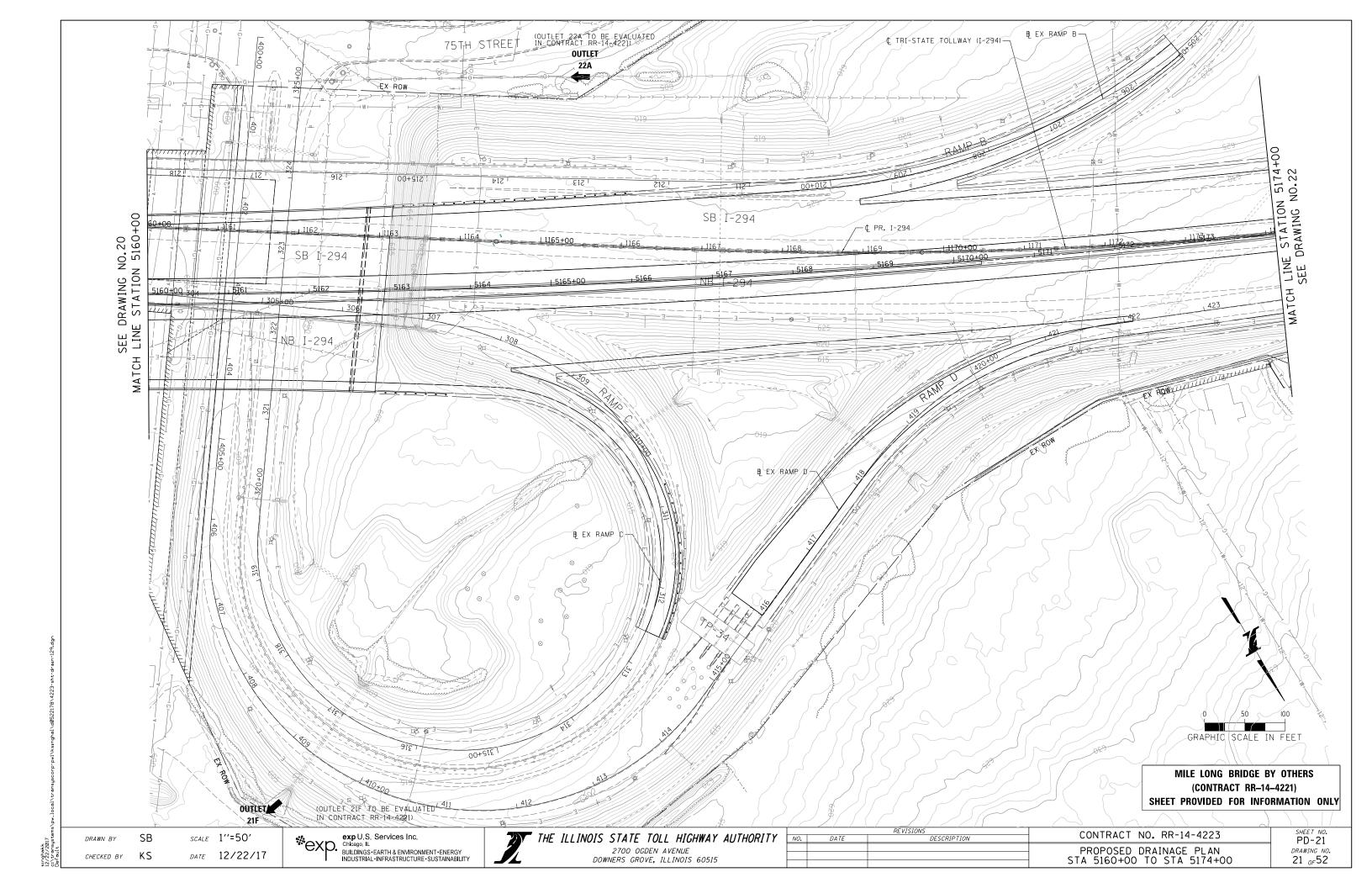
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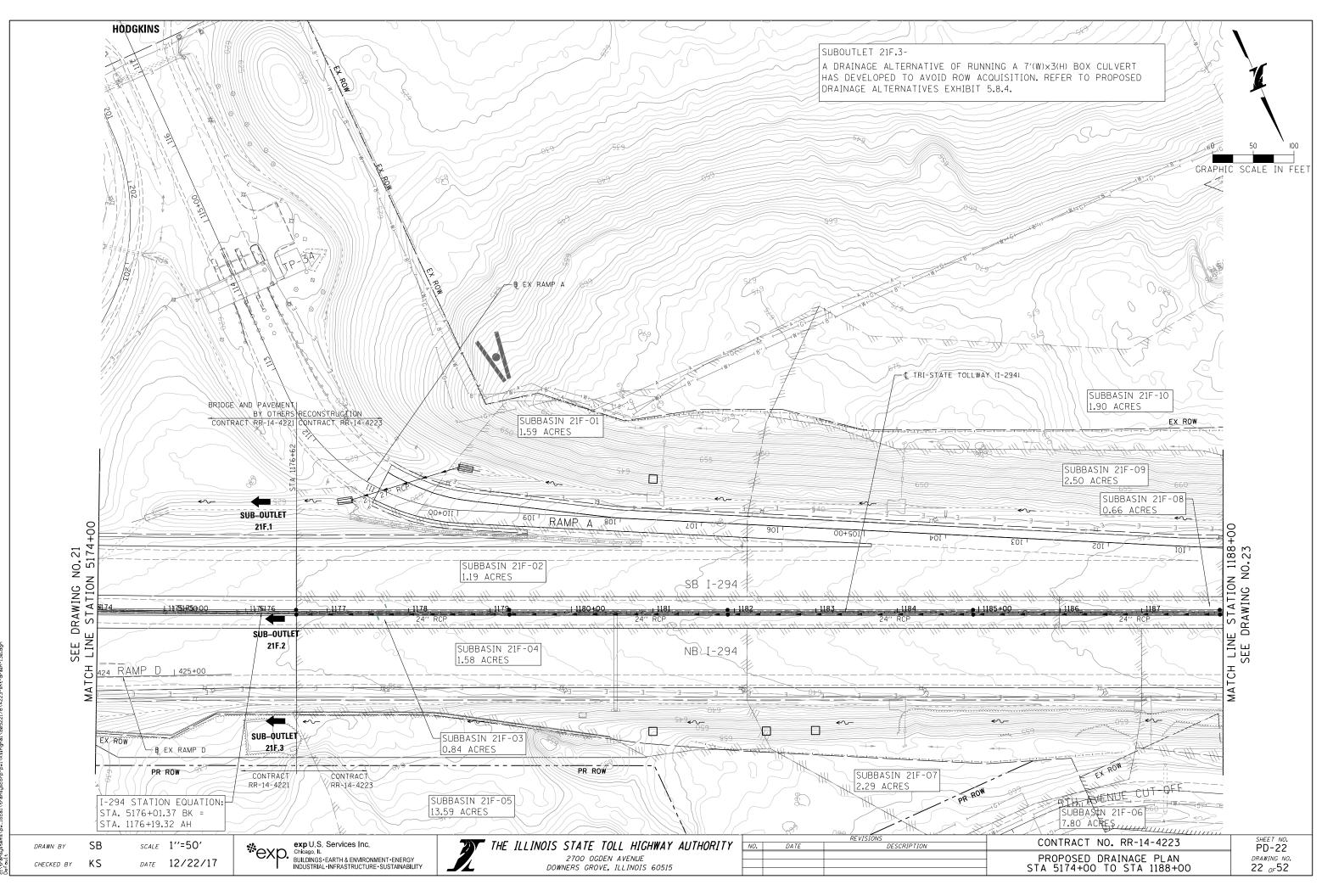




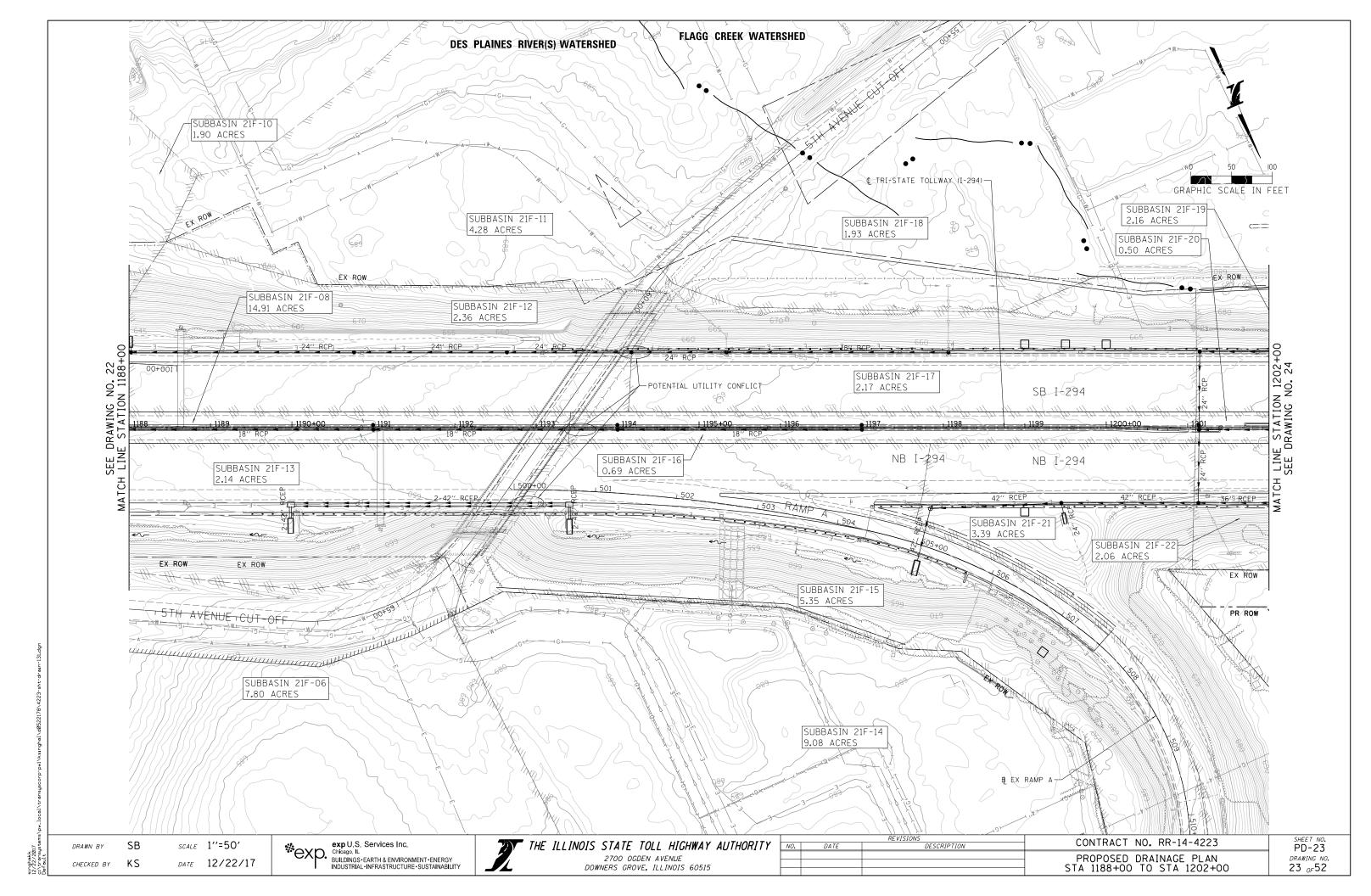


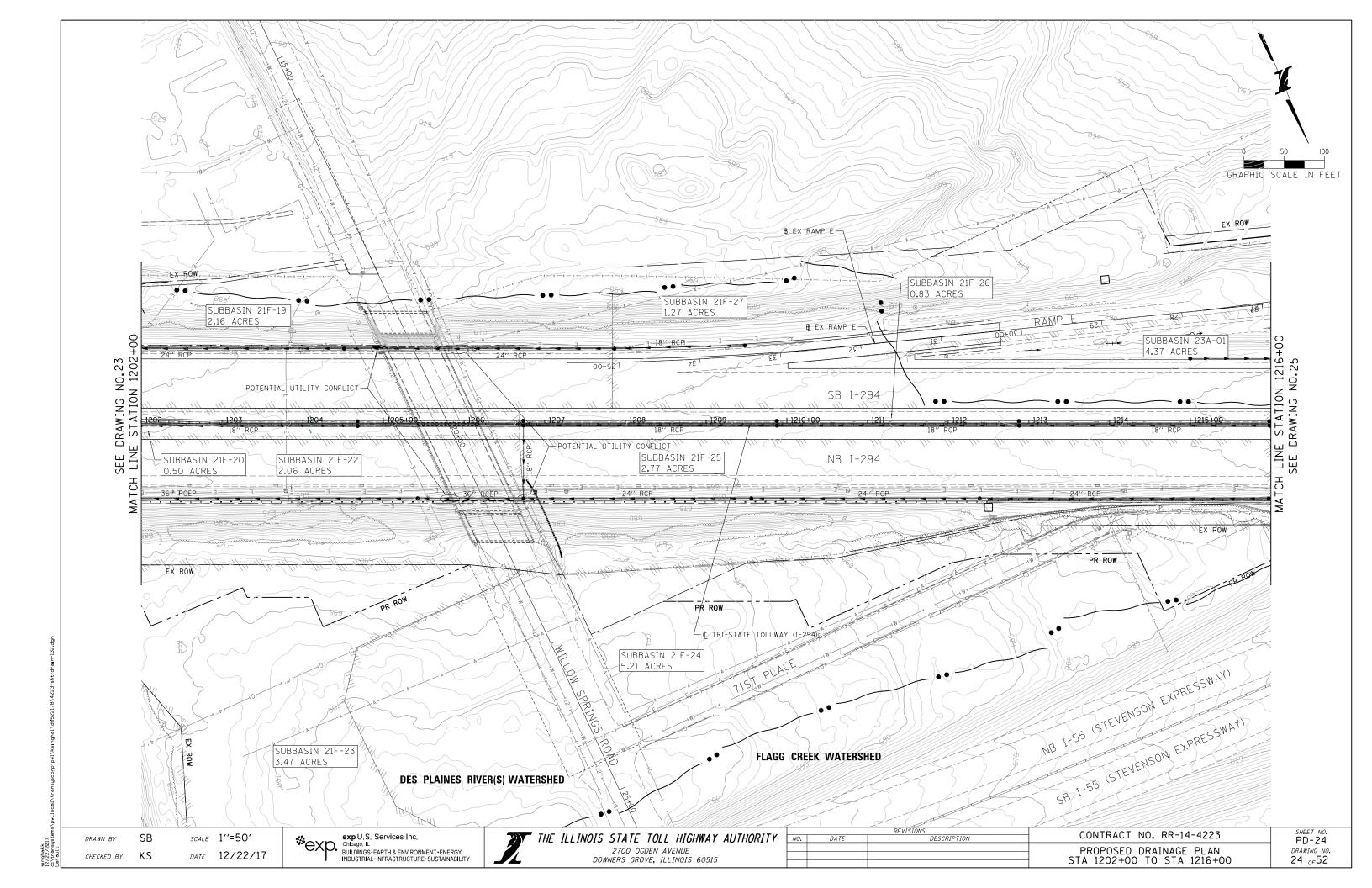


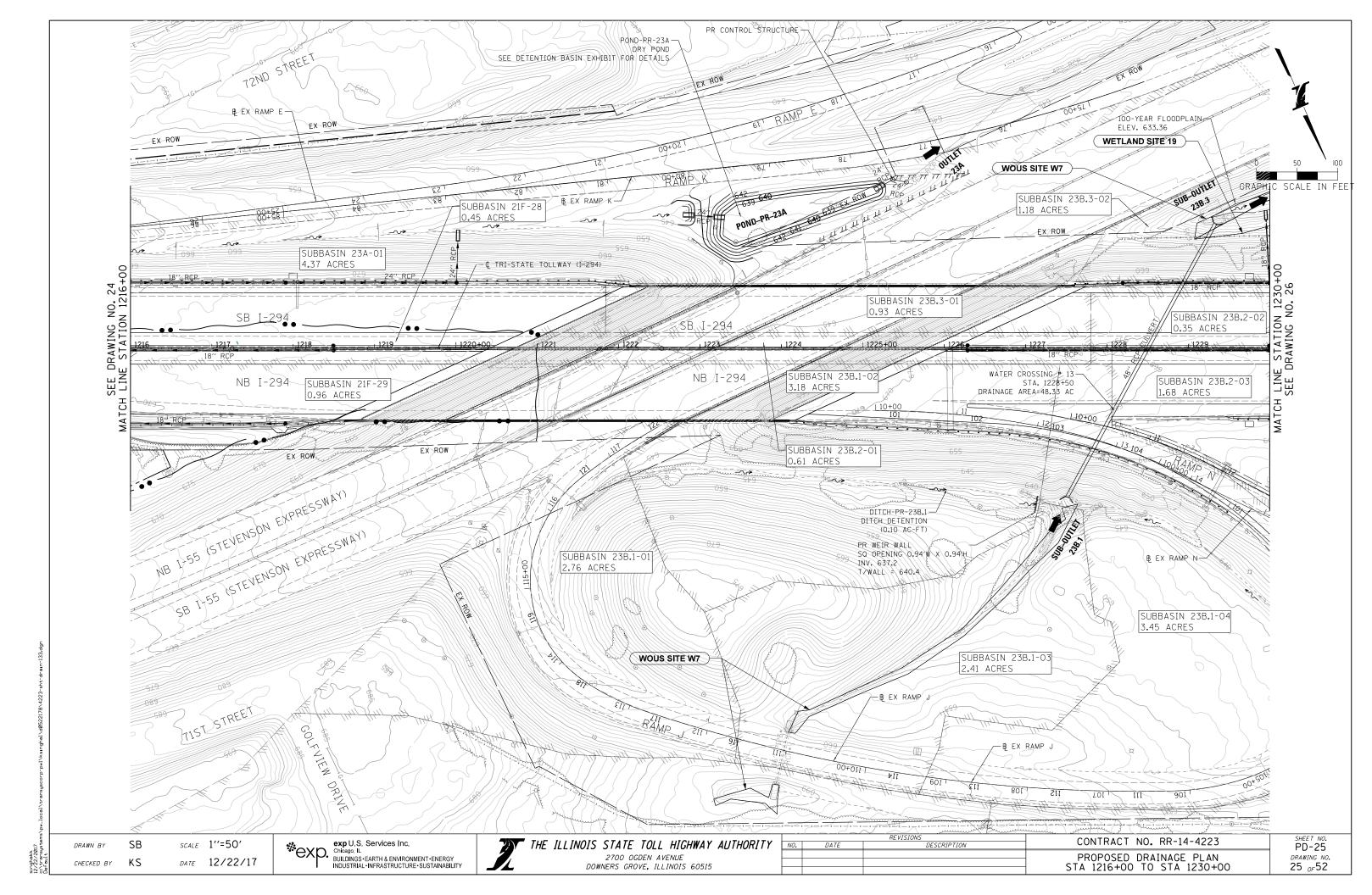


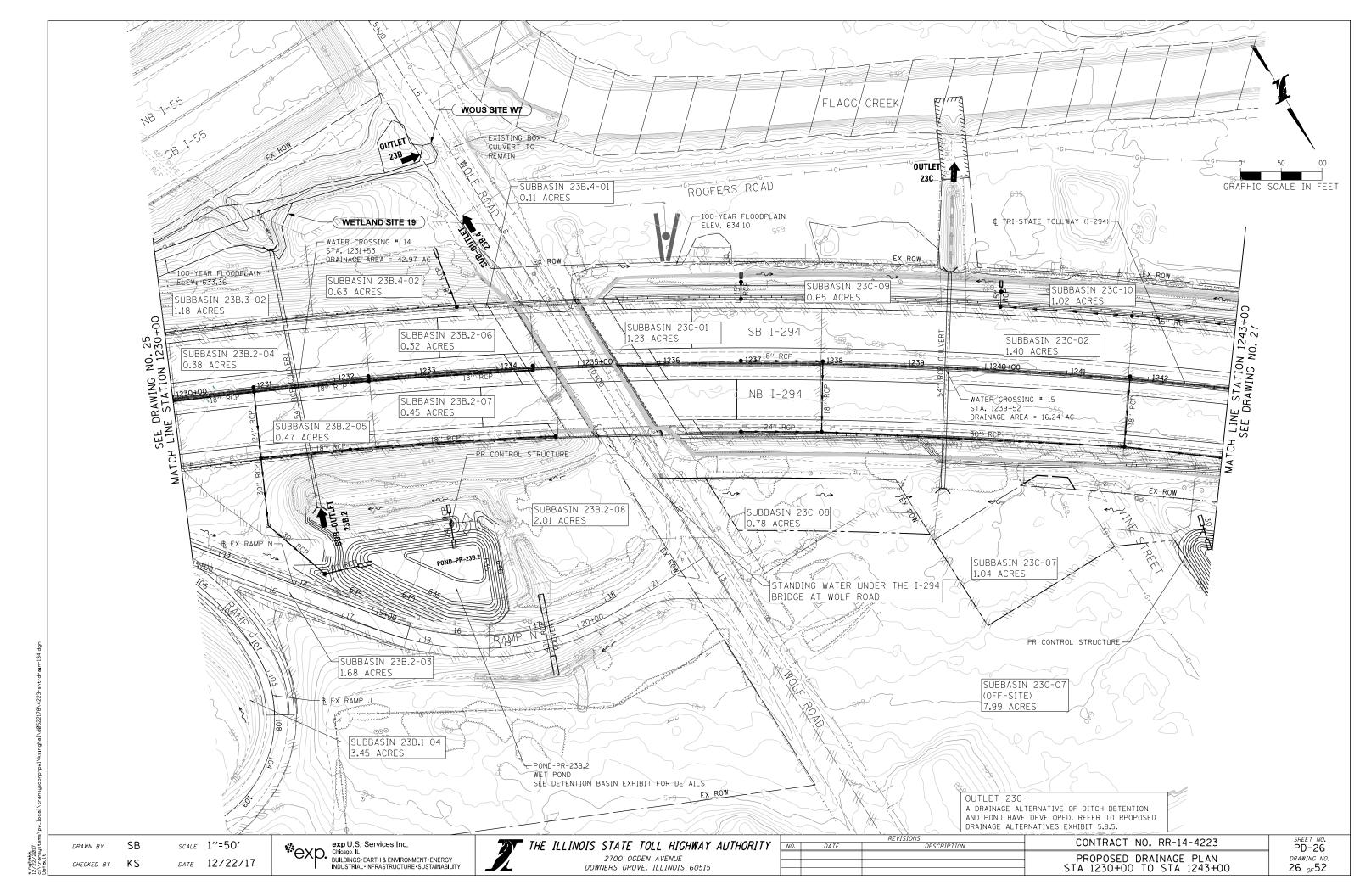


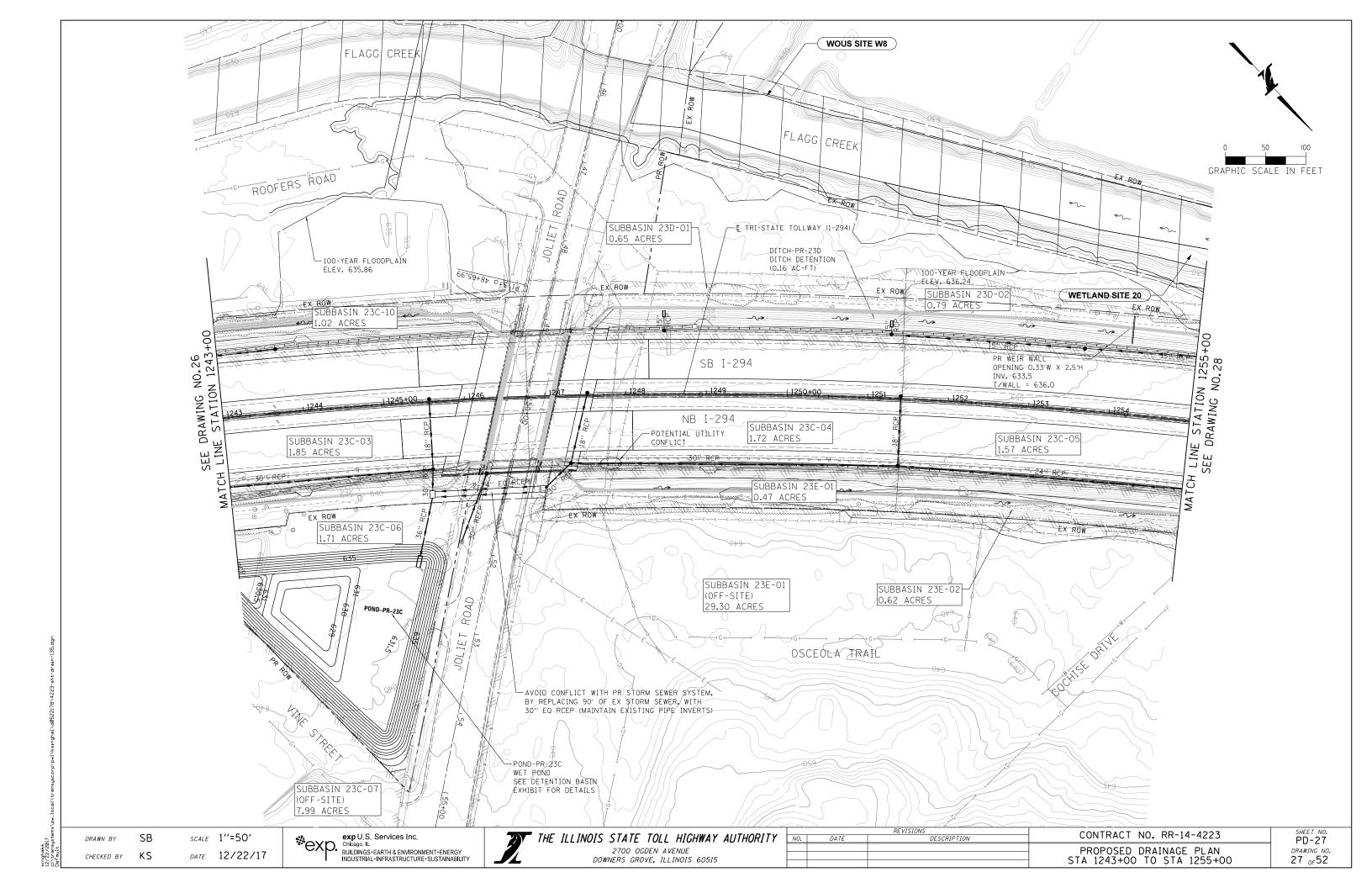
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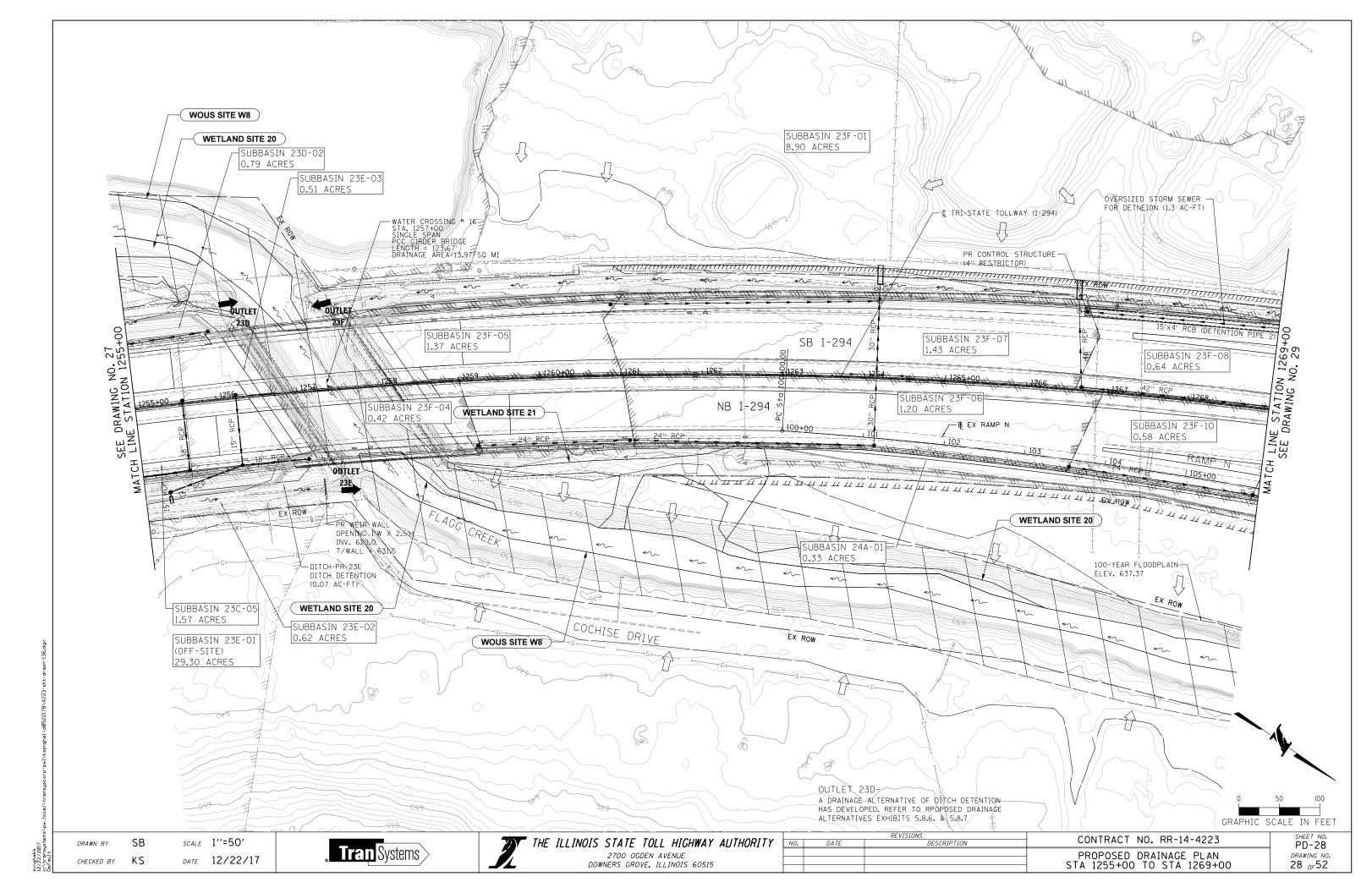


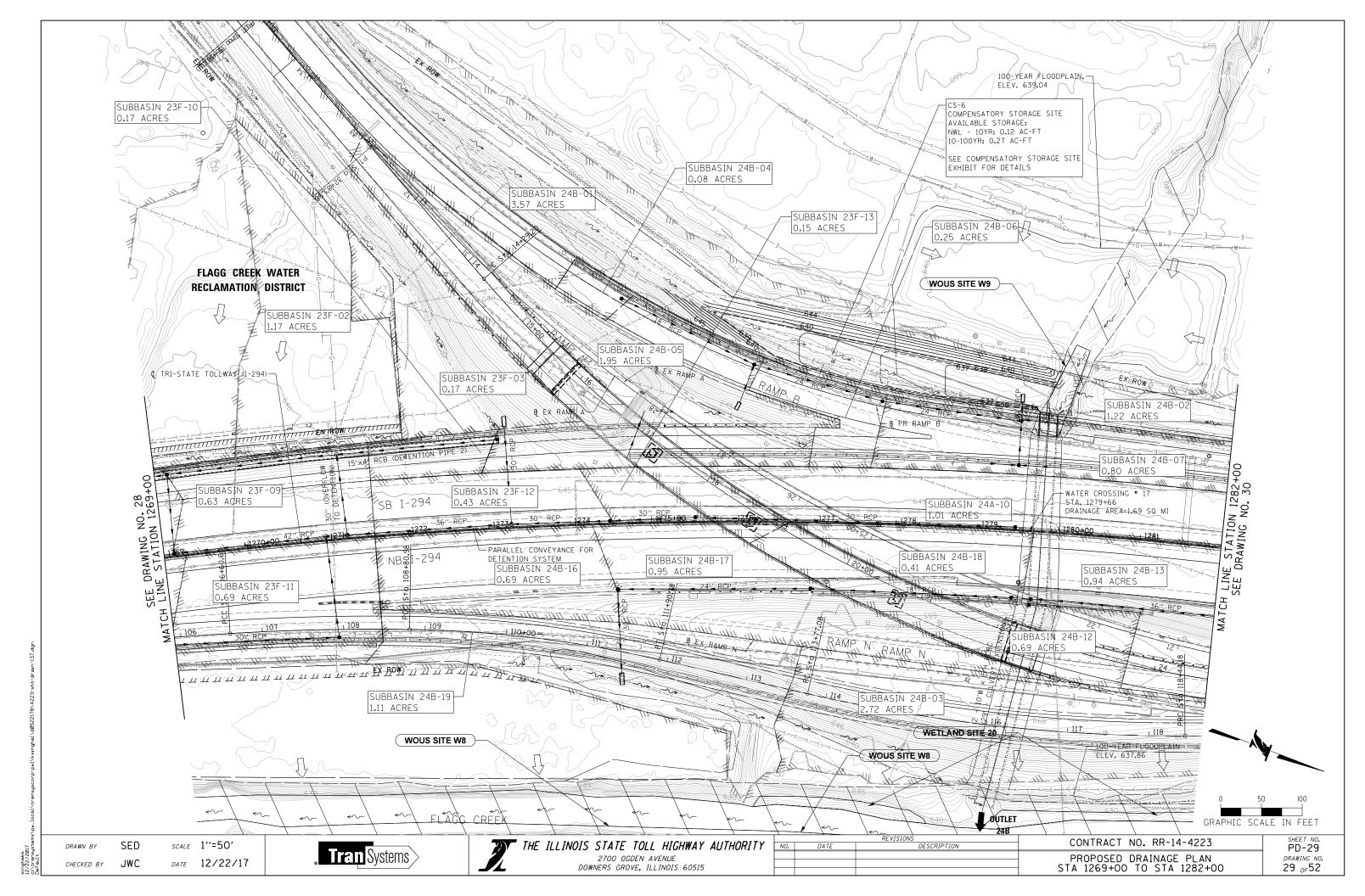


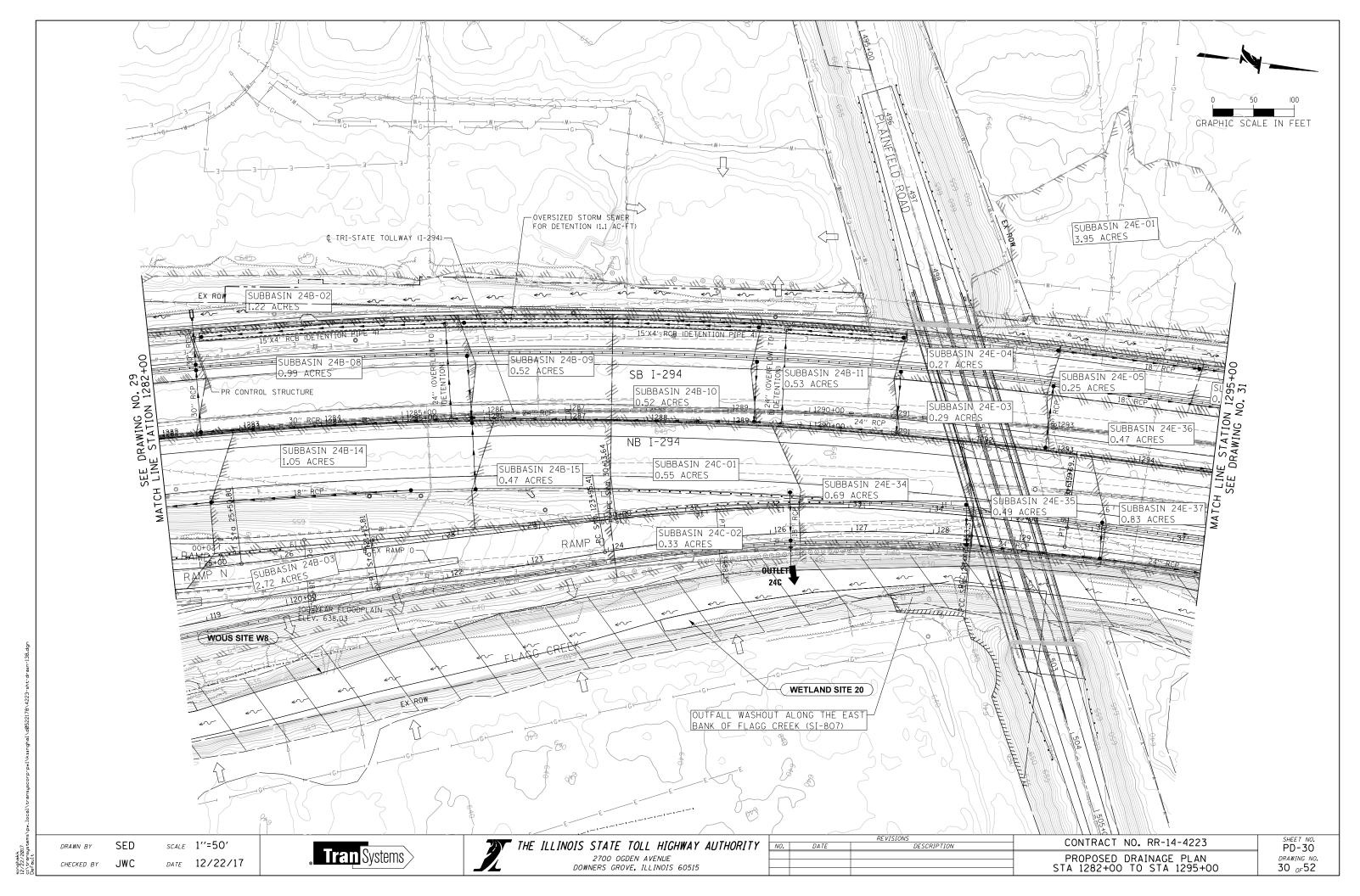


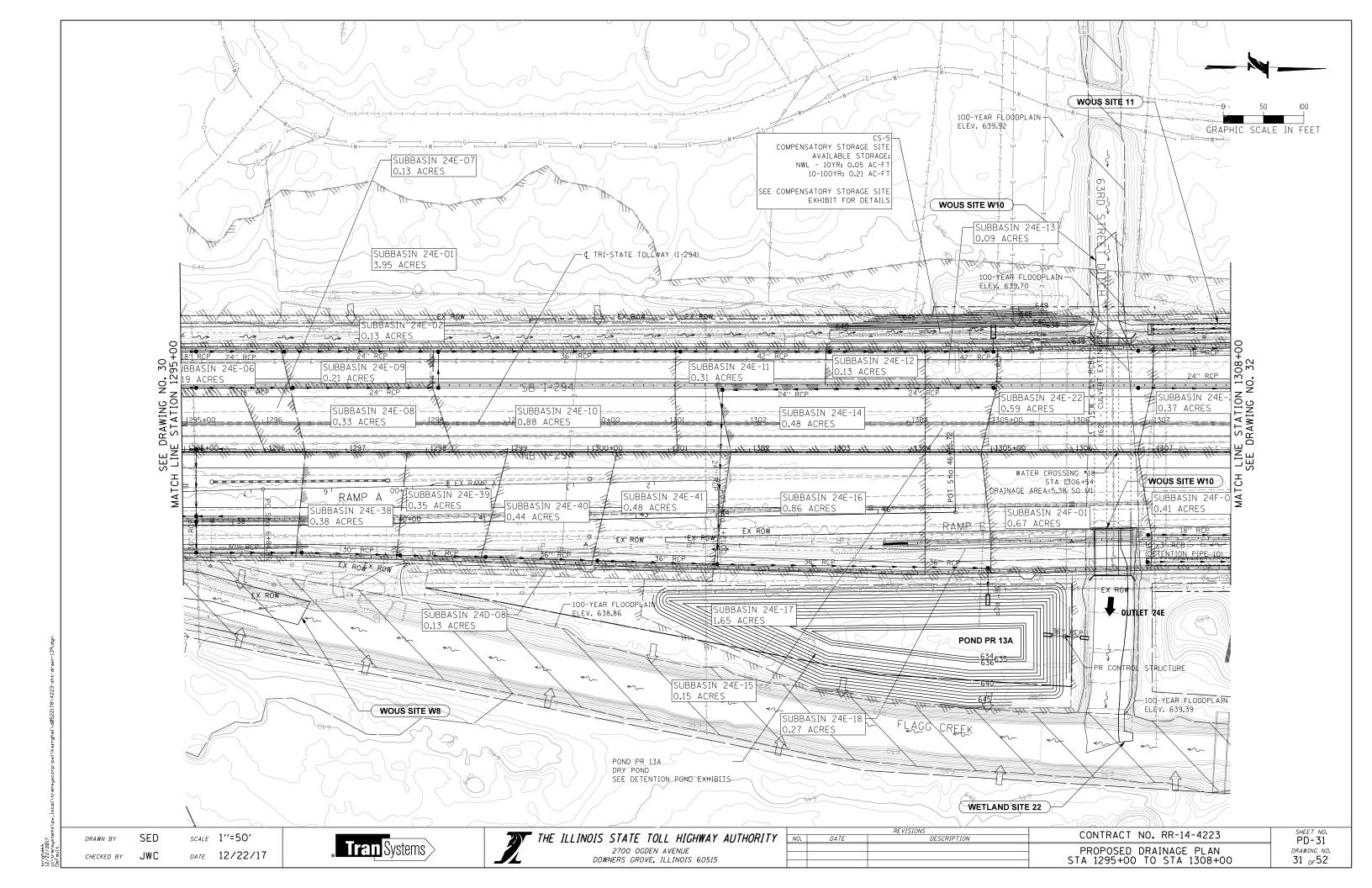


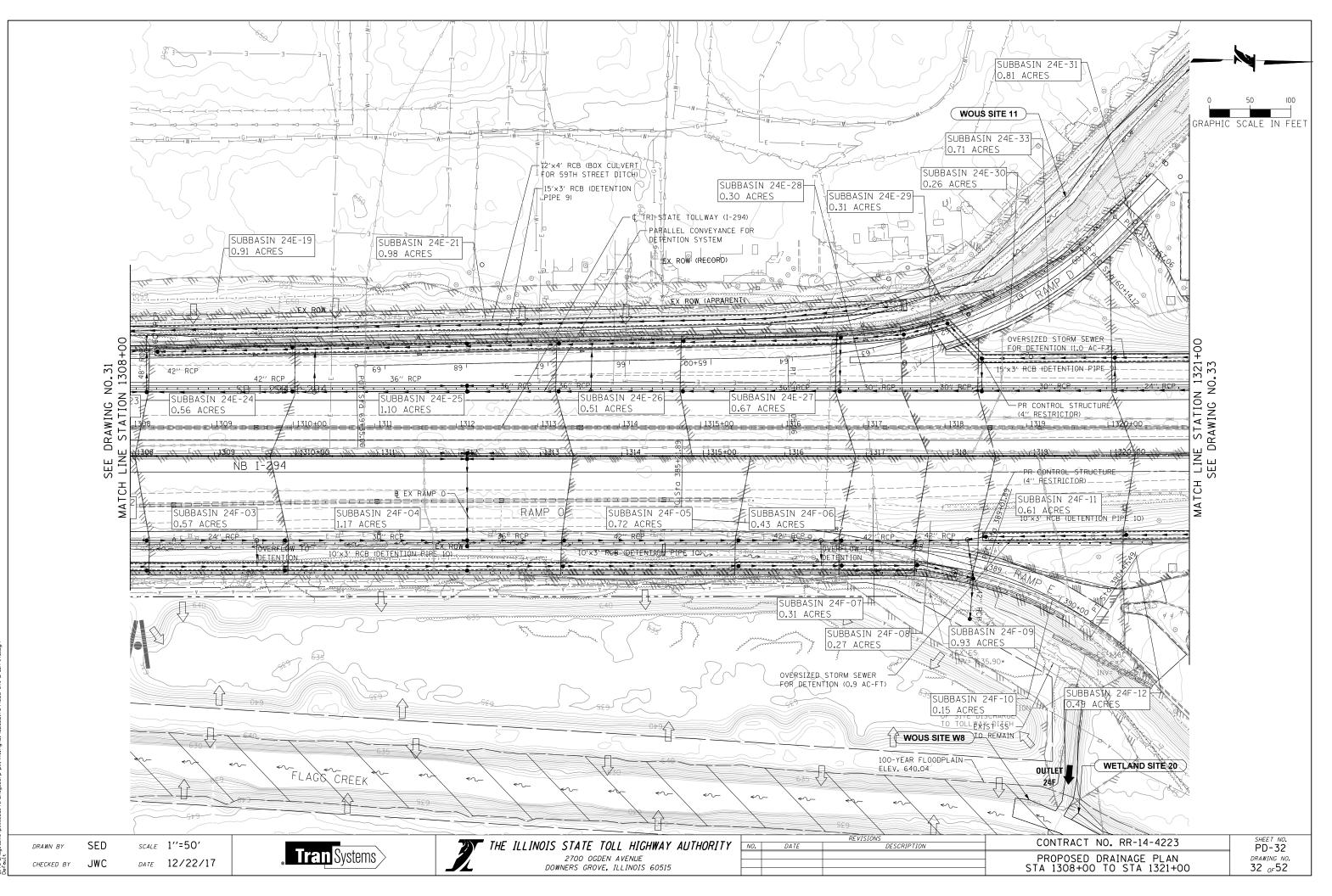


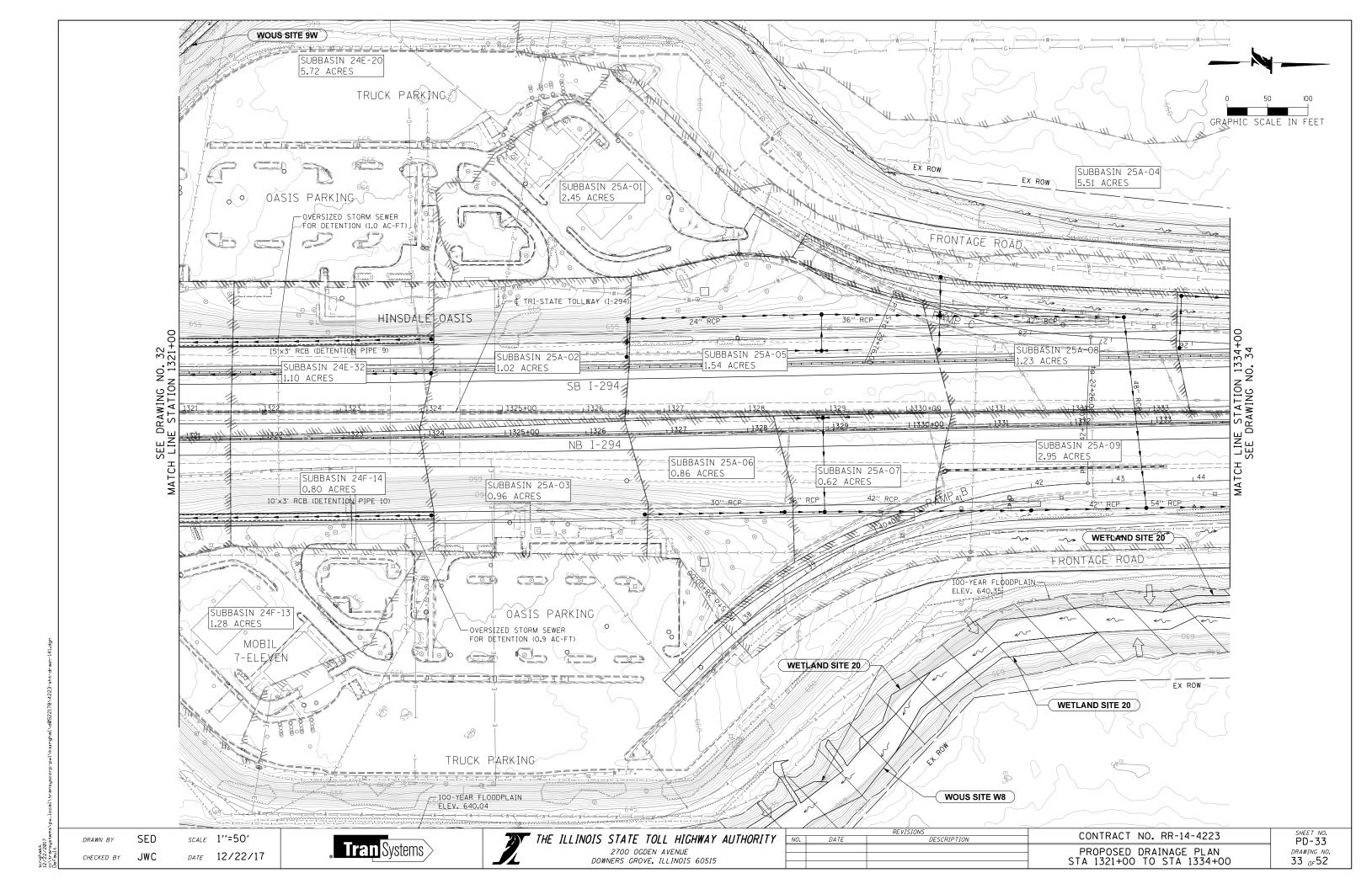


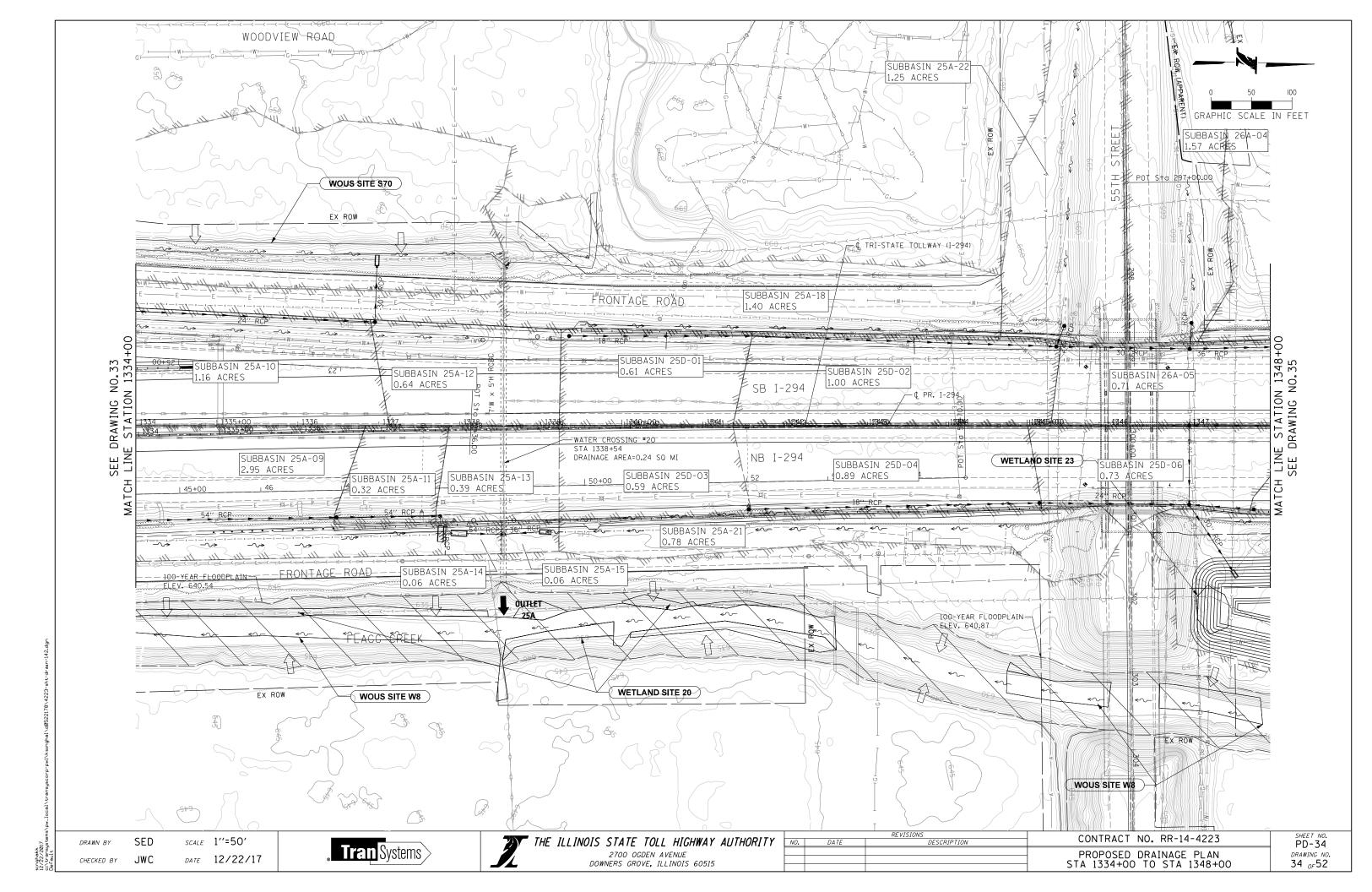


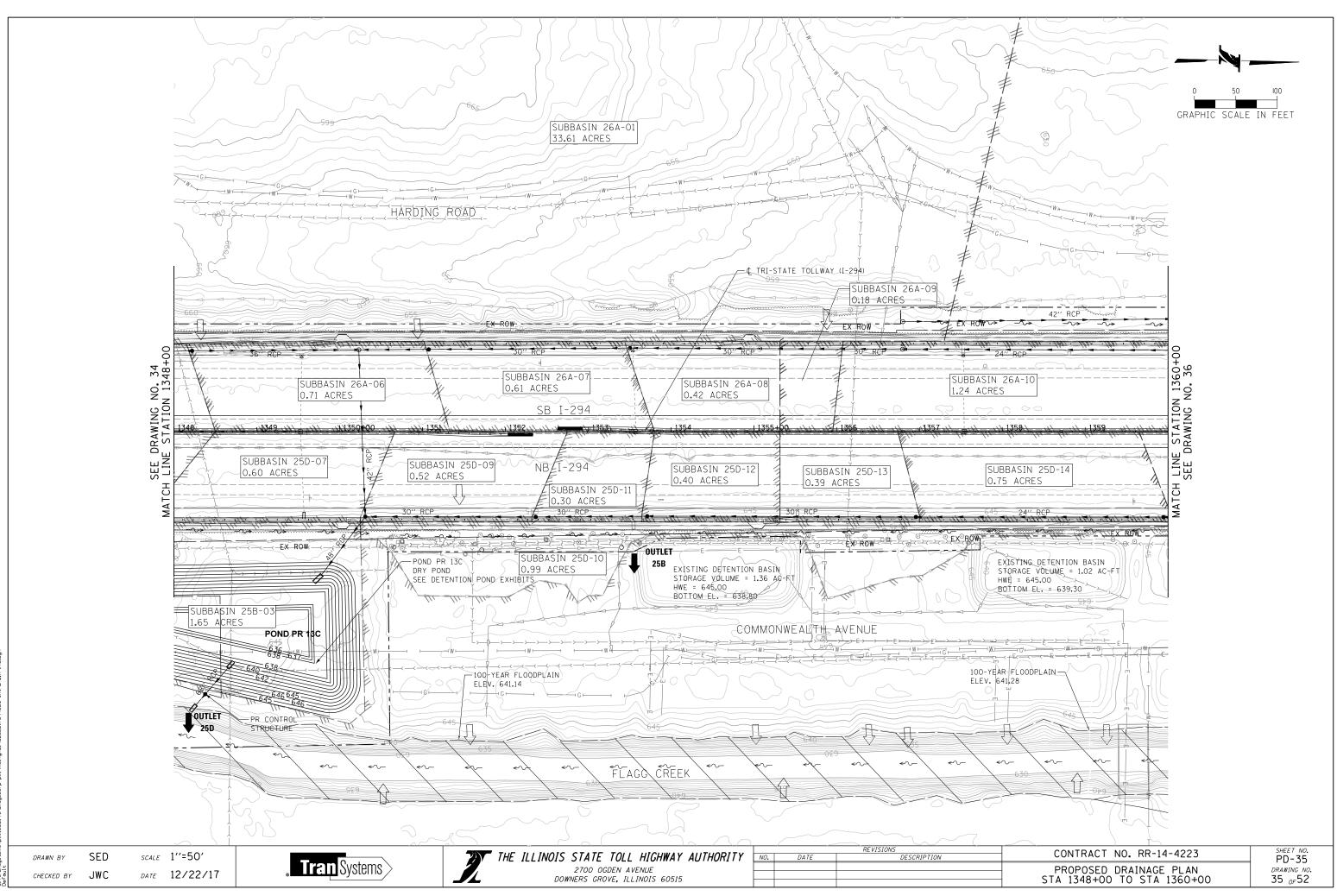


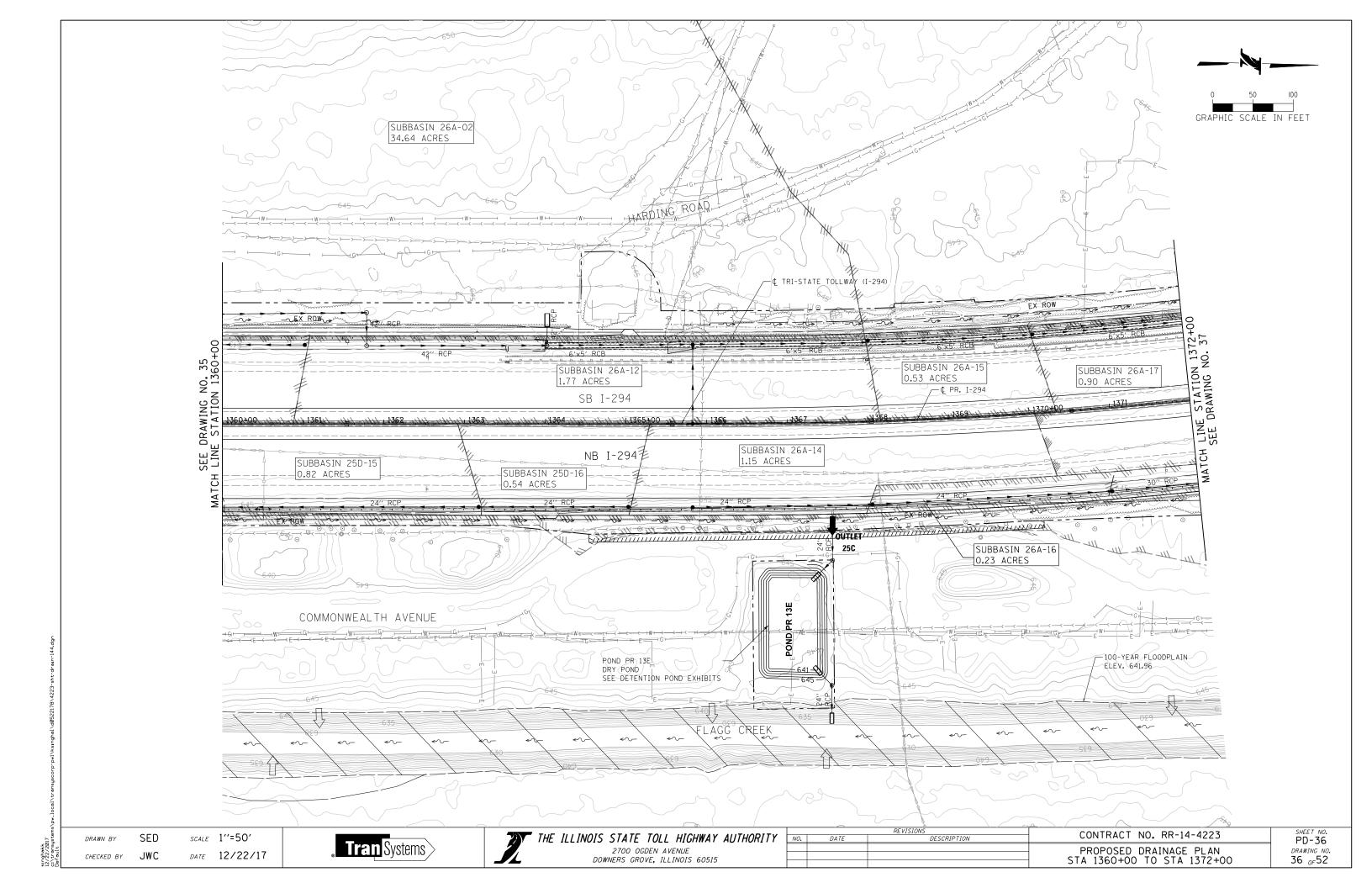


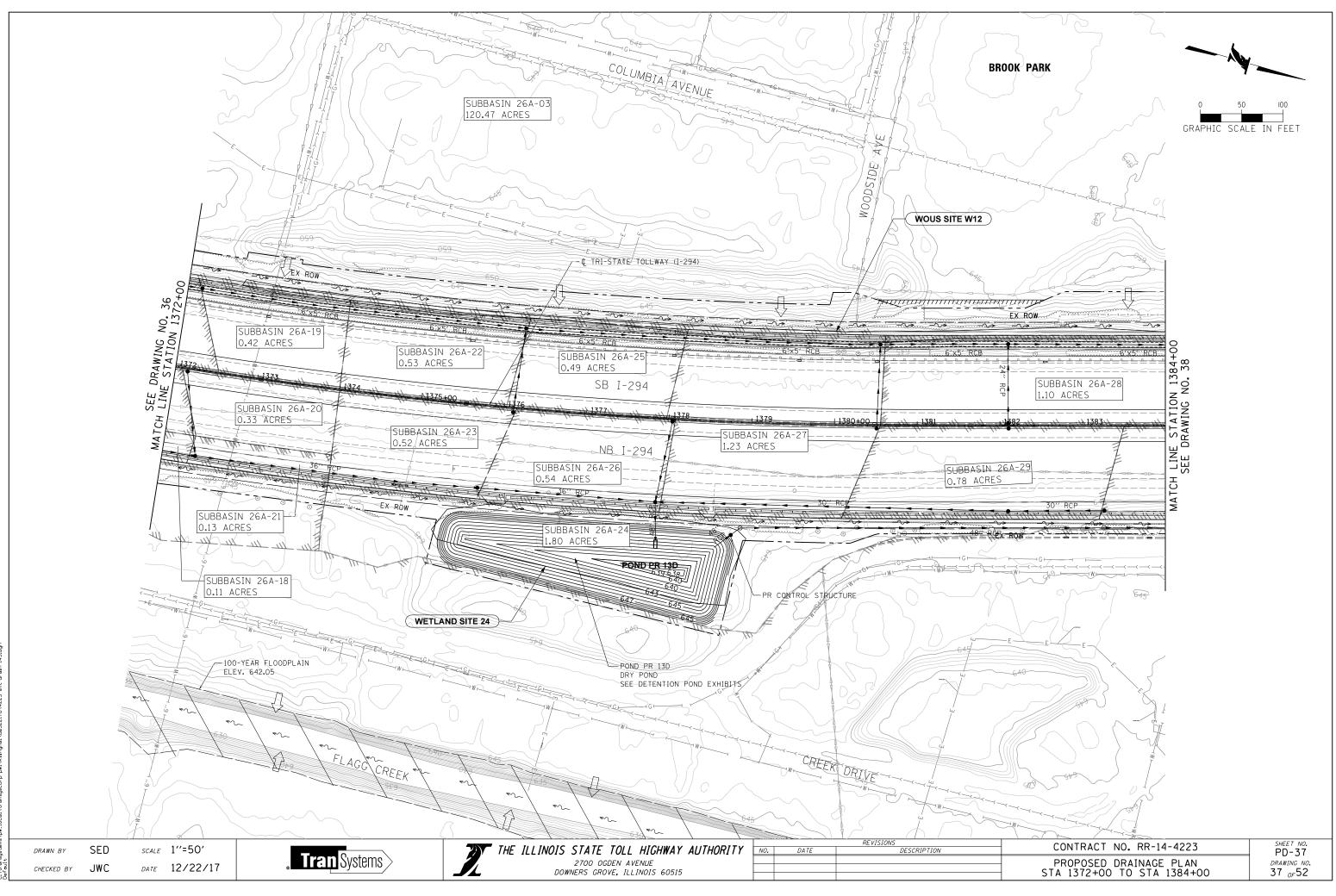


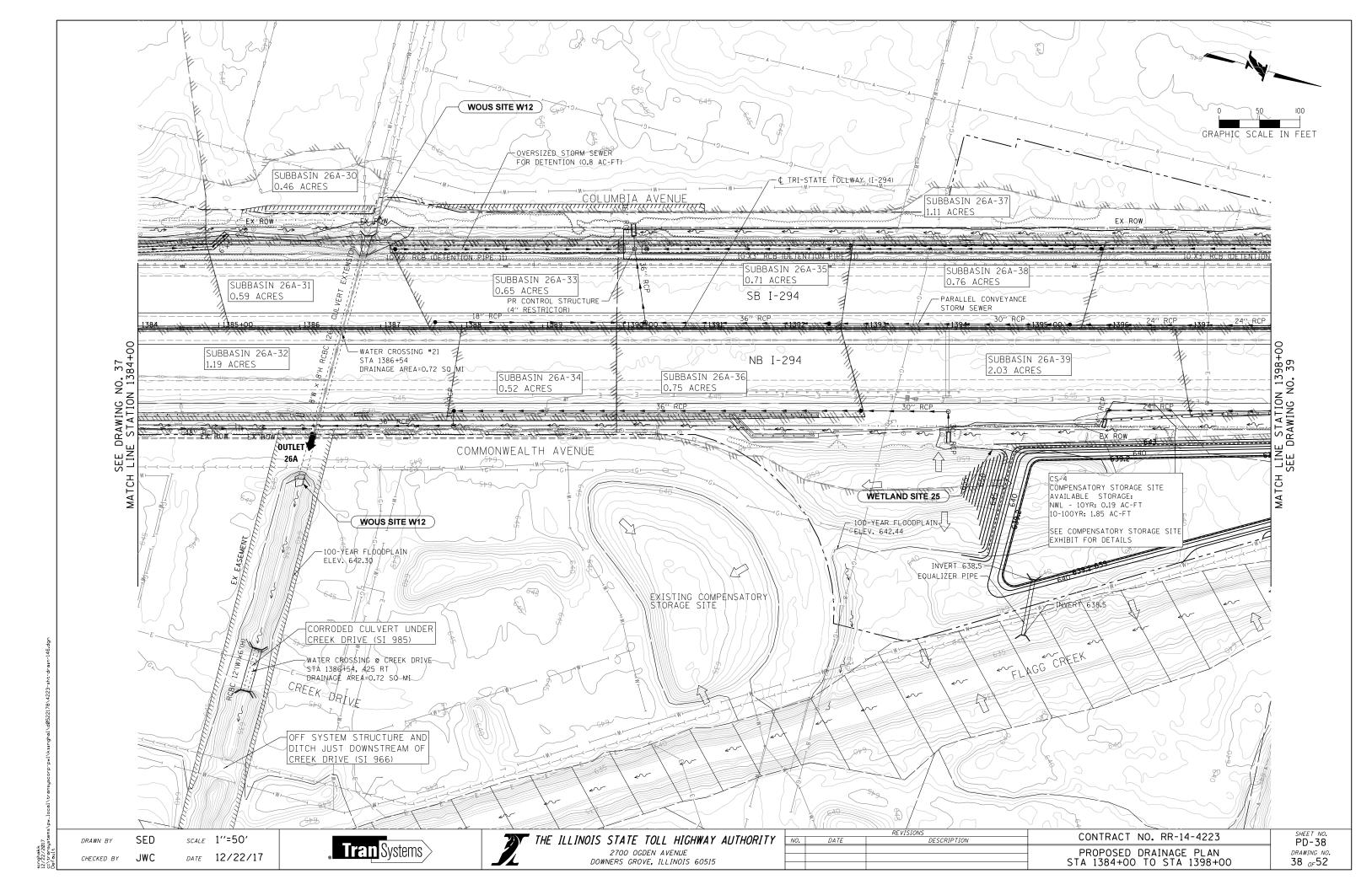


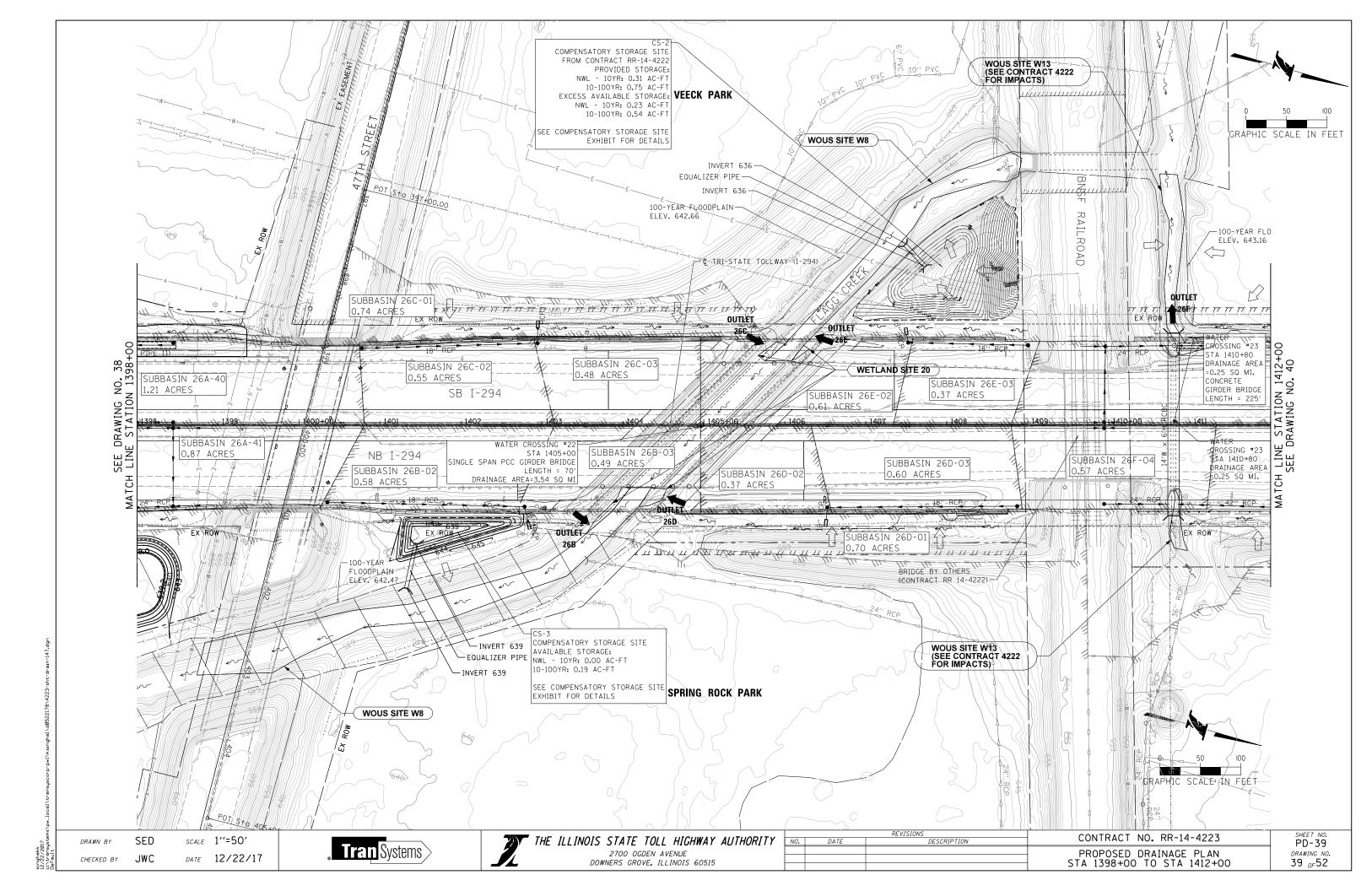


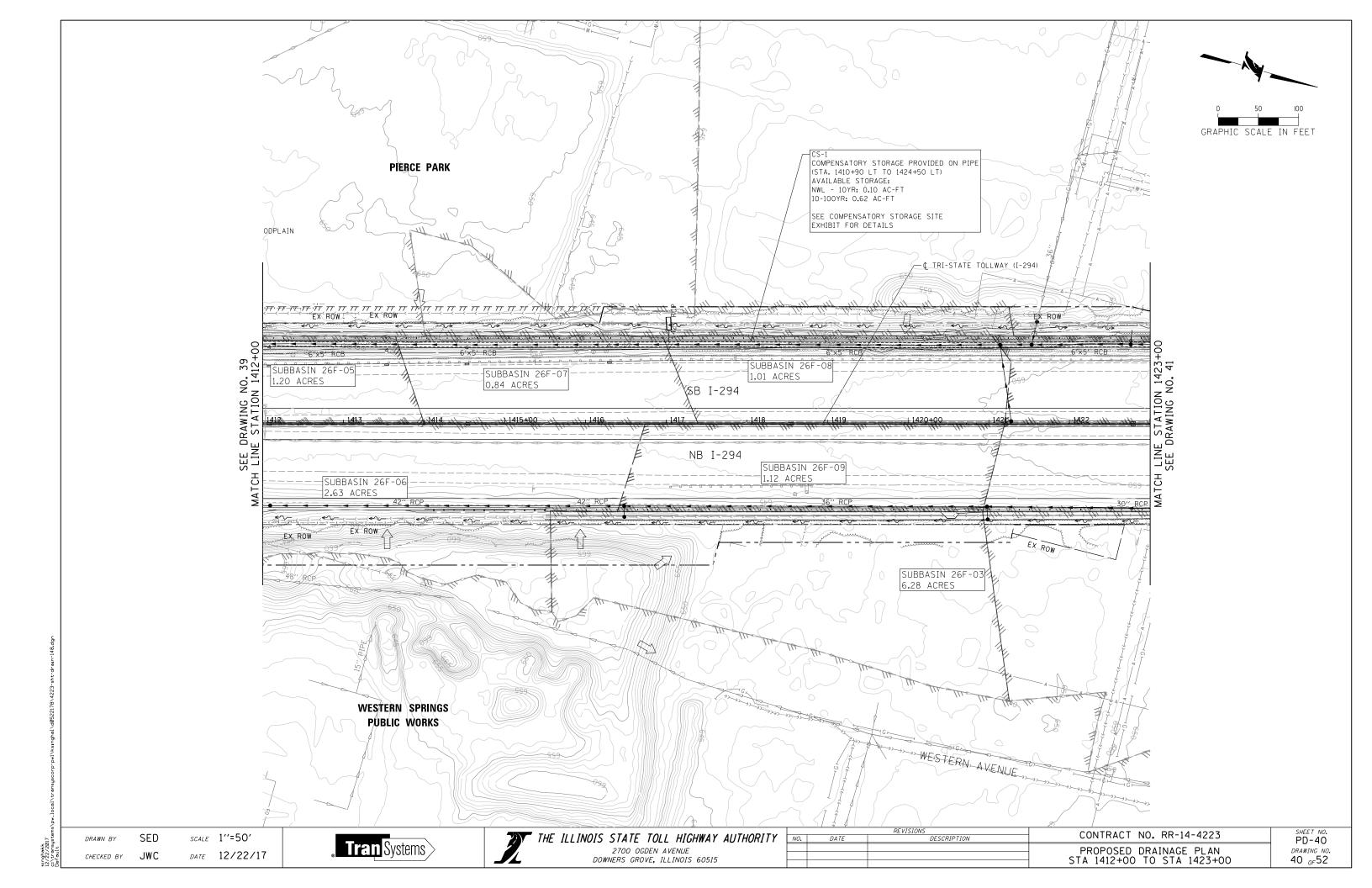


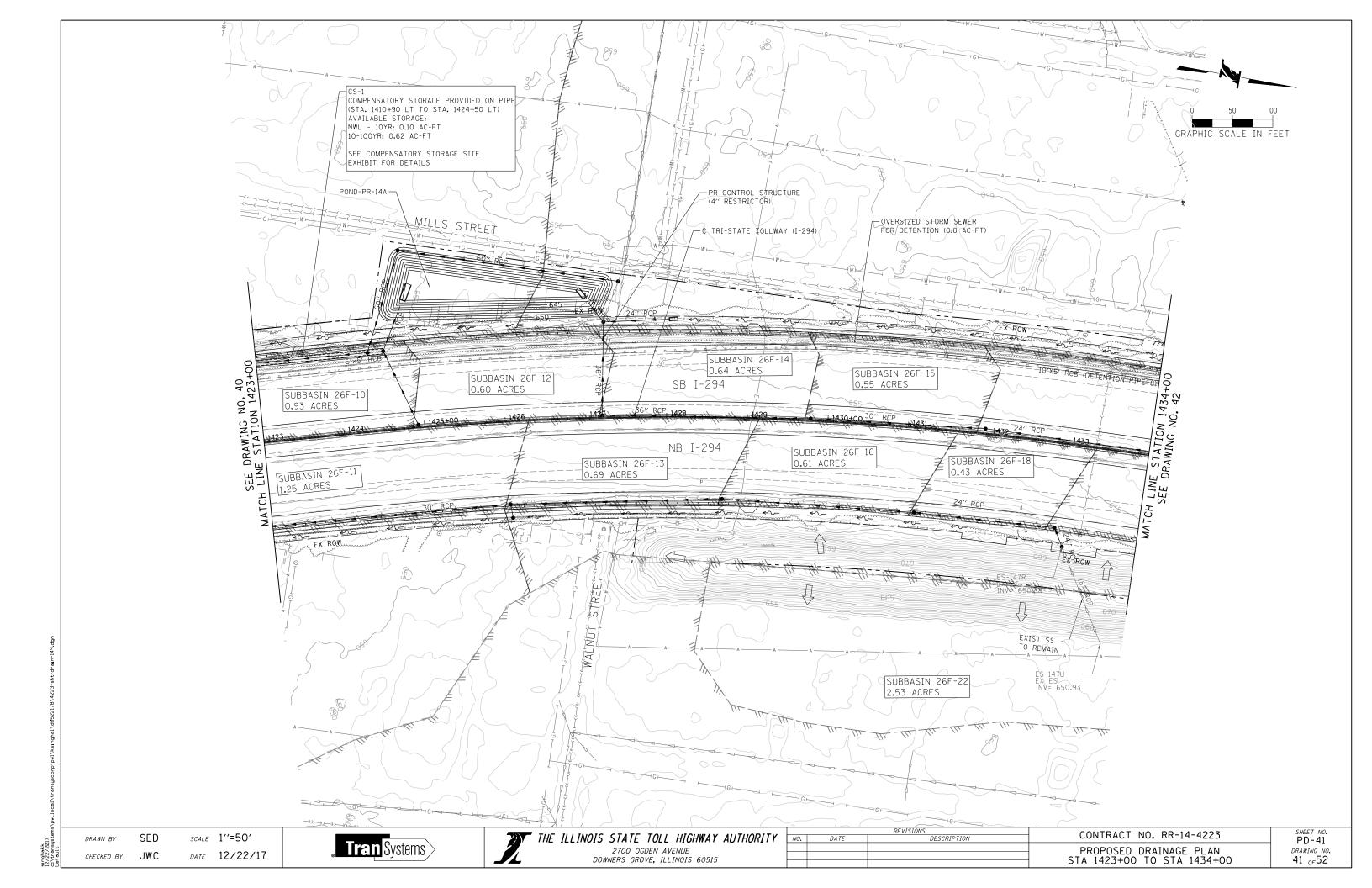


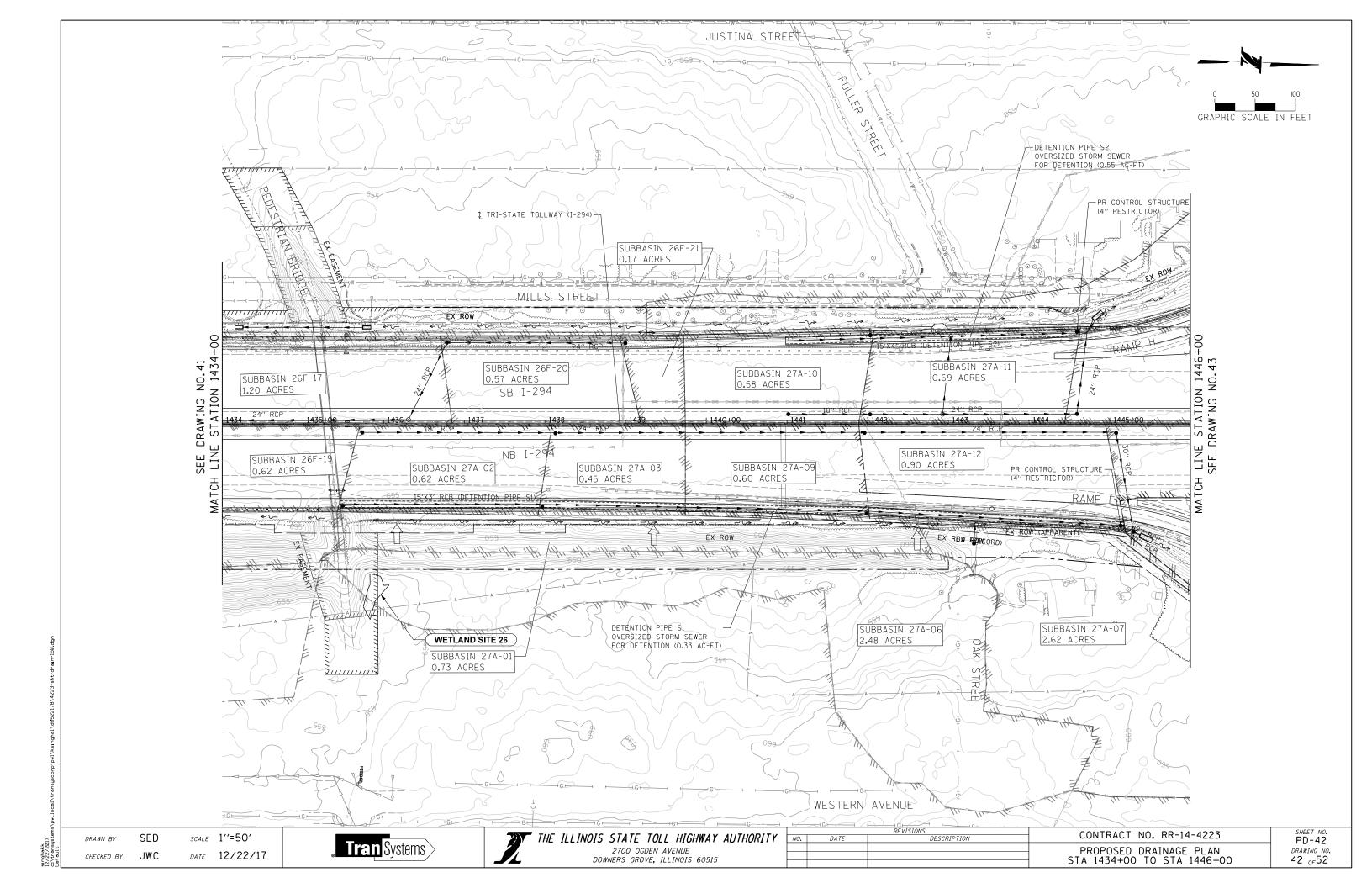


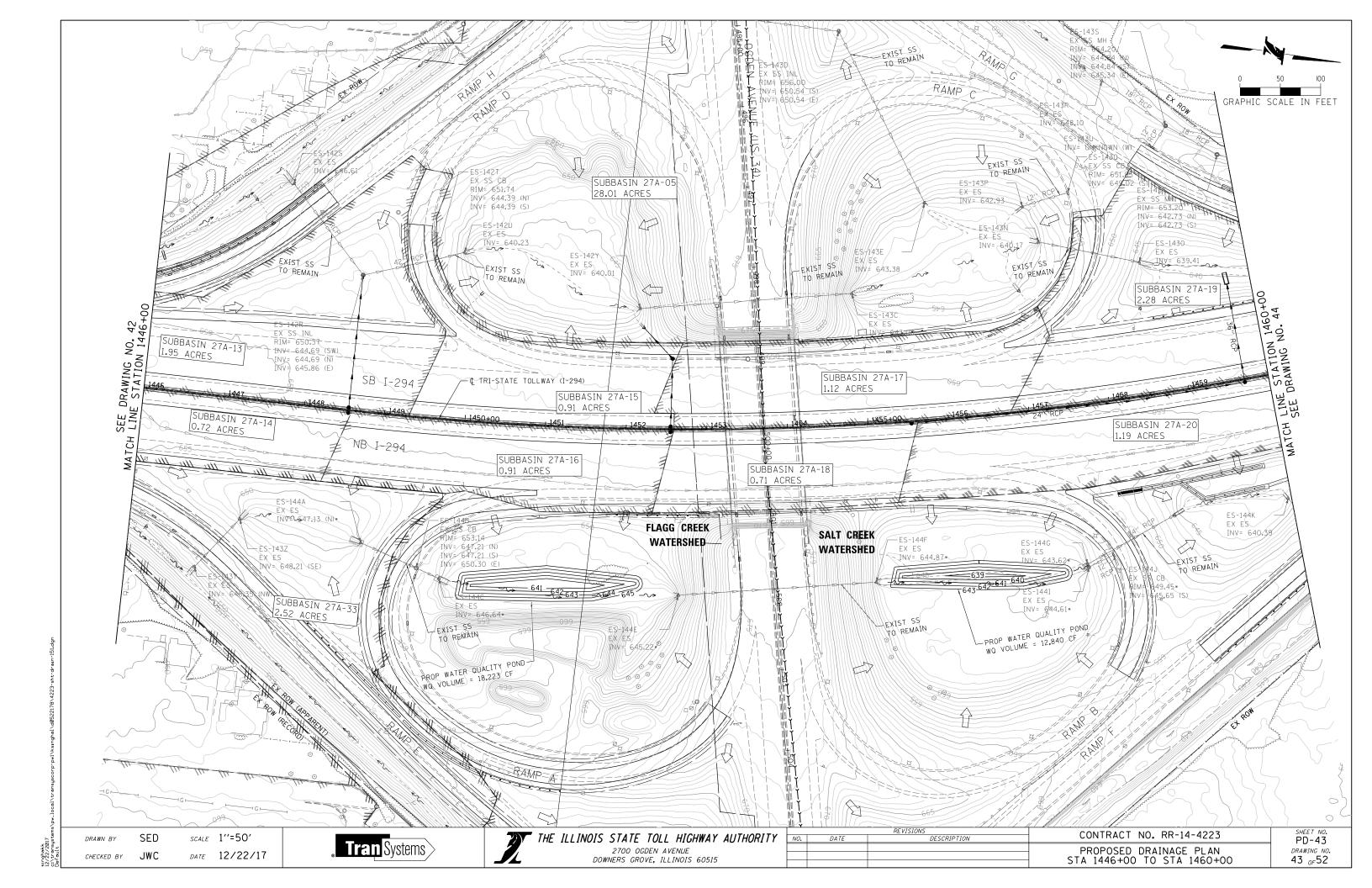


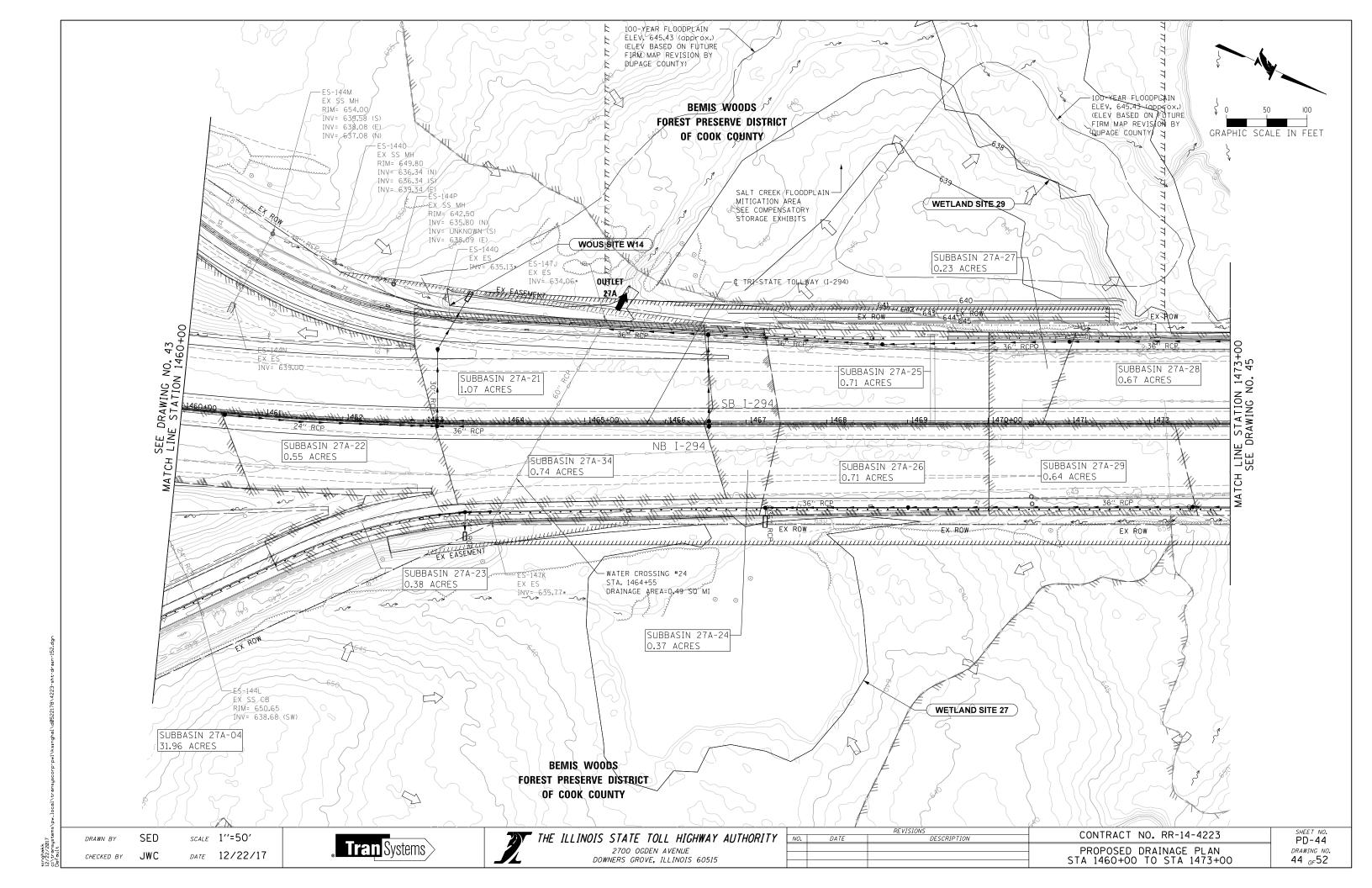


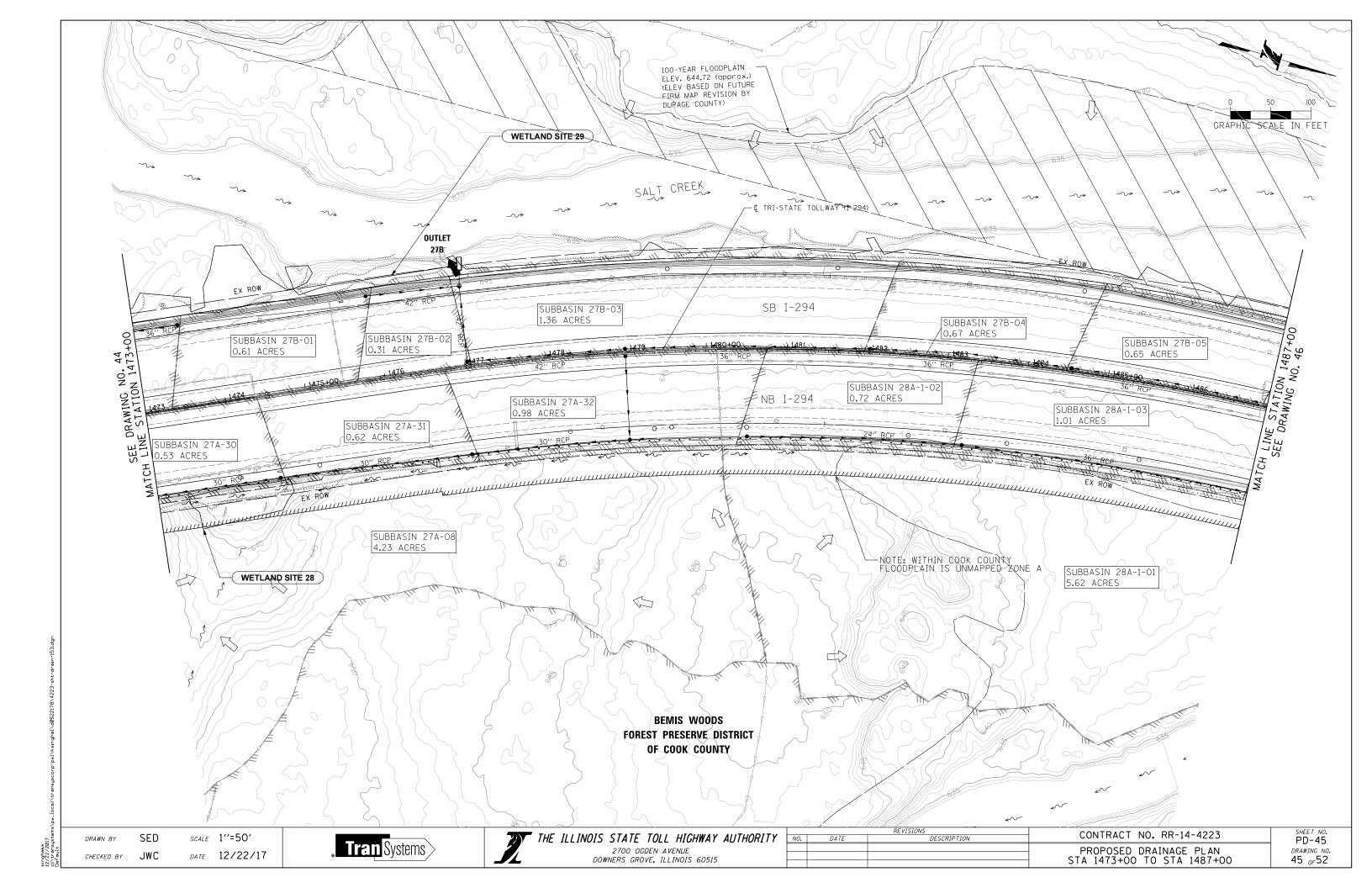


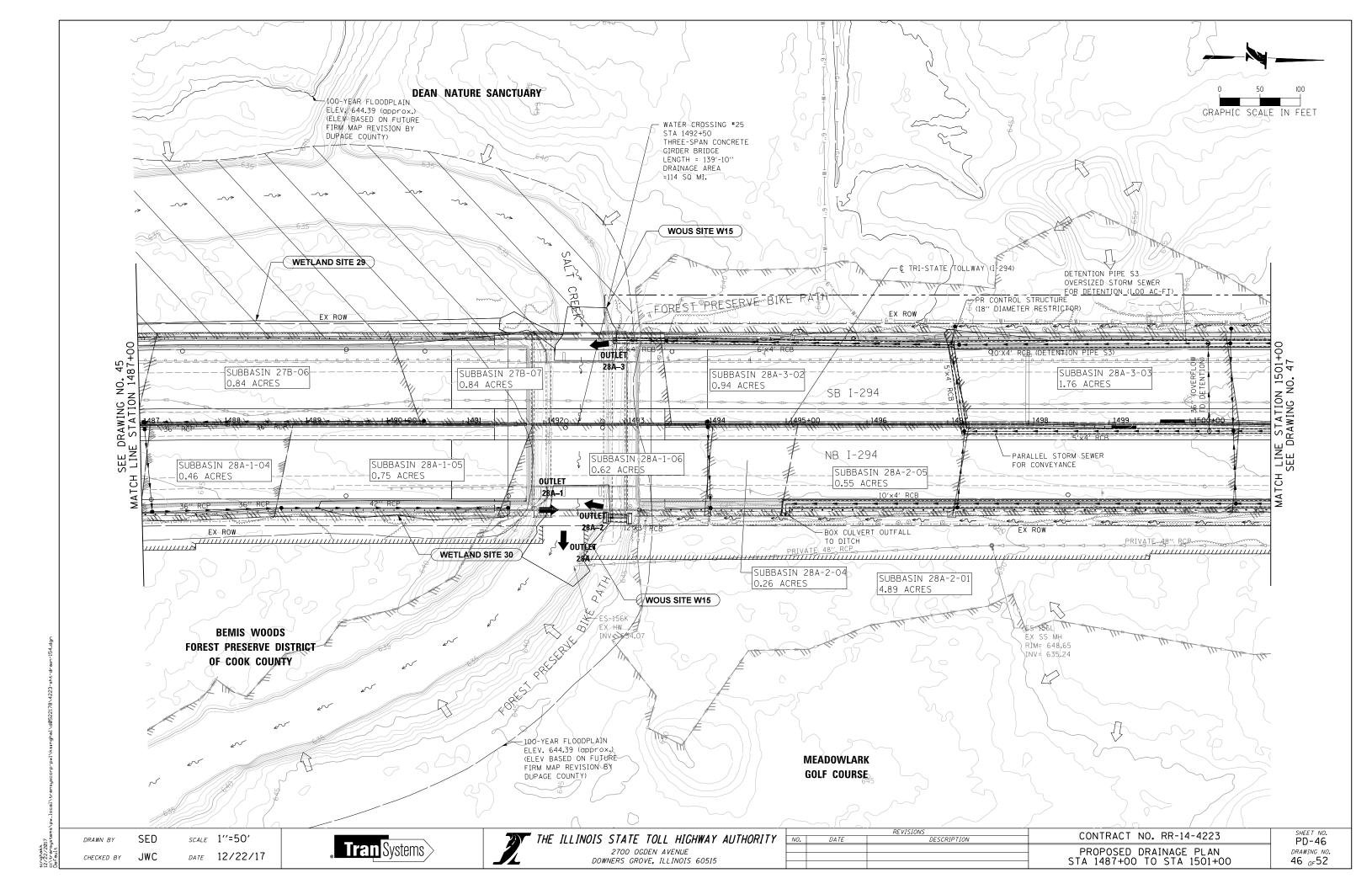


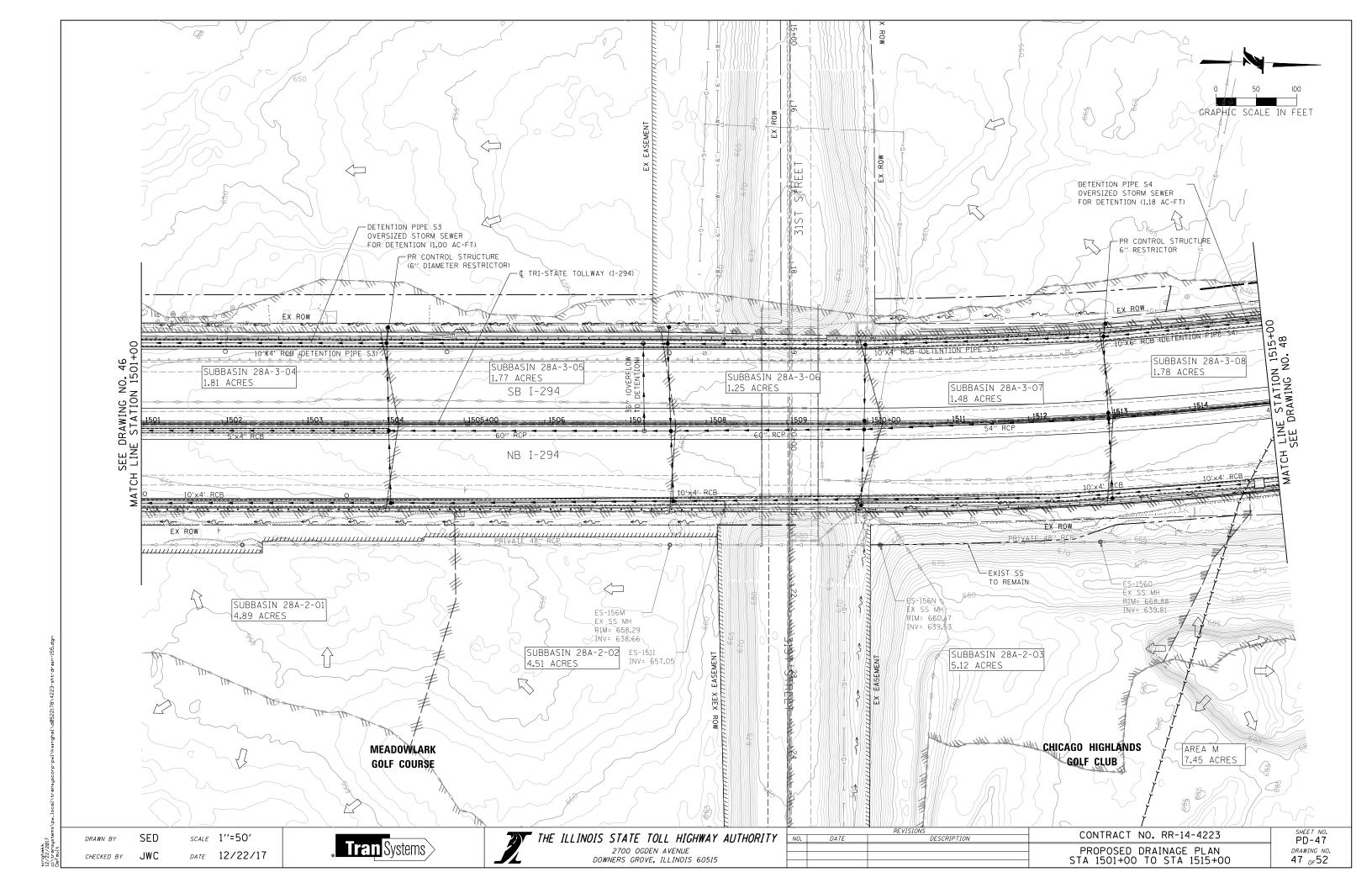


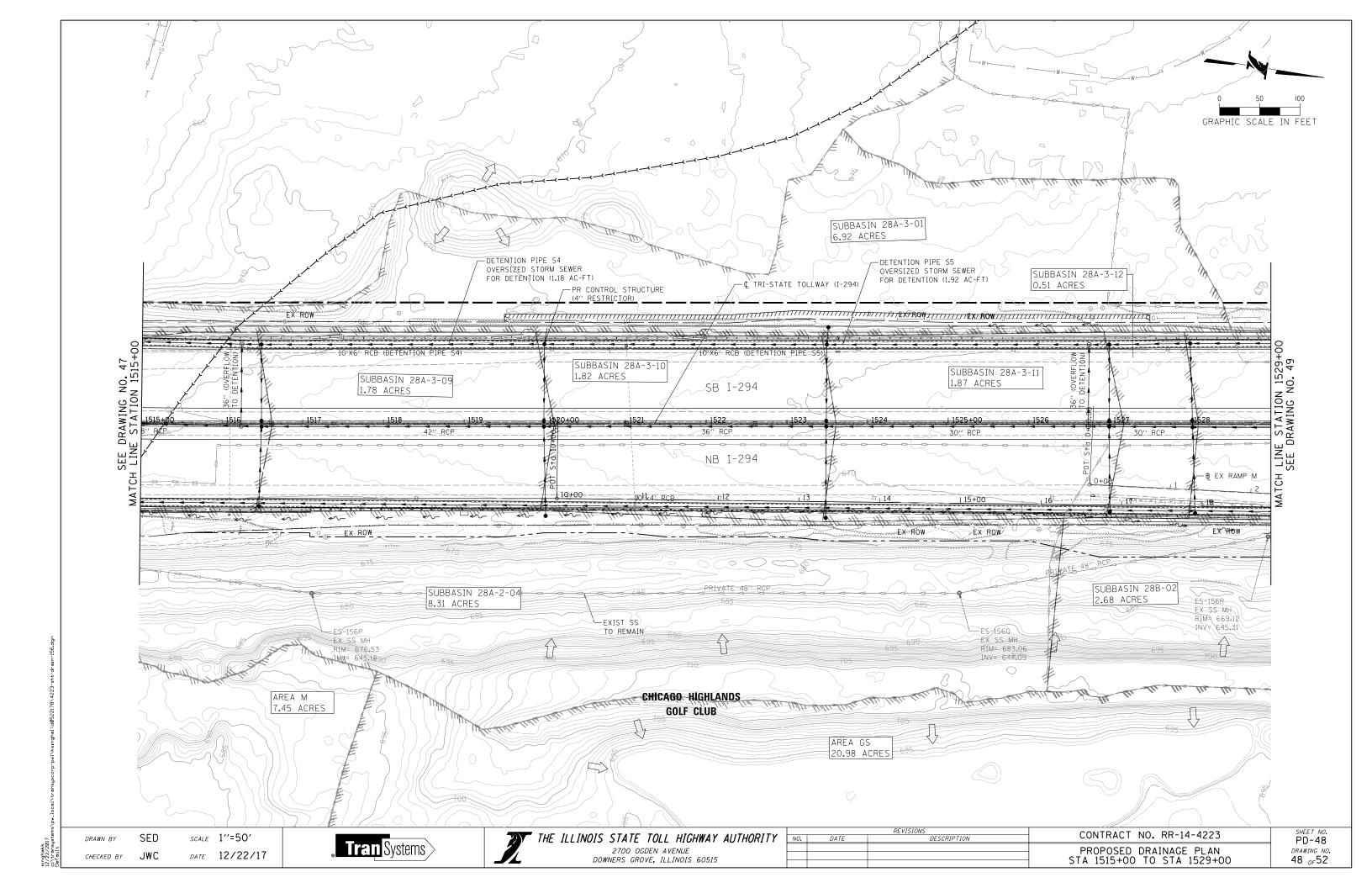


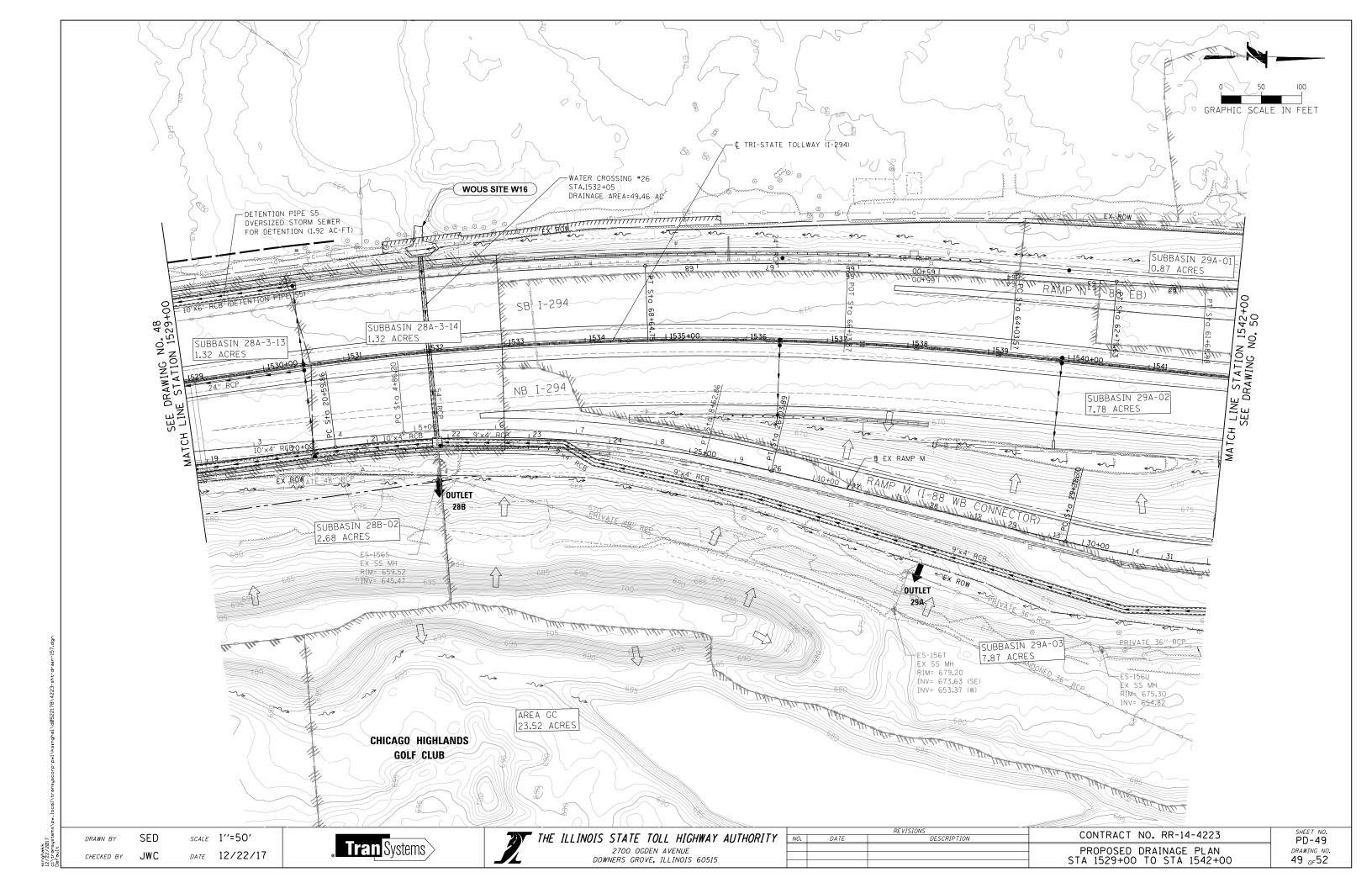


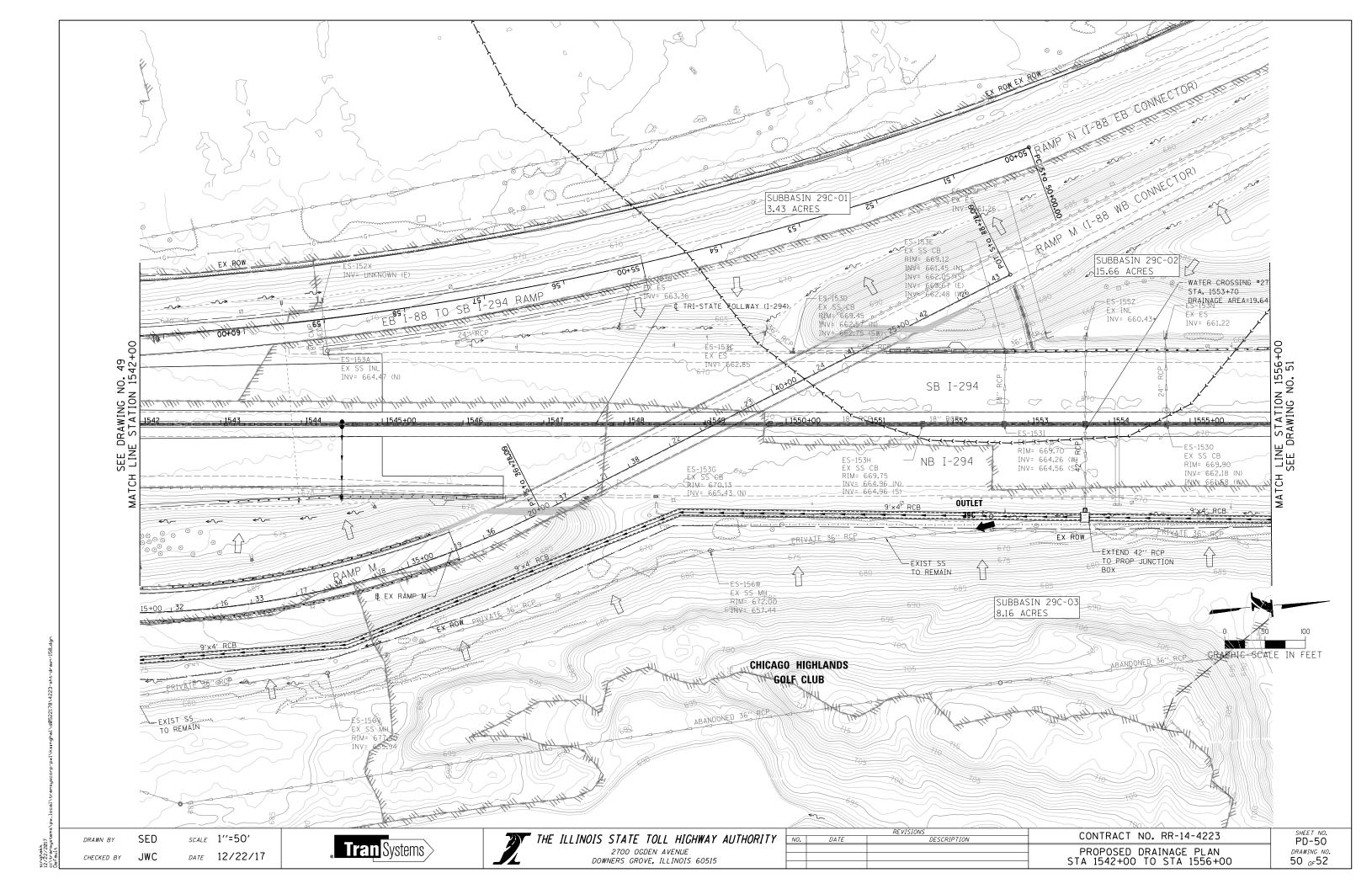


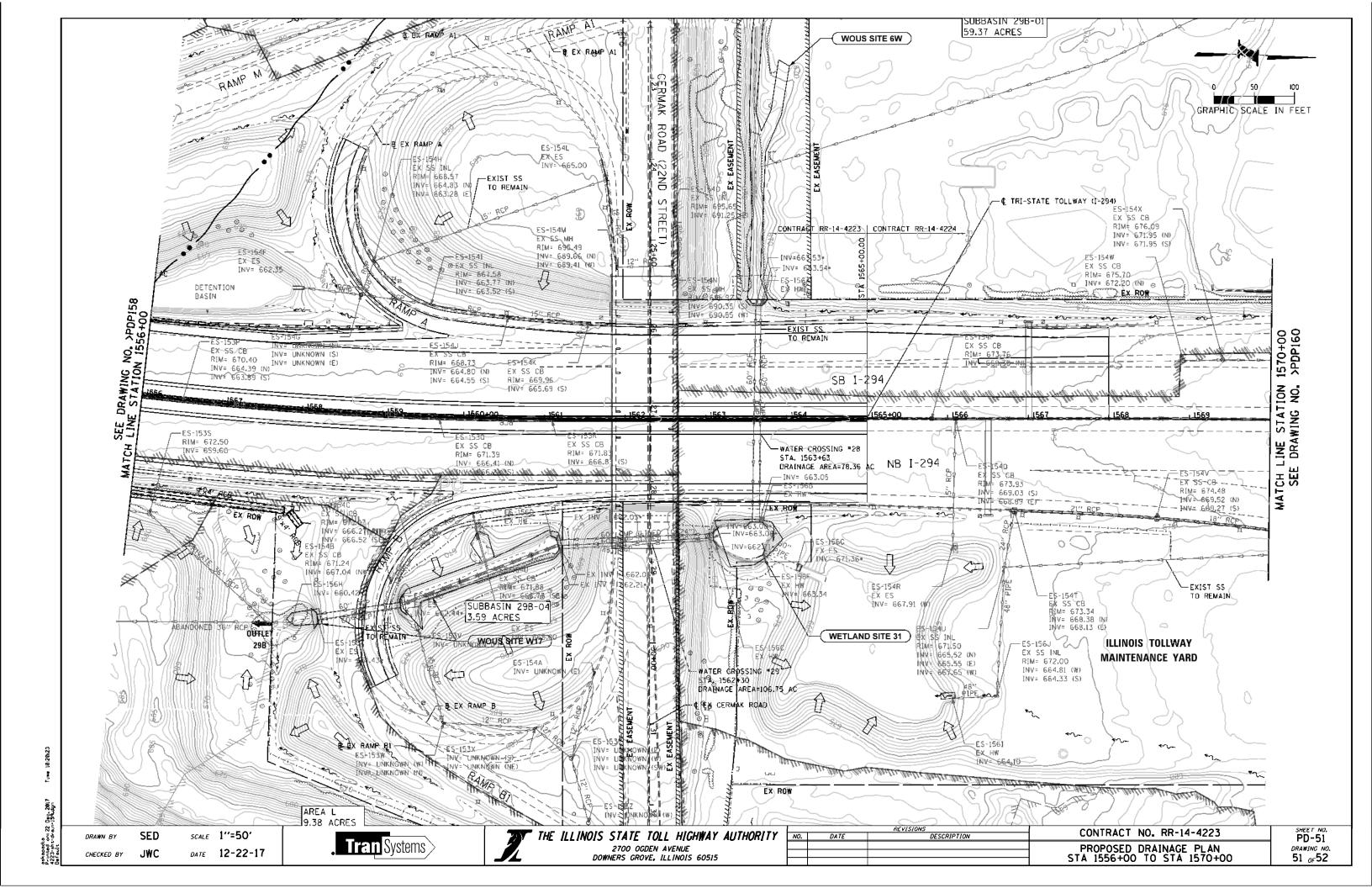


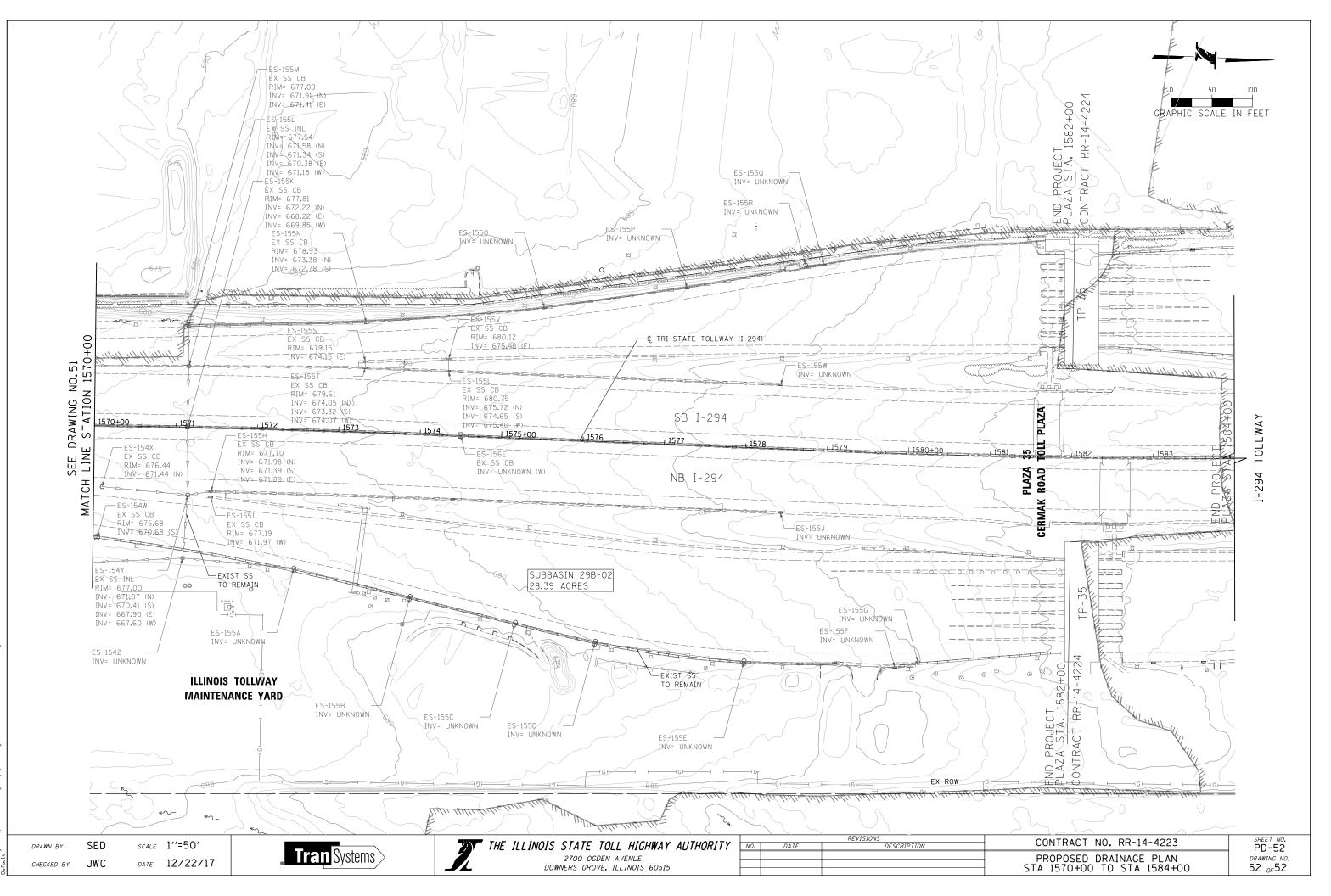






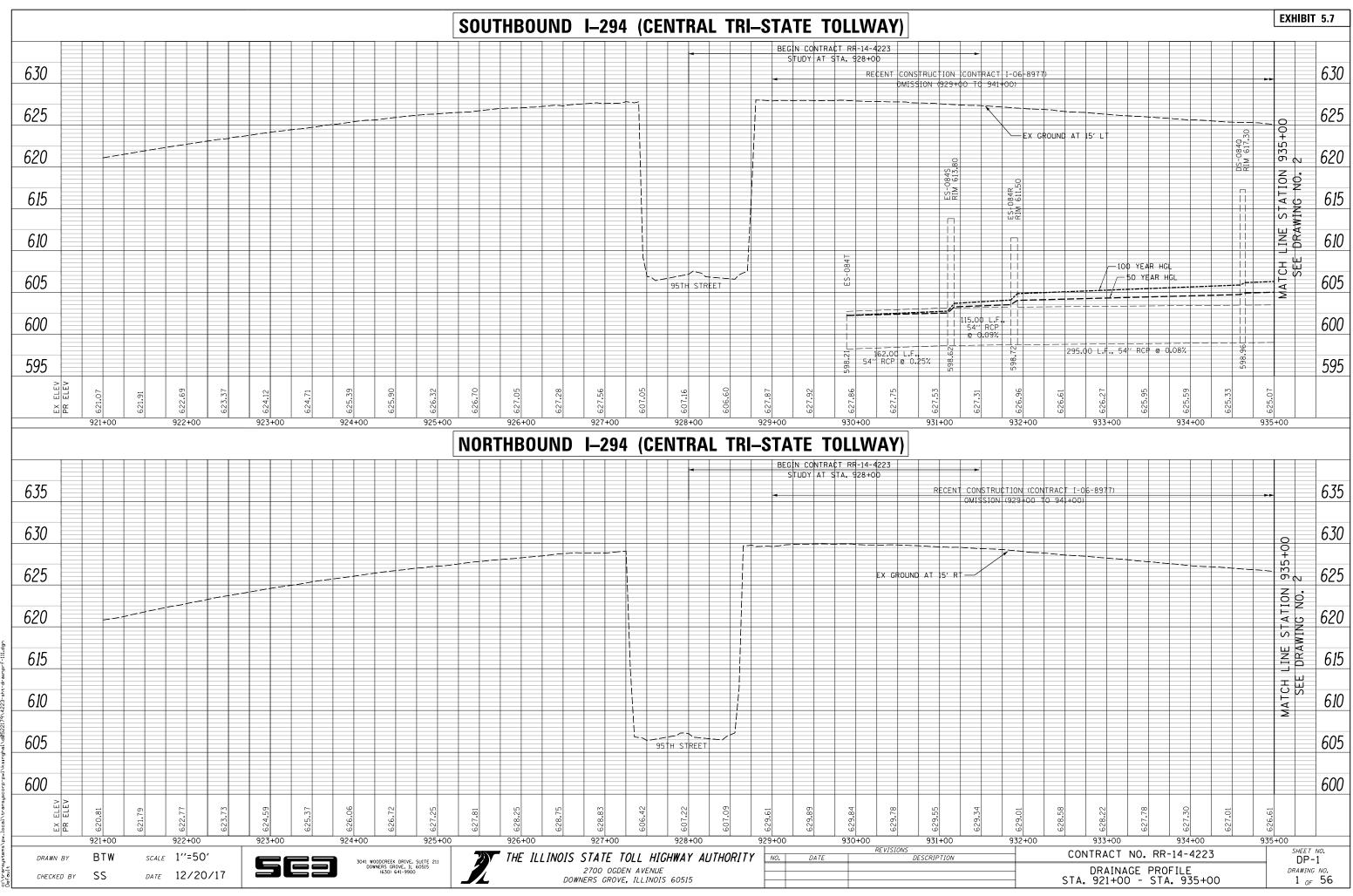


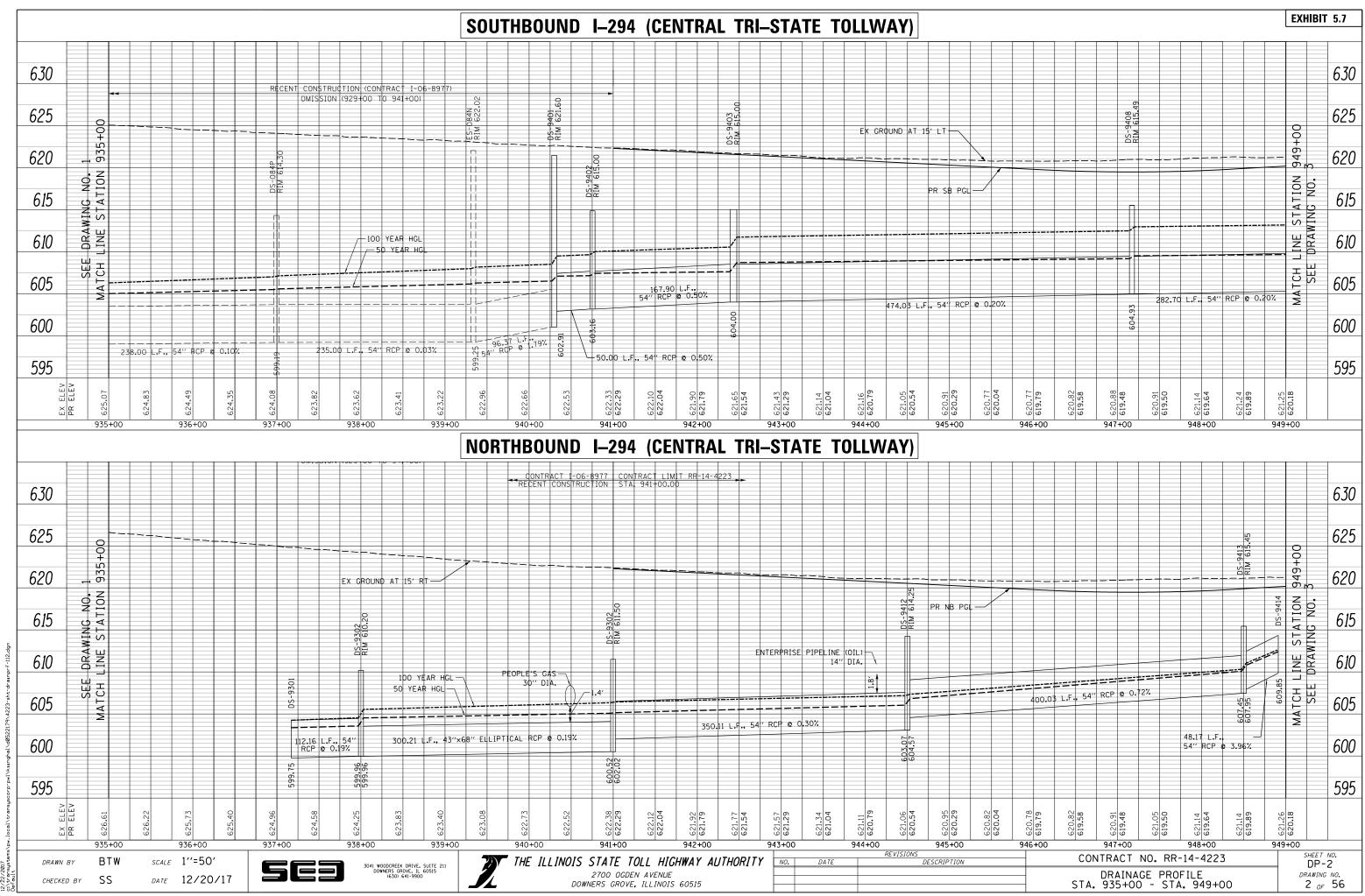




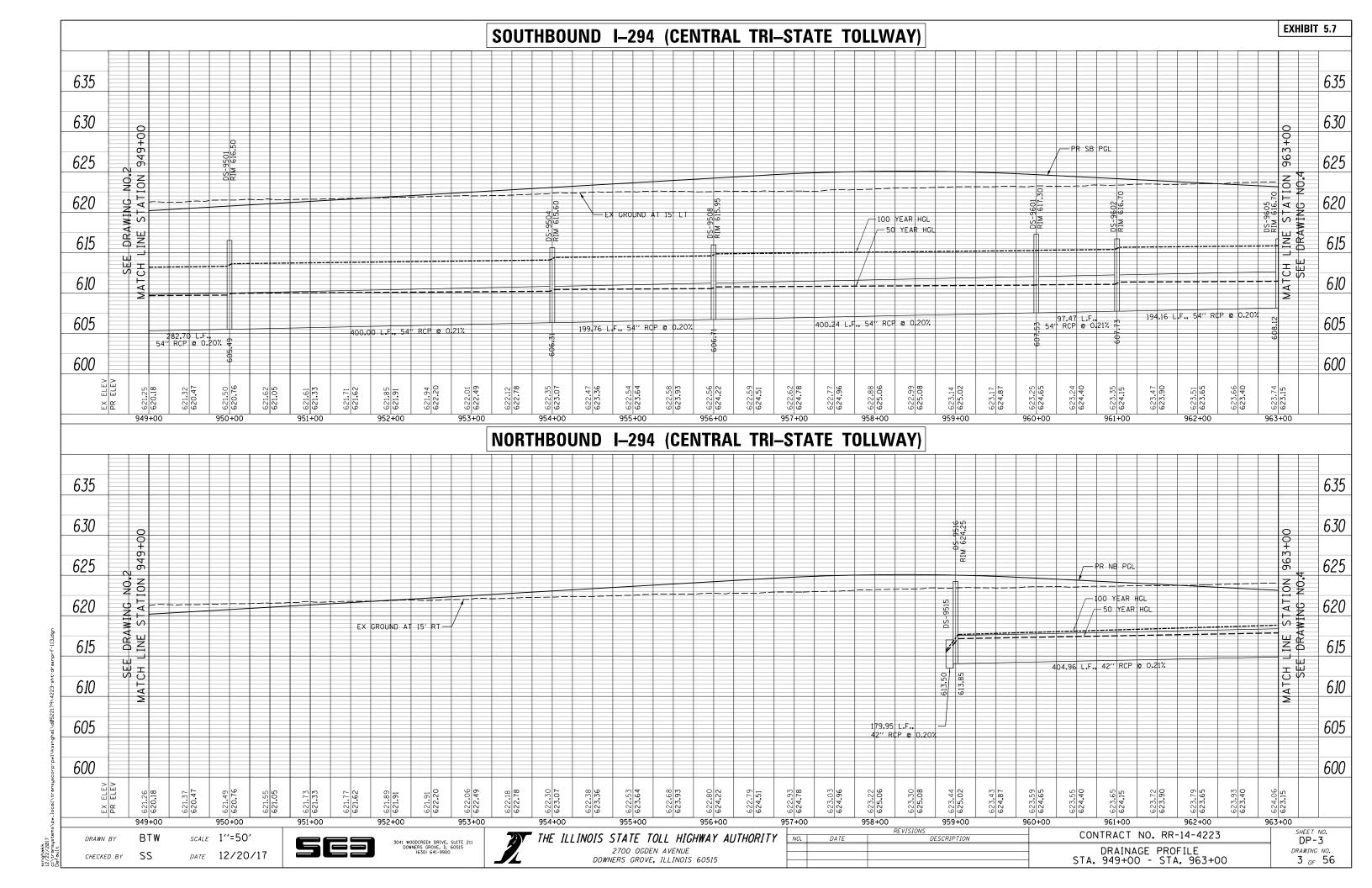
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5.7 DRAINAGE PROFILE





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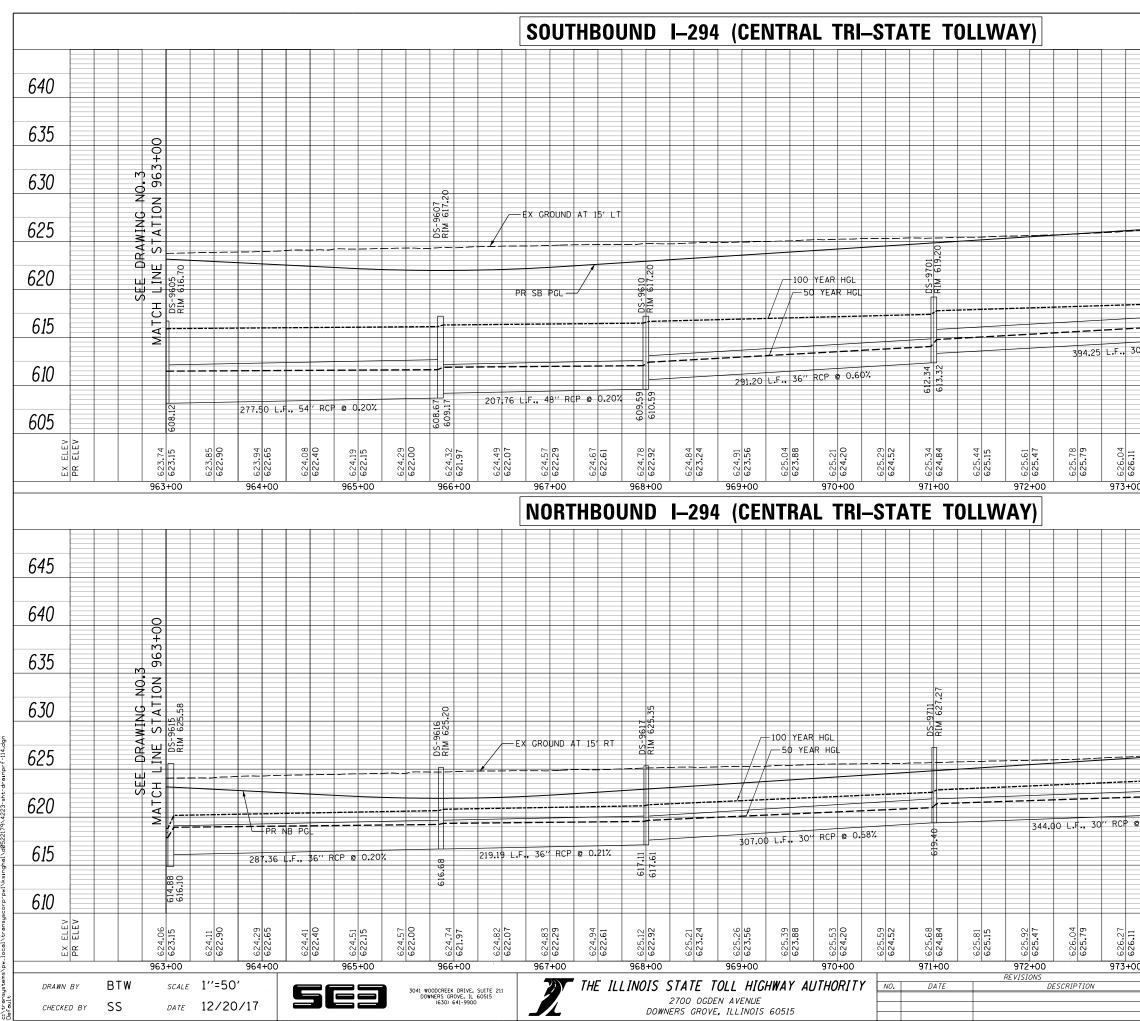


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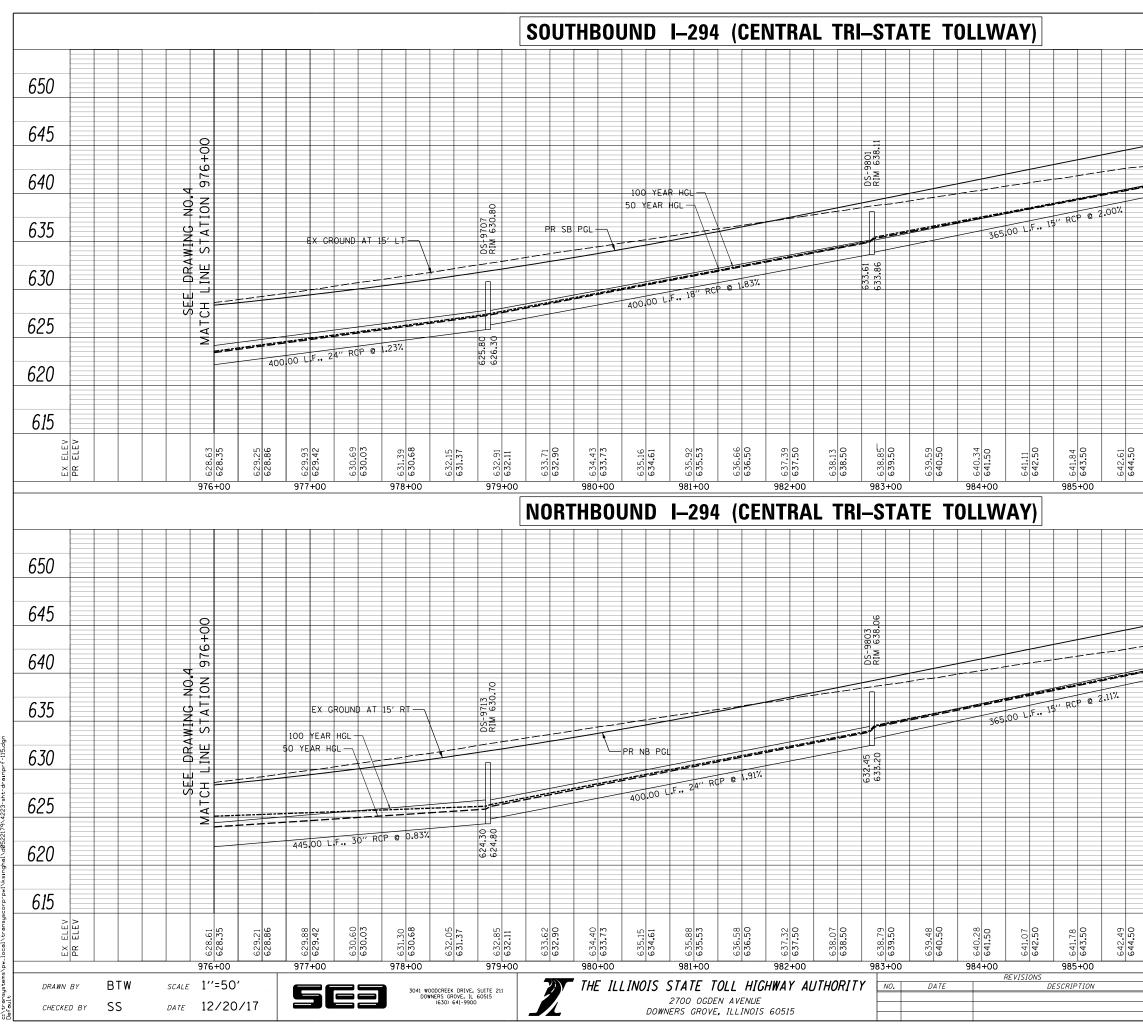
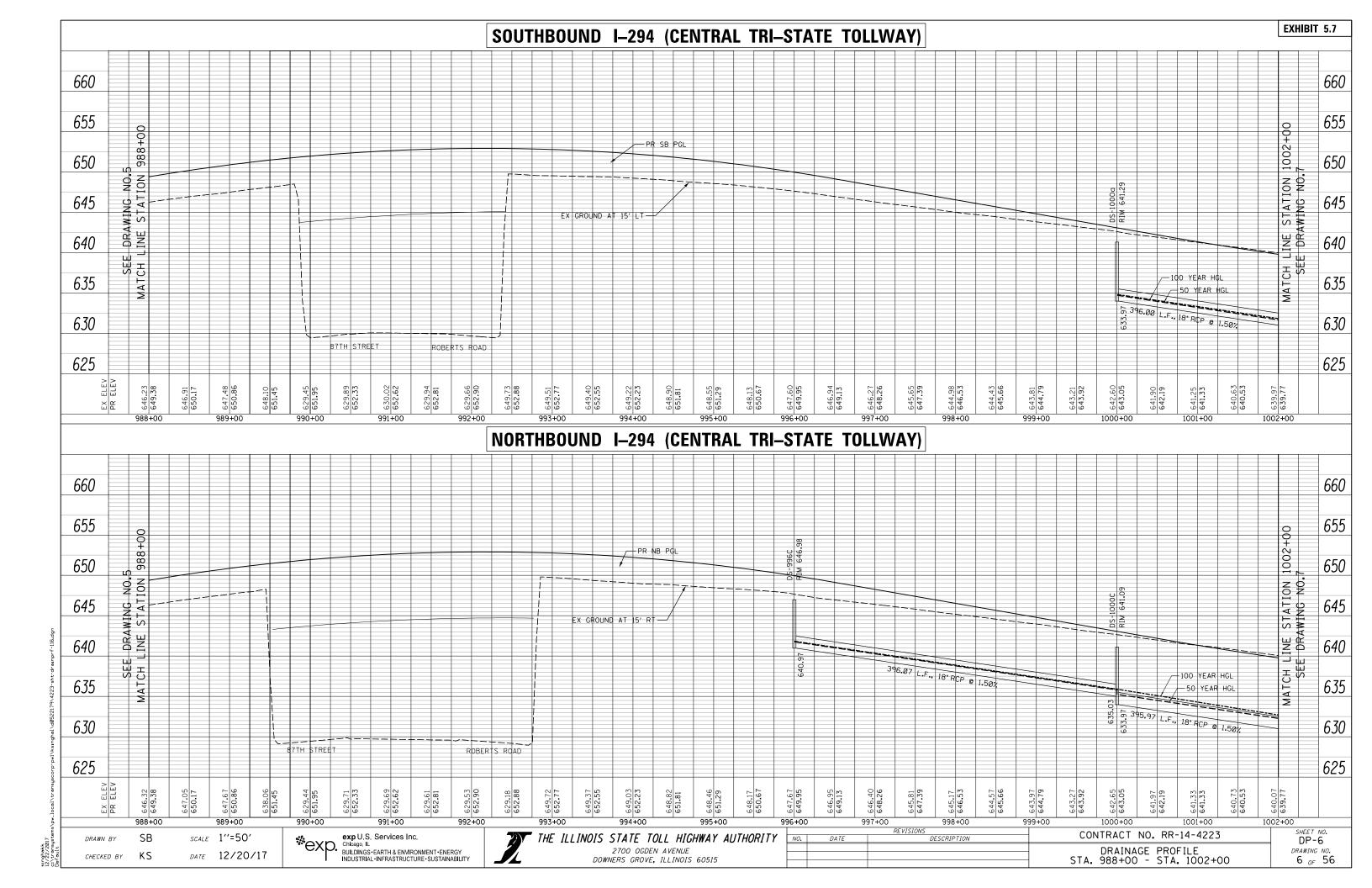
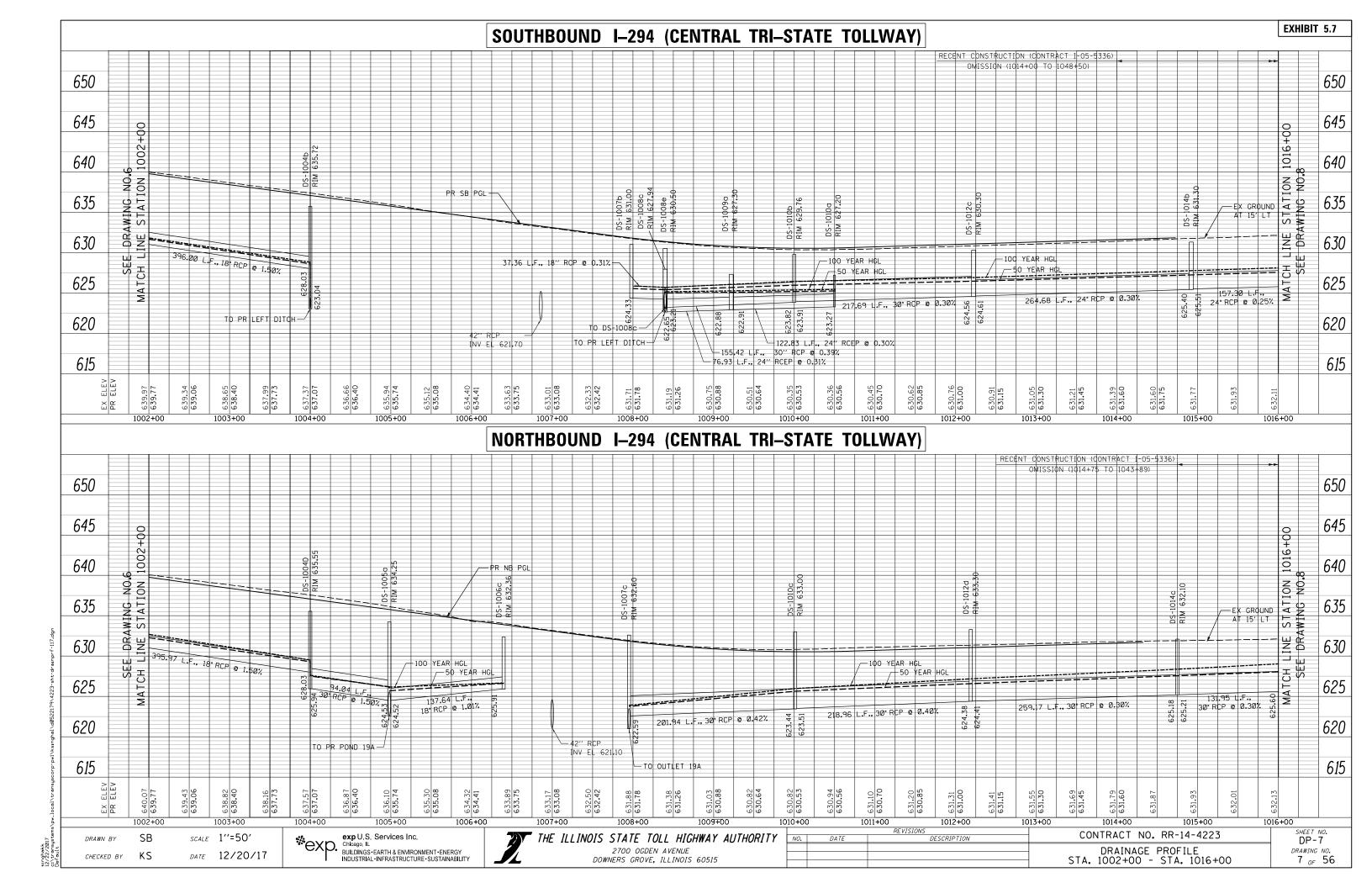
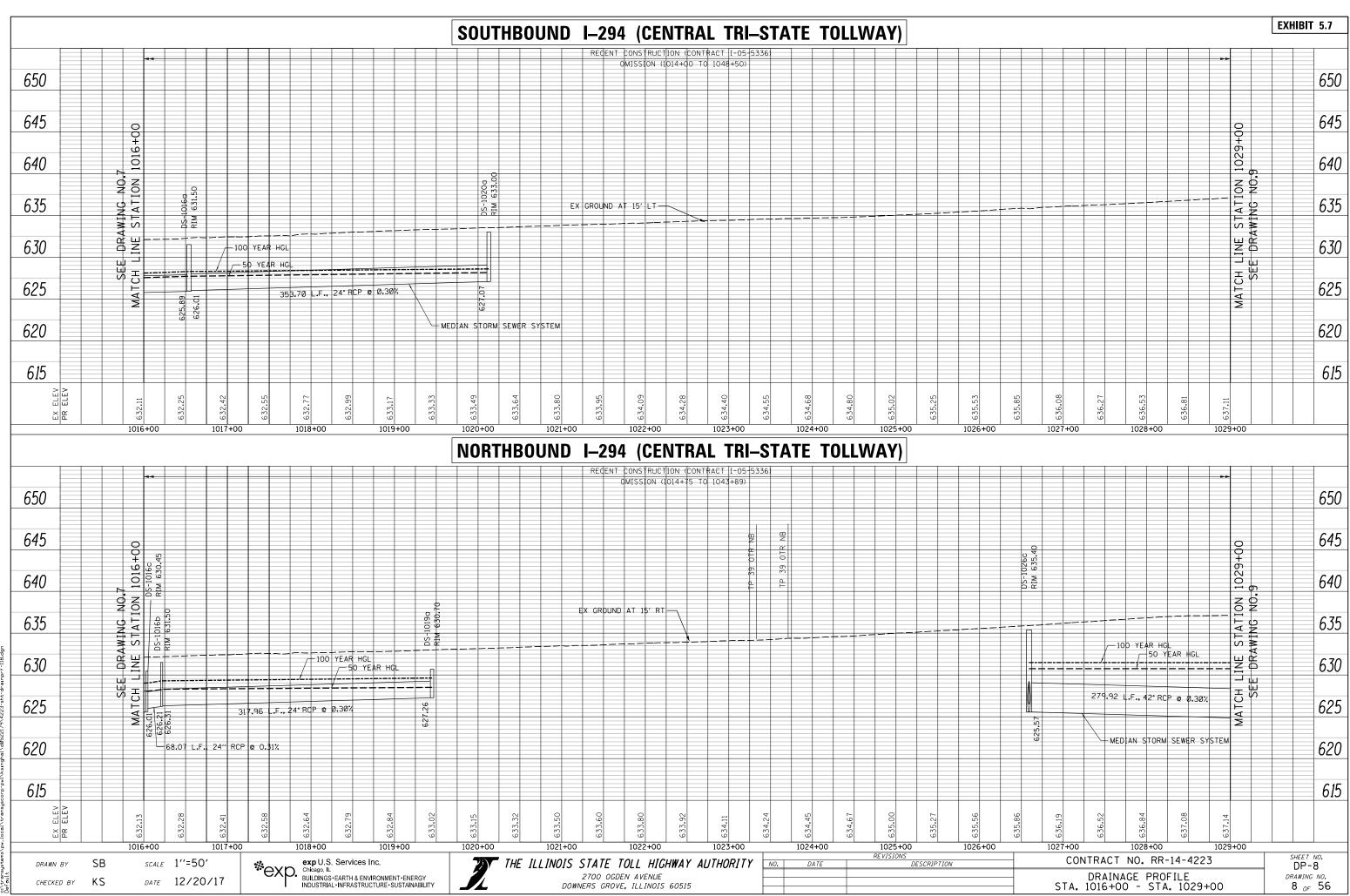


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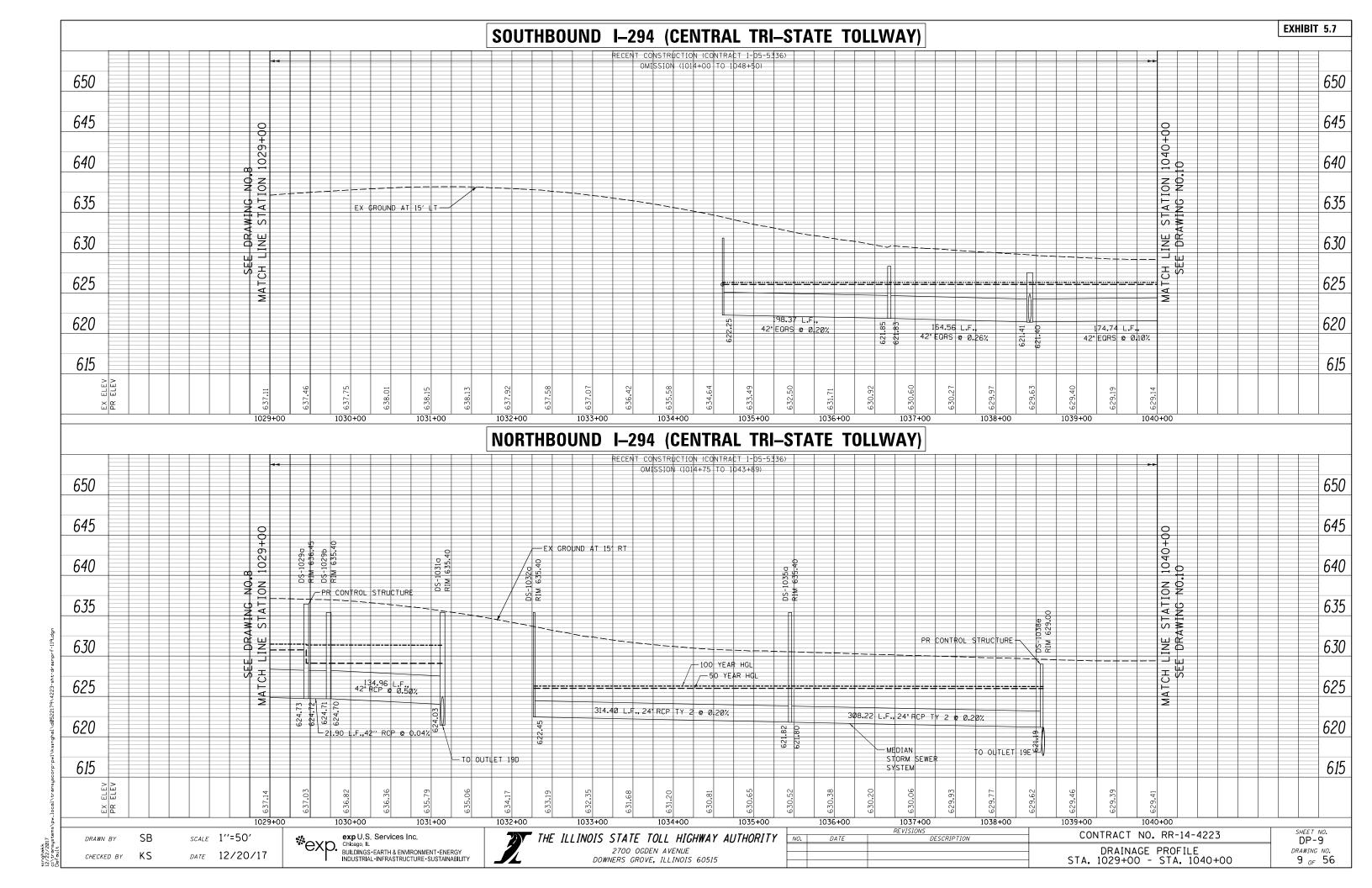


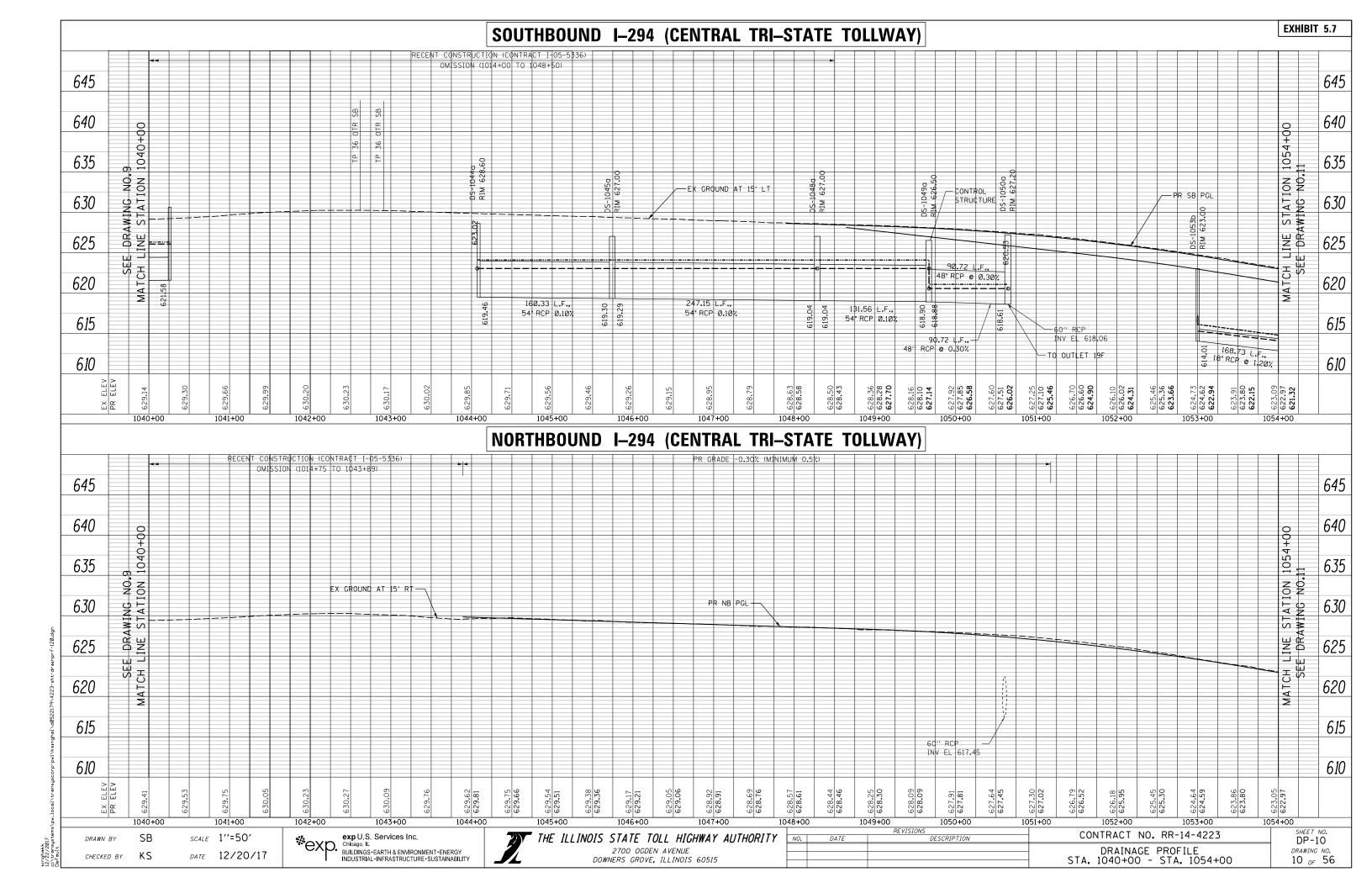


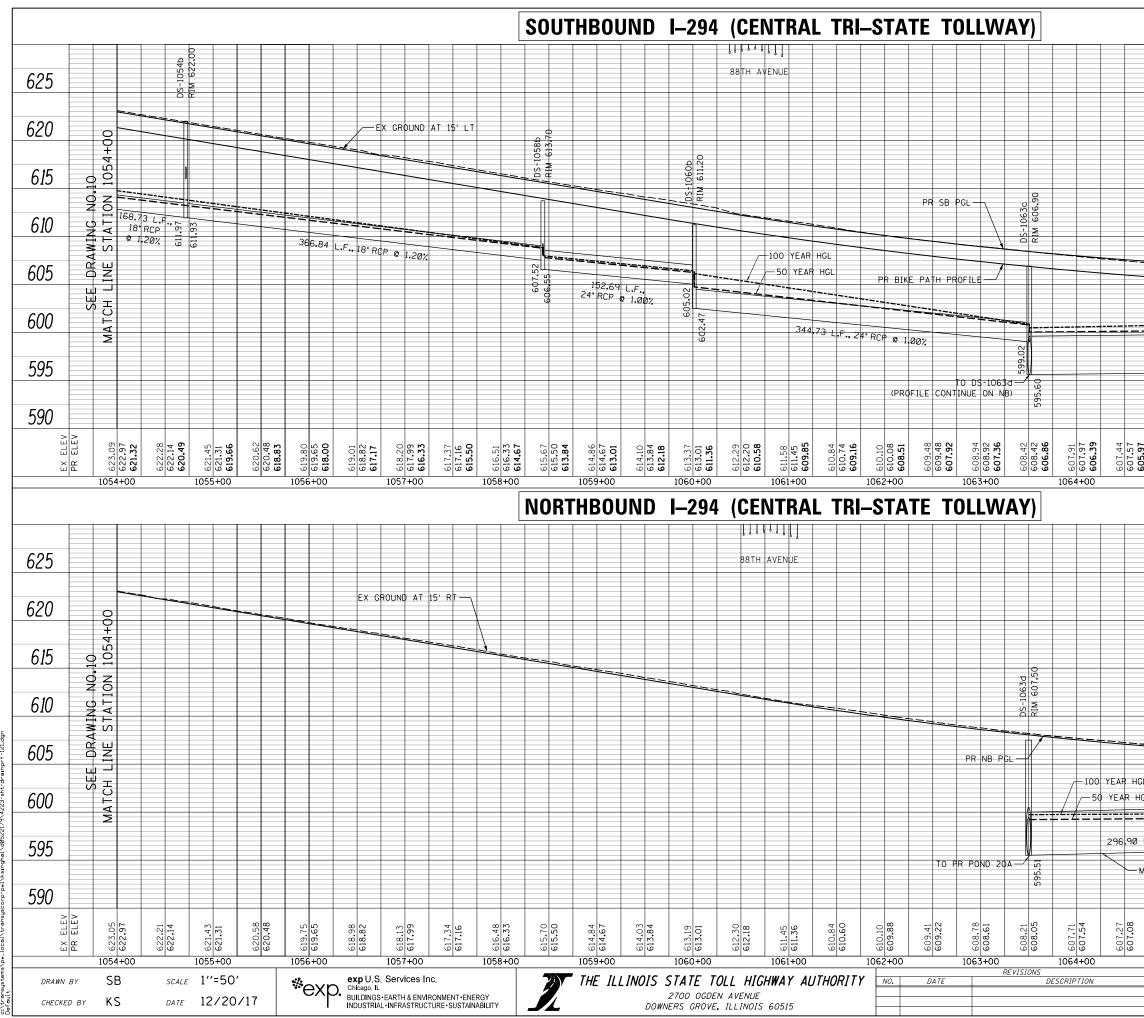


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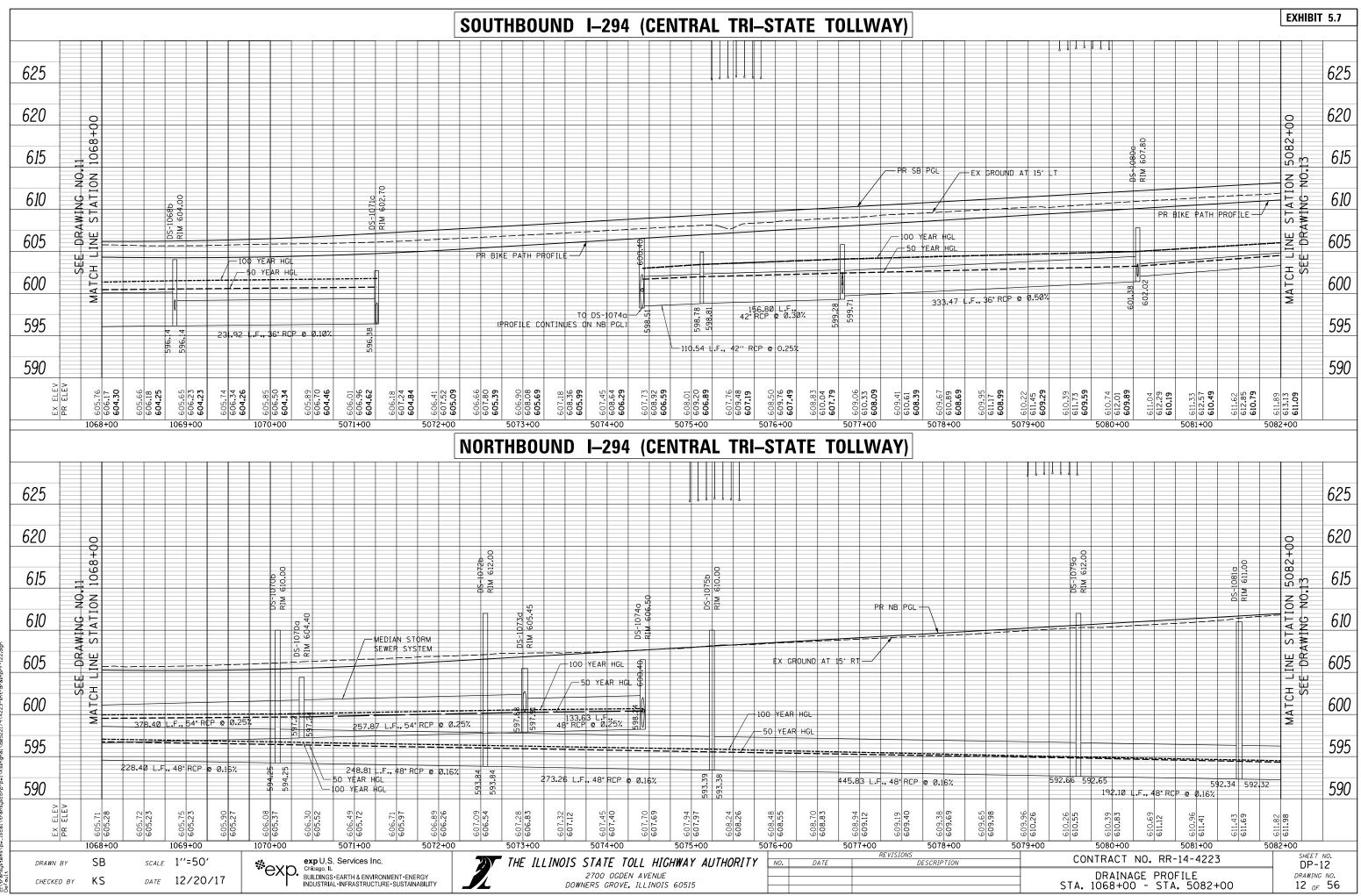
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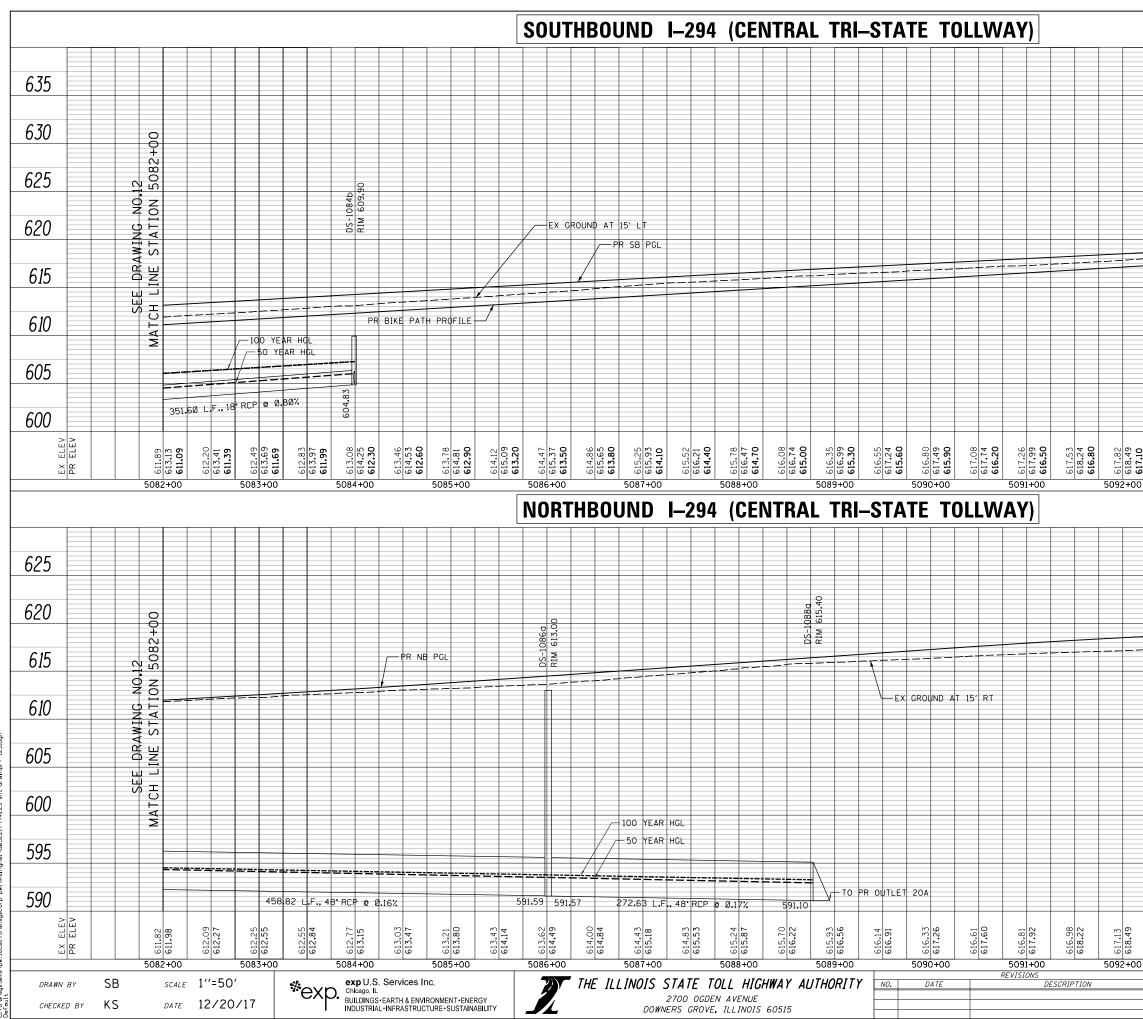


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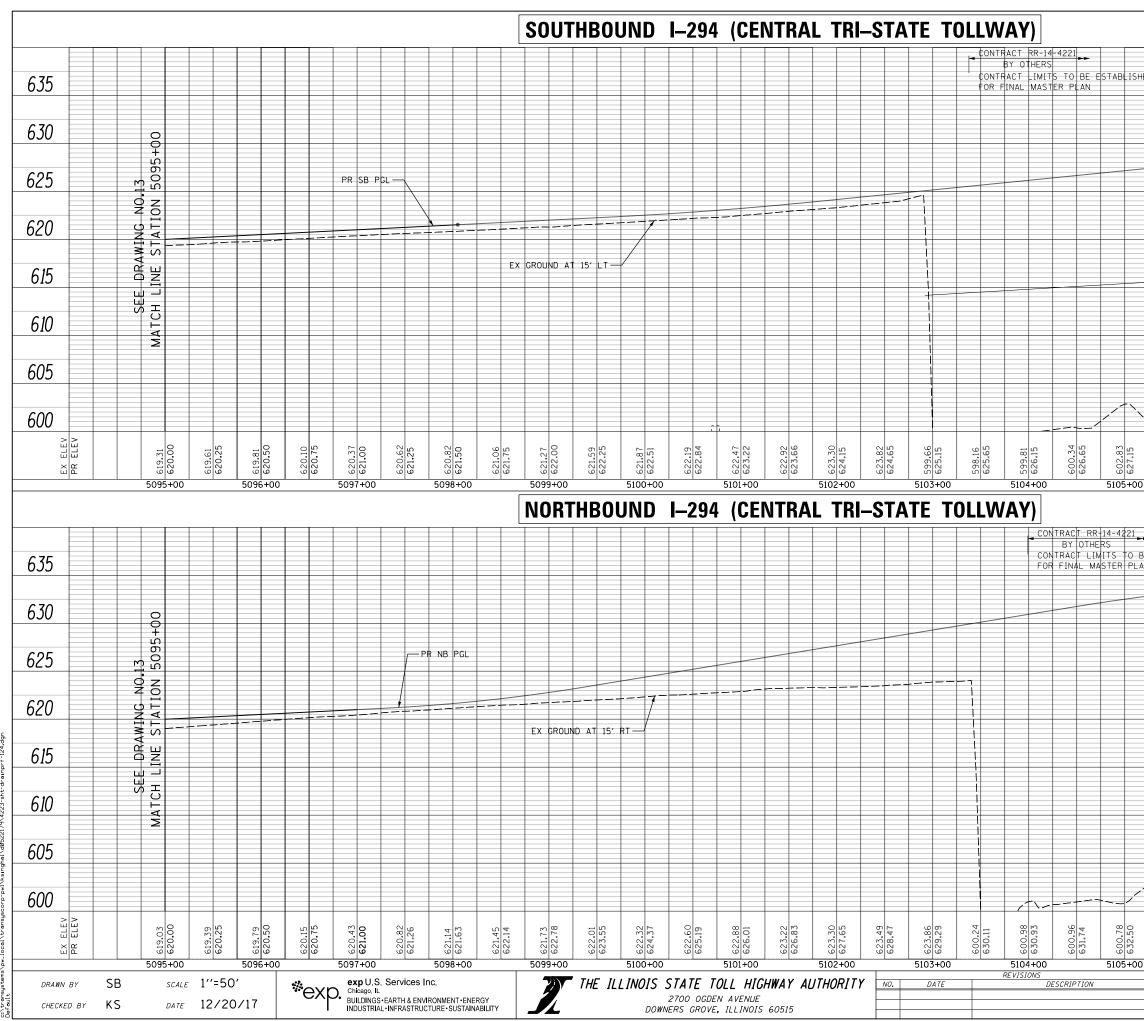
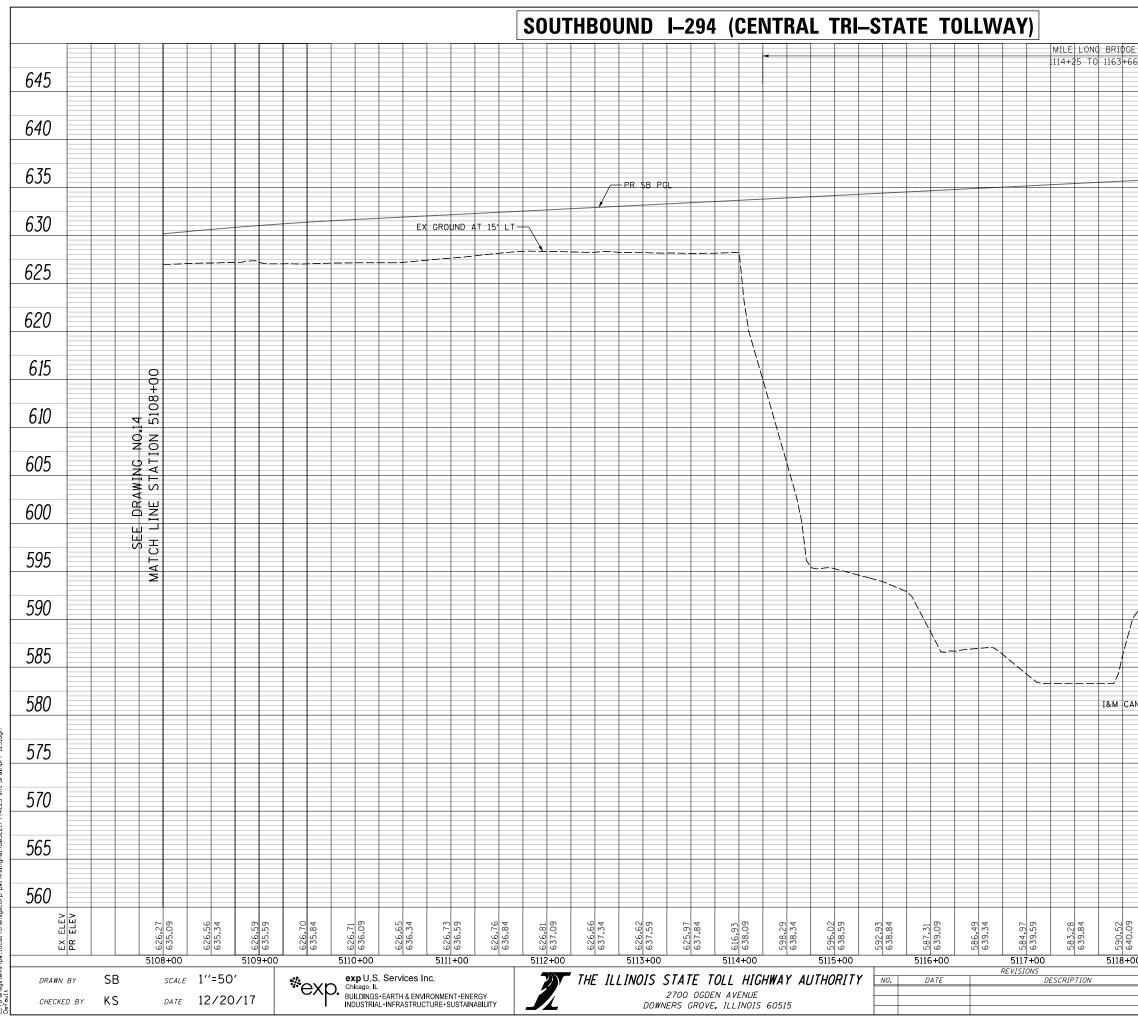
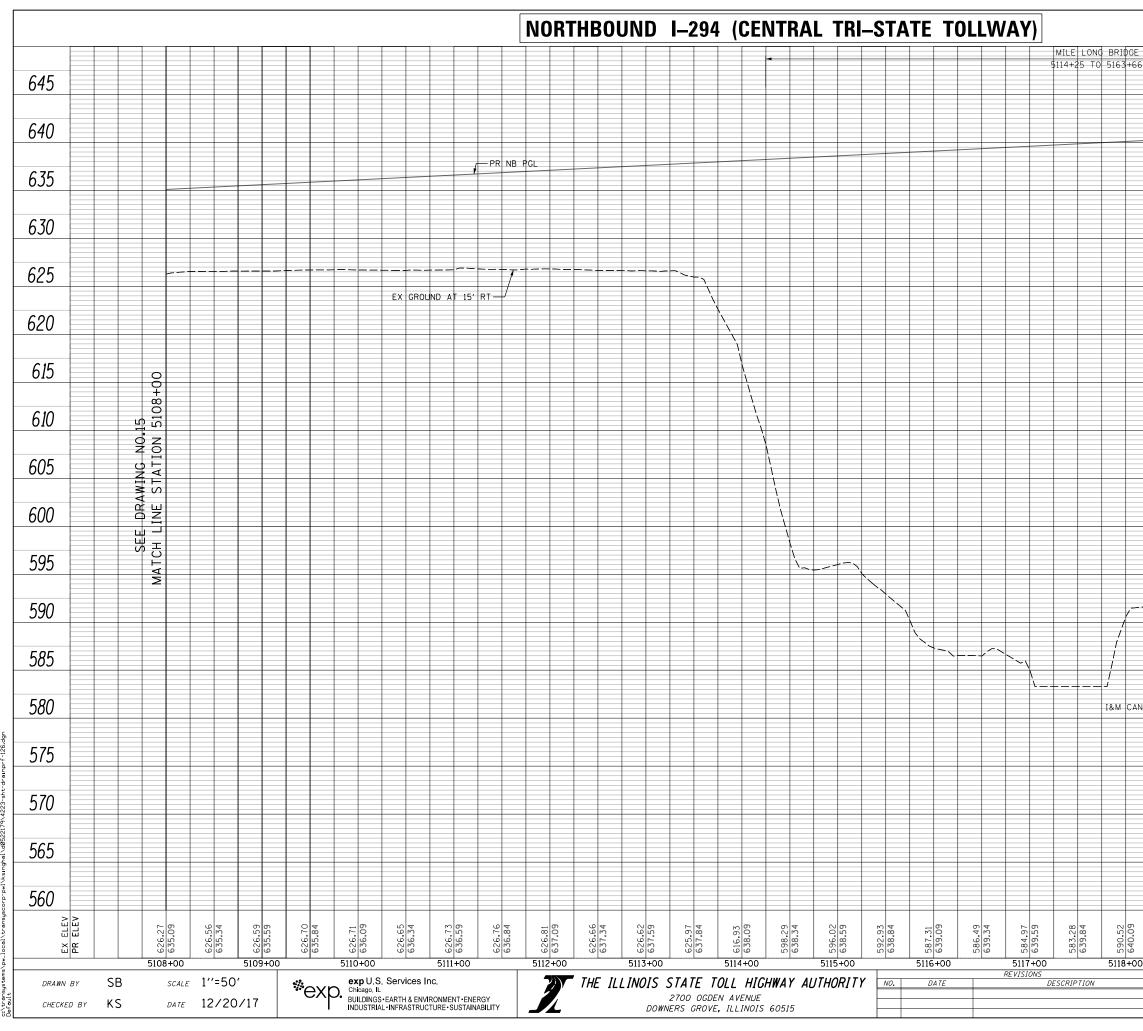


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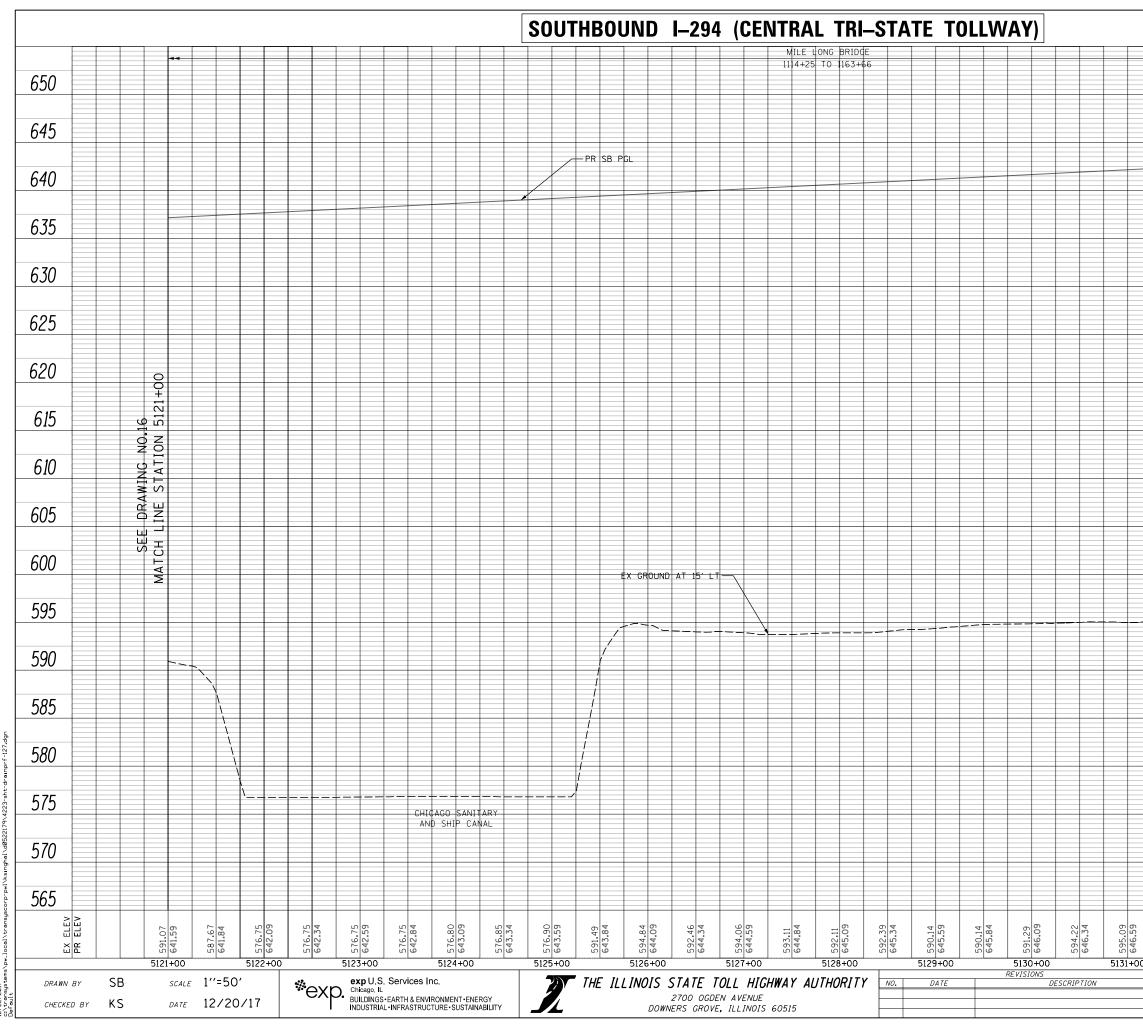
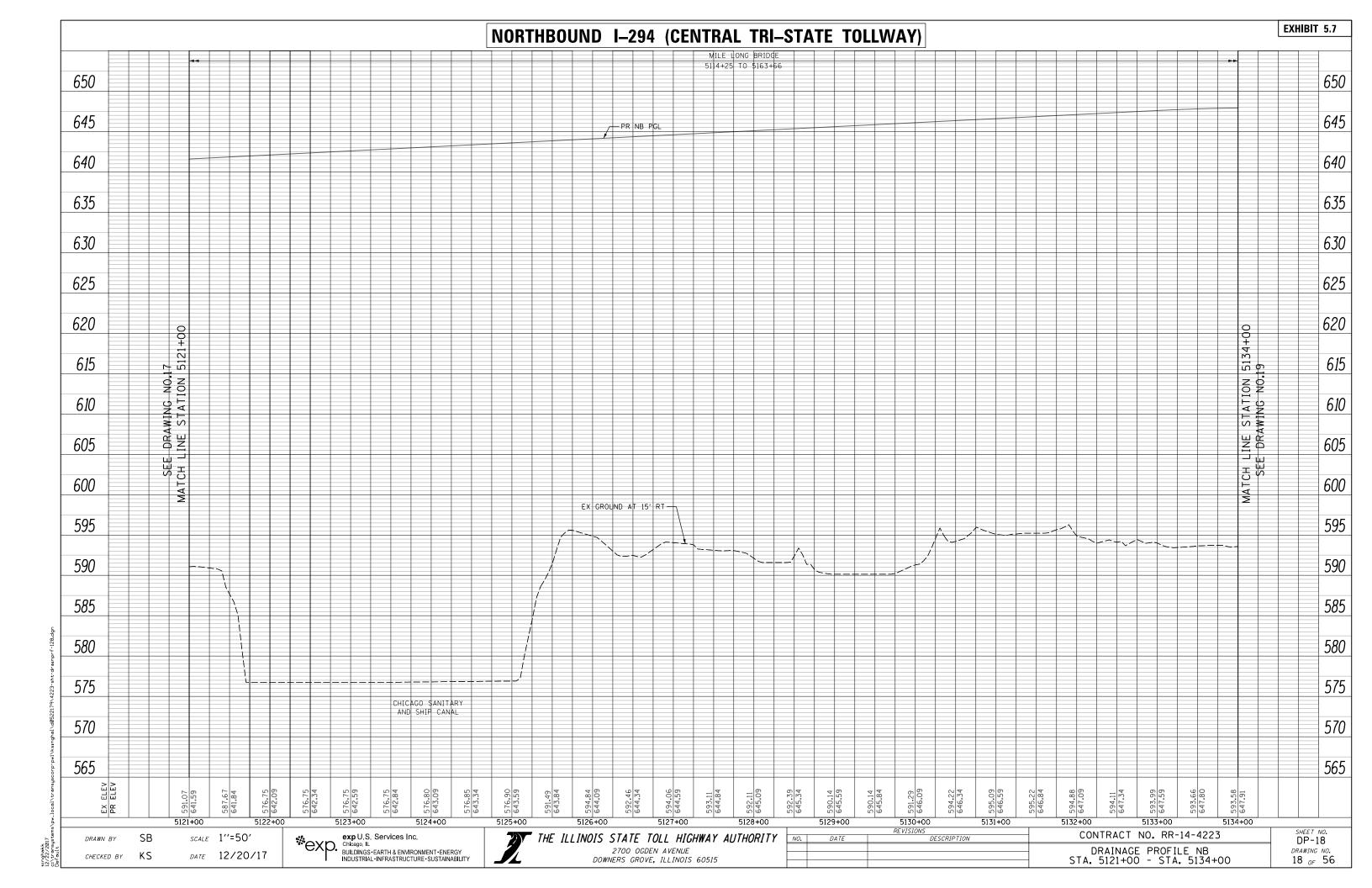
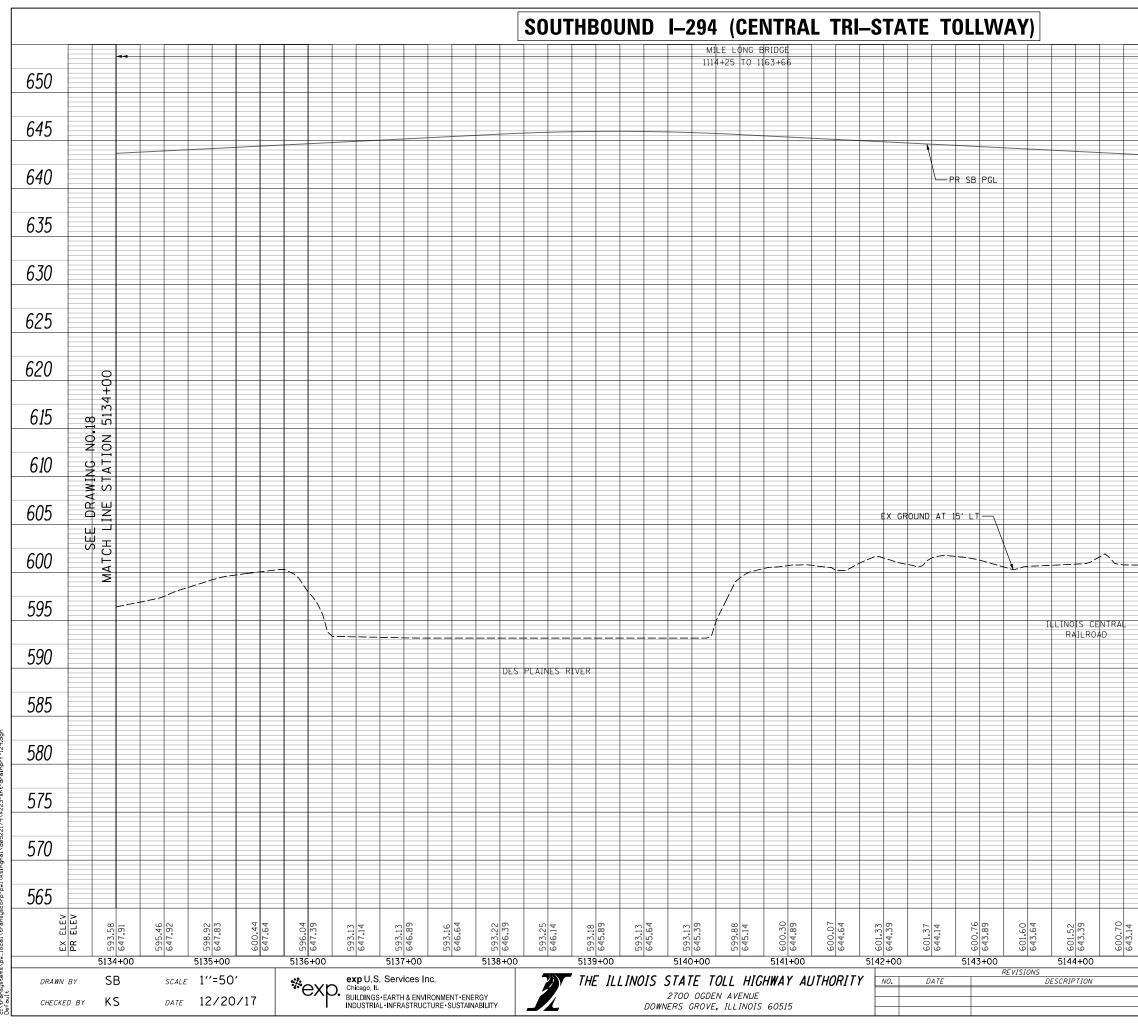
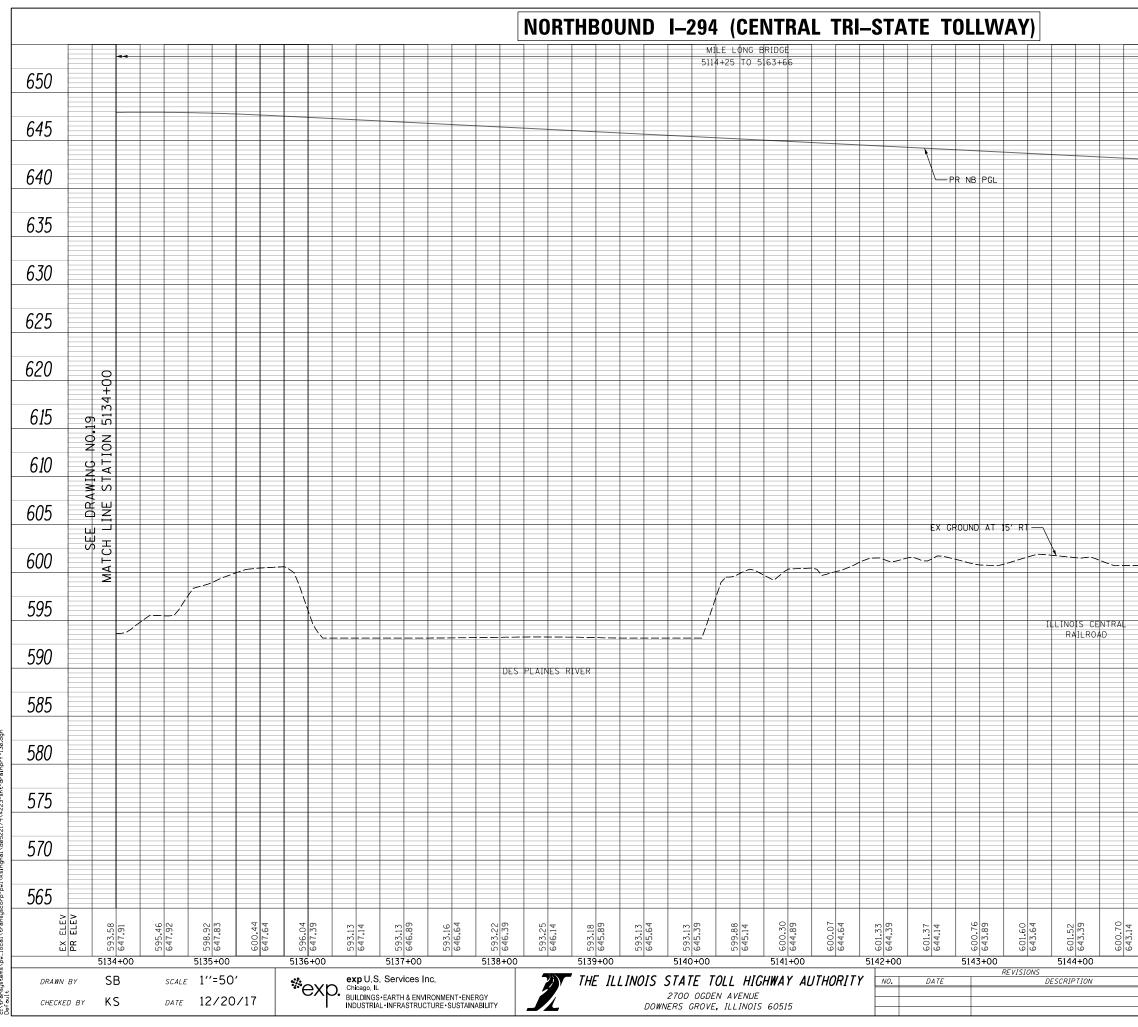


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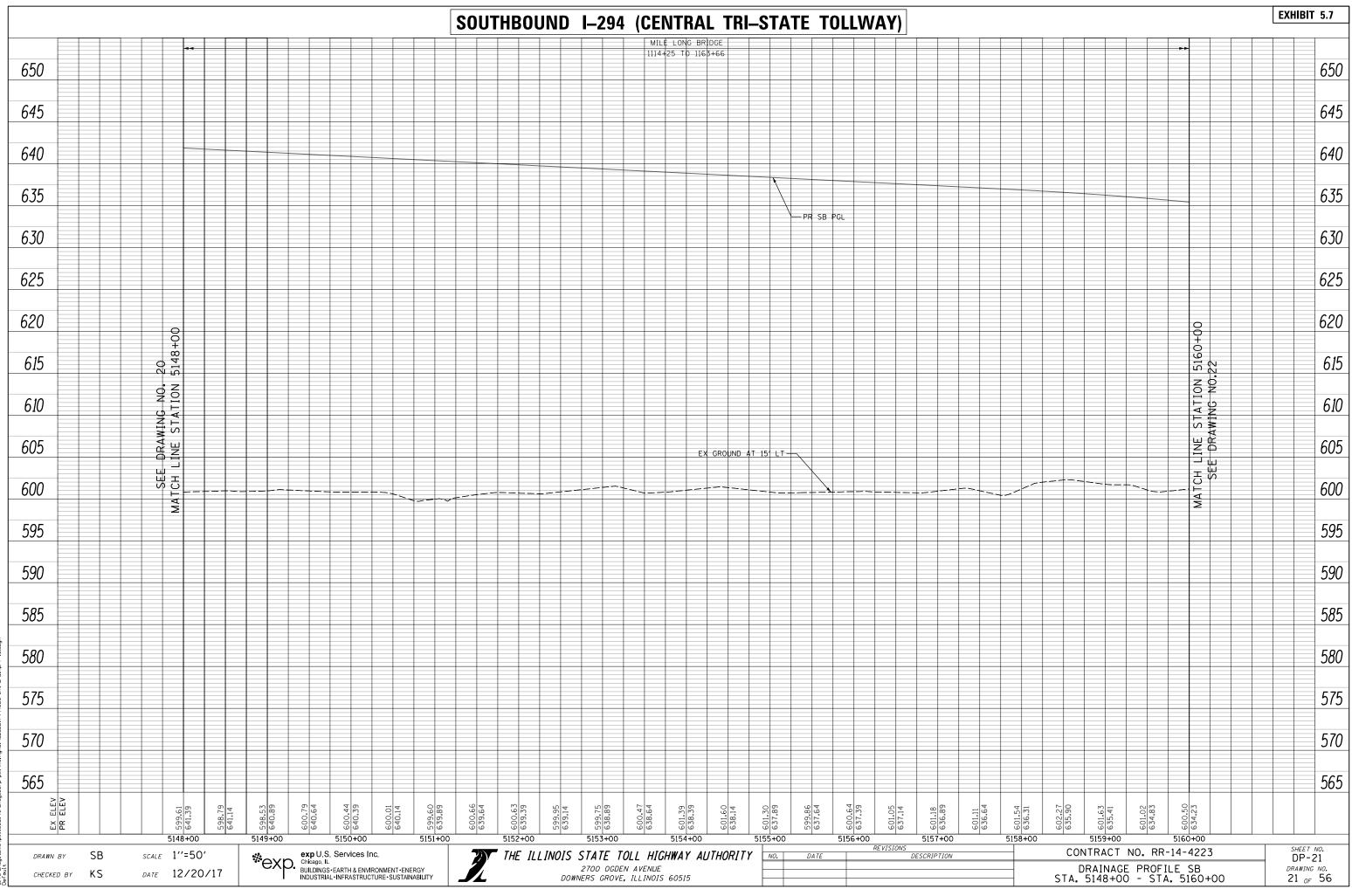




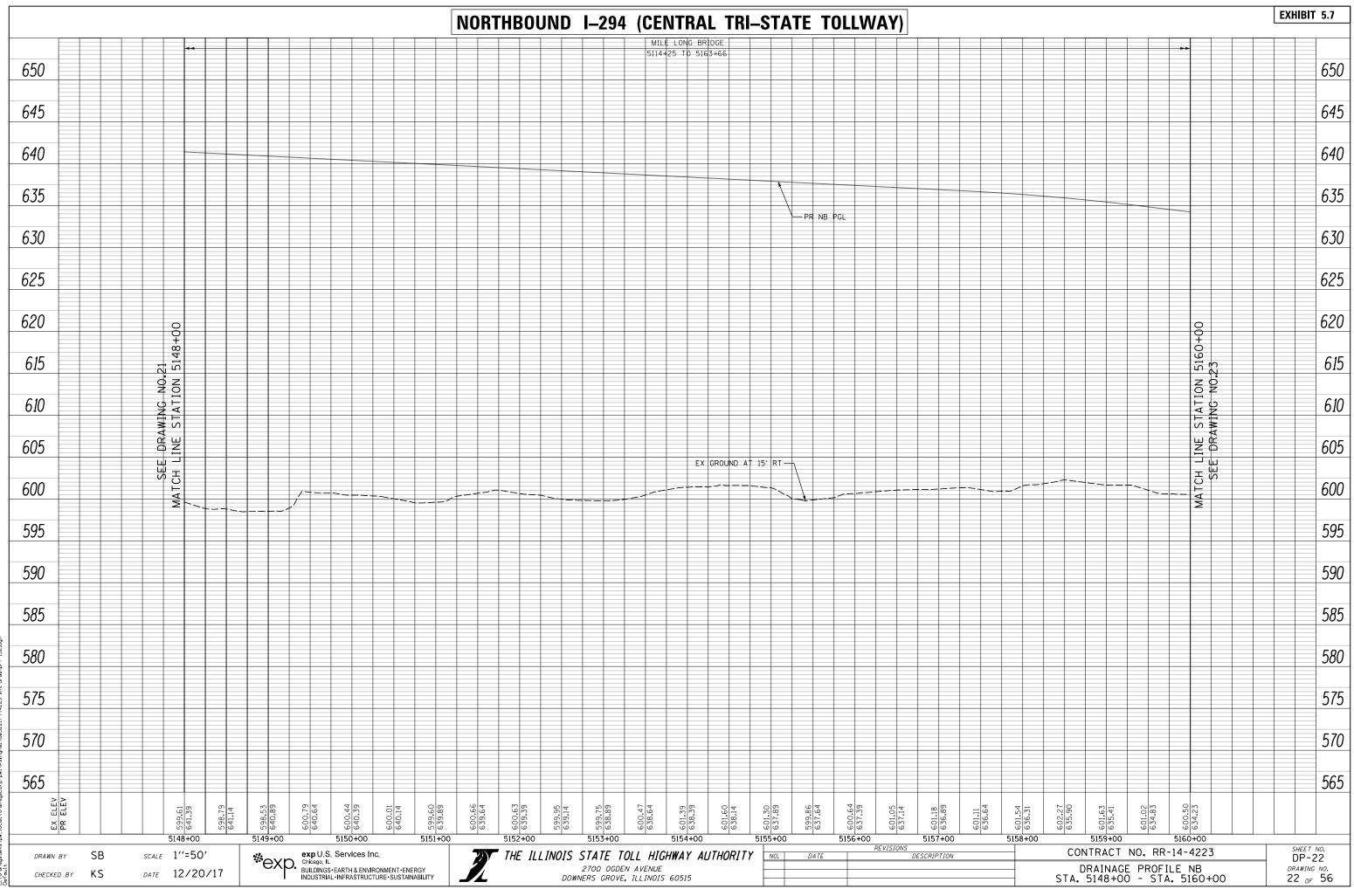
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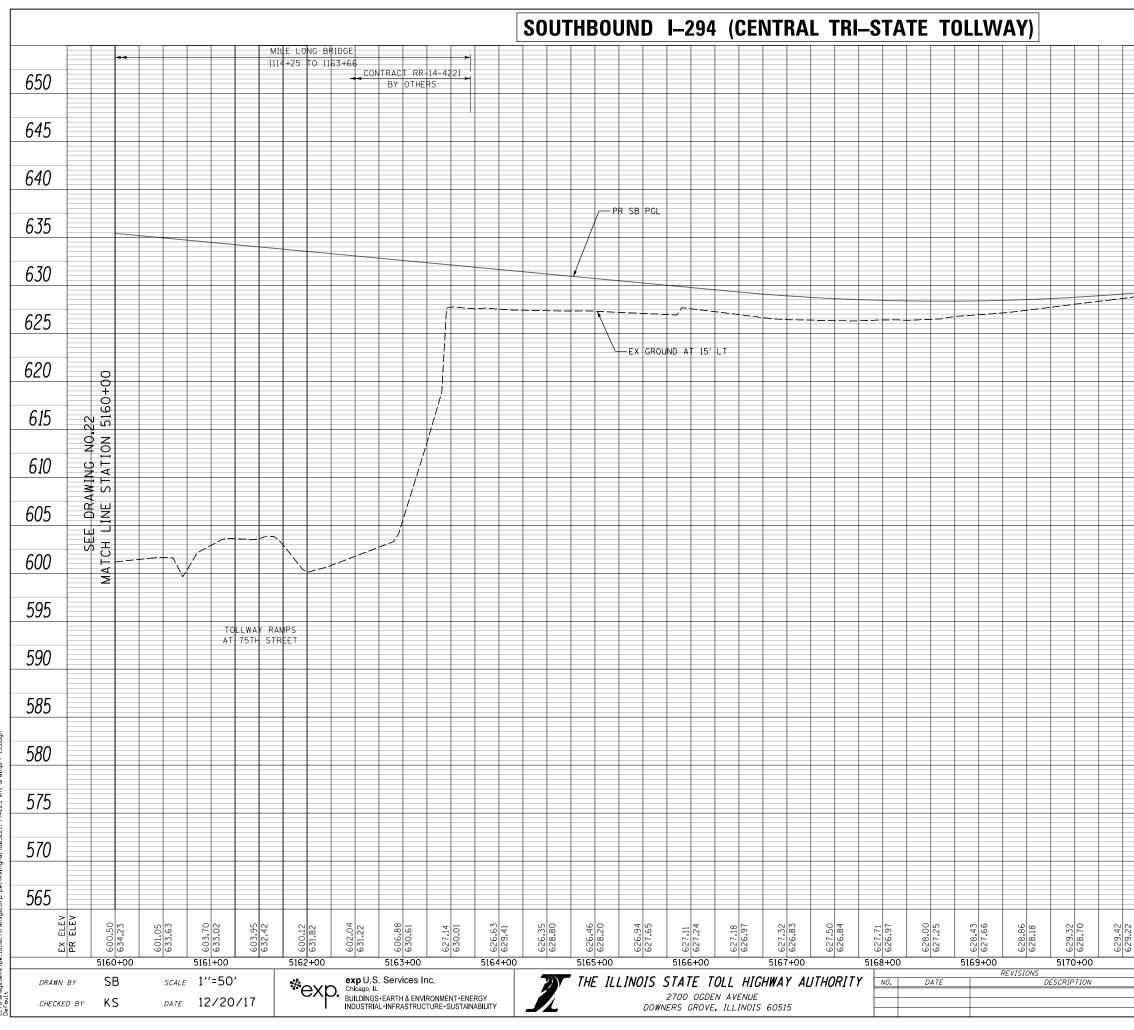
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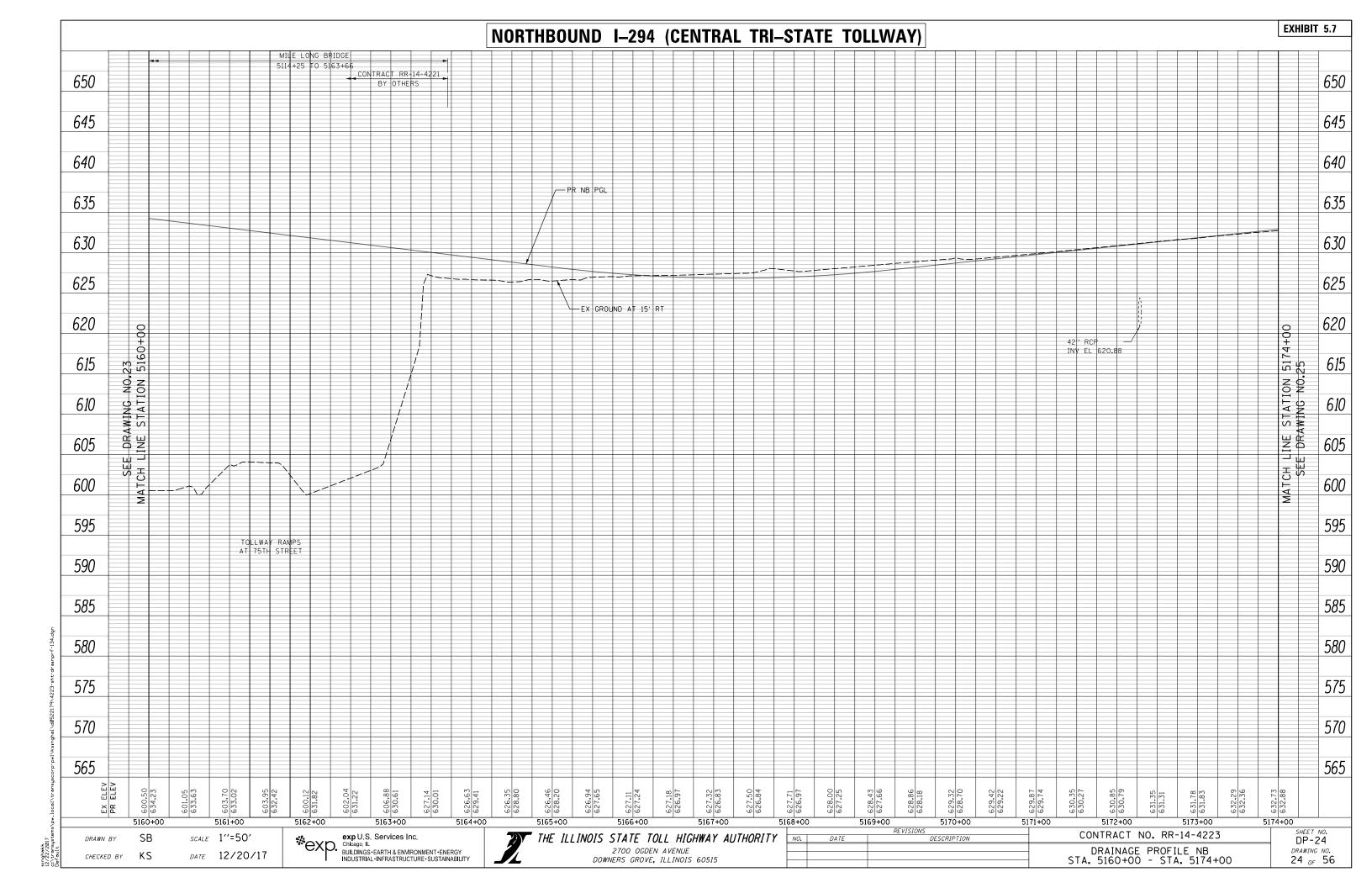


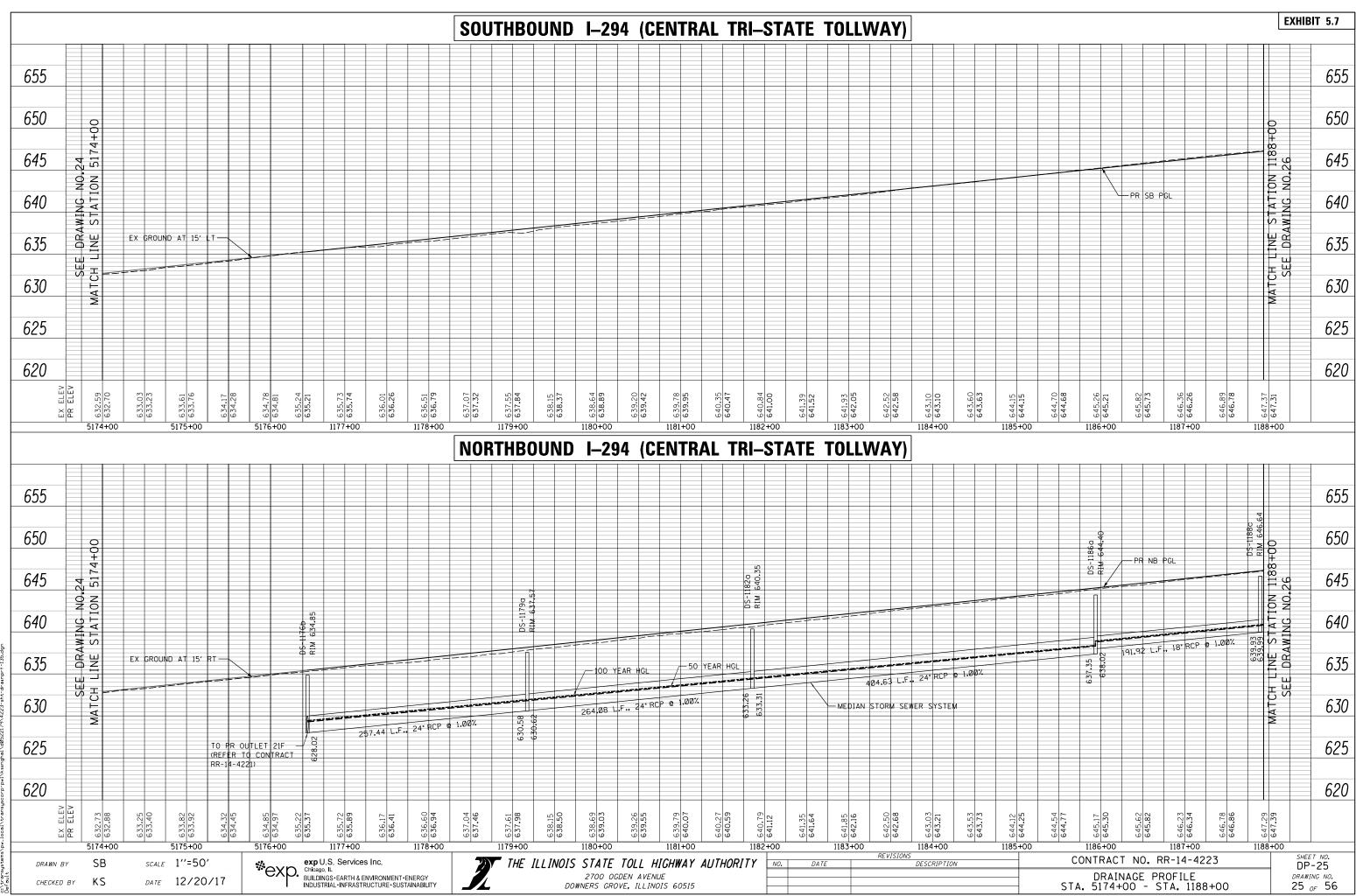
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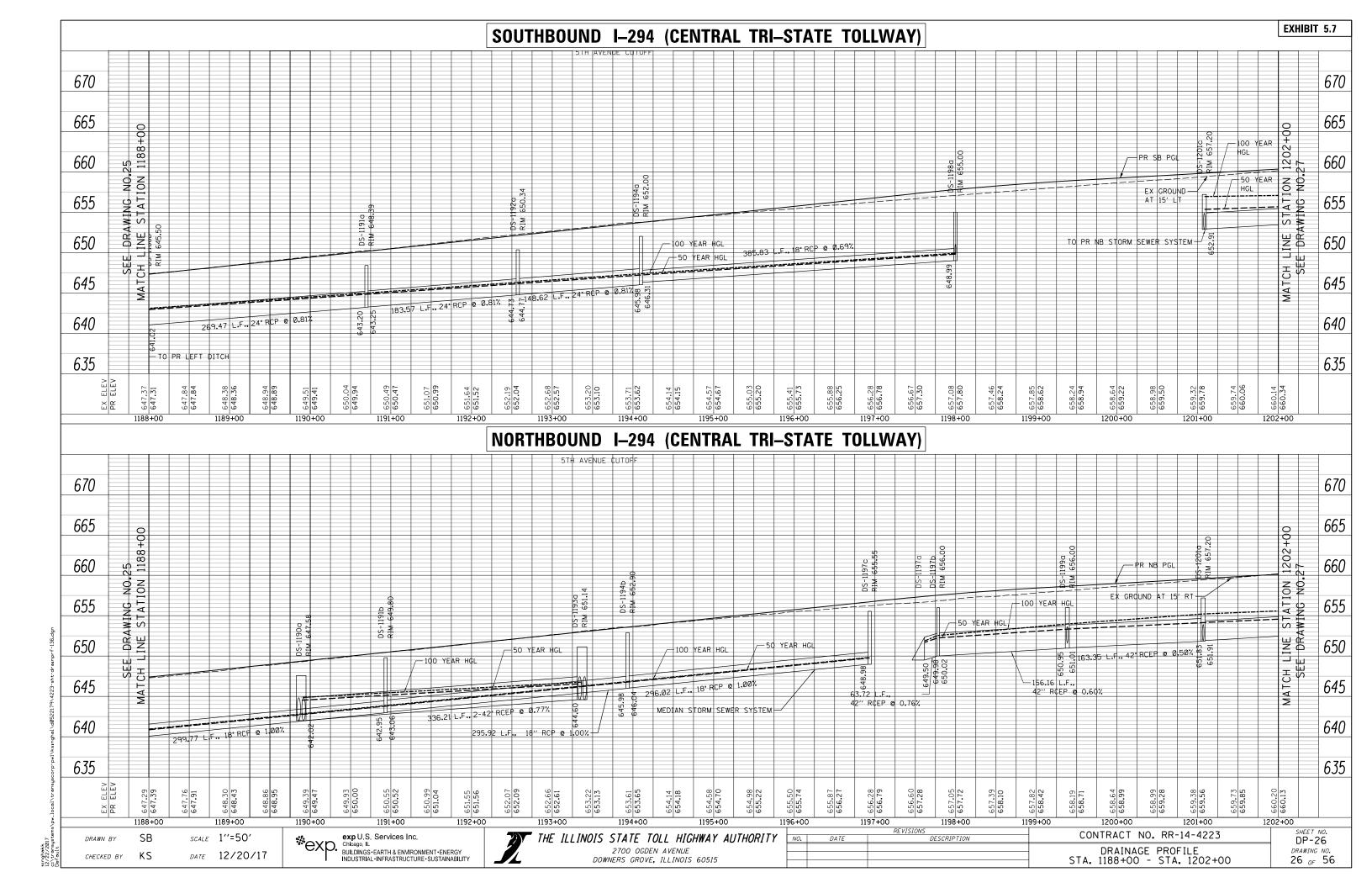
31nghakk 2/22/2017

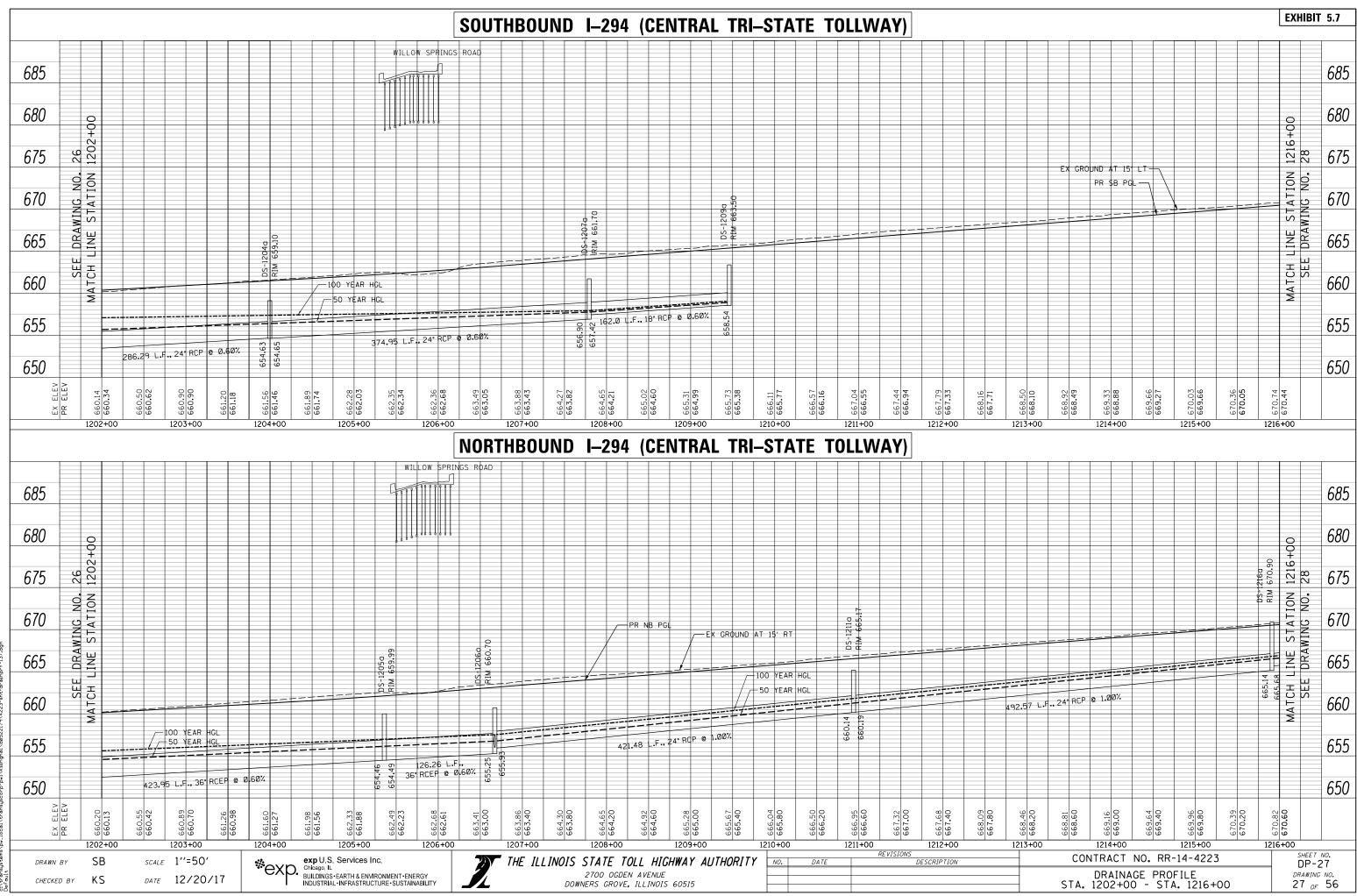
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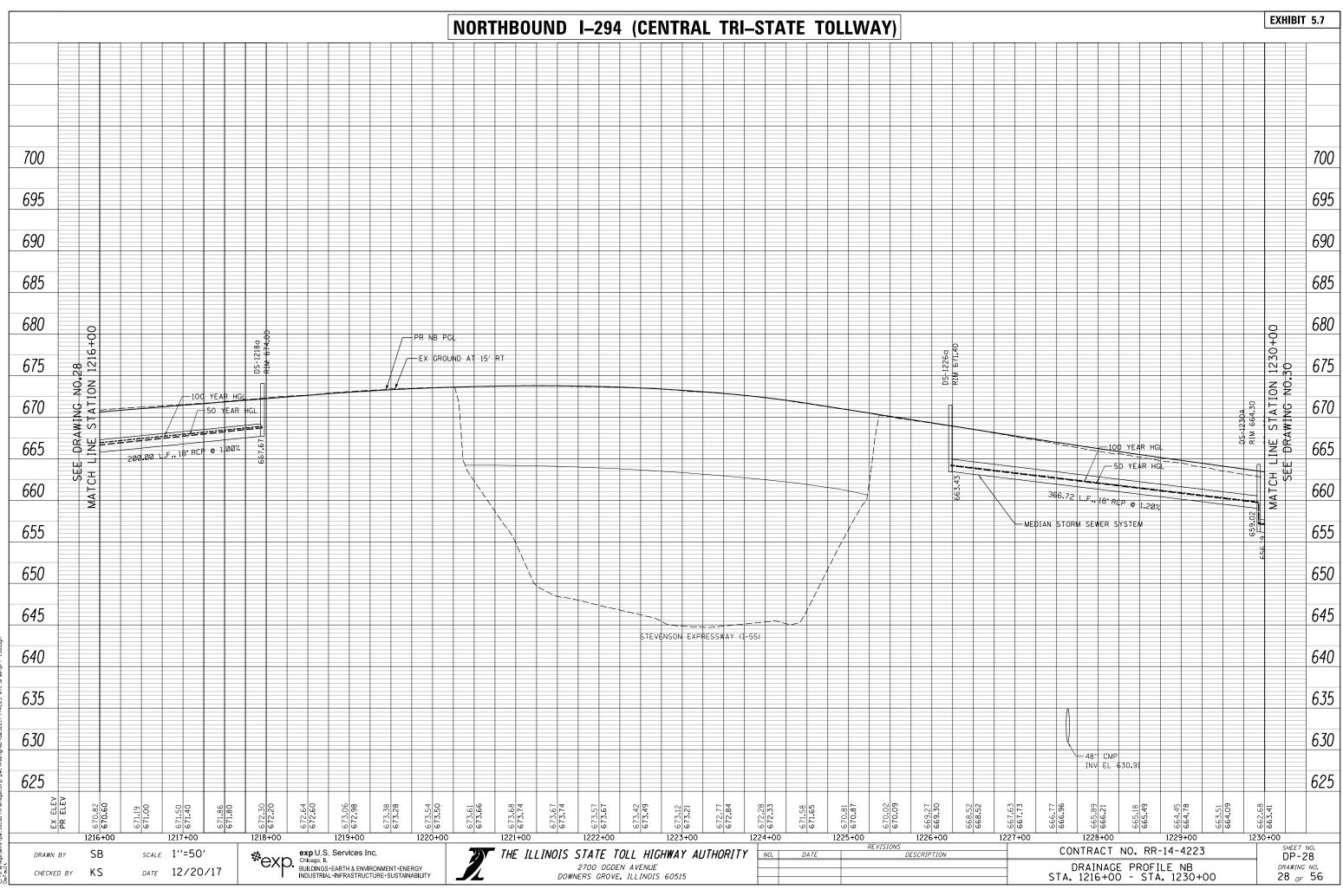


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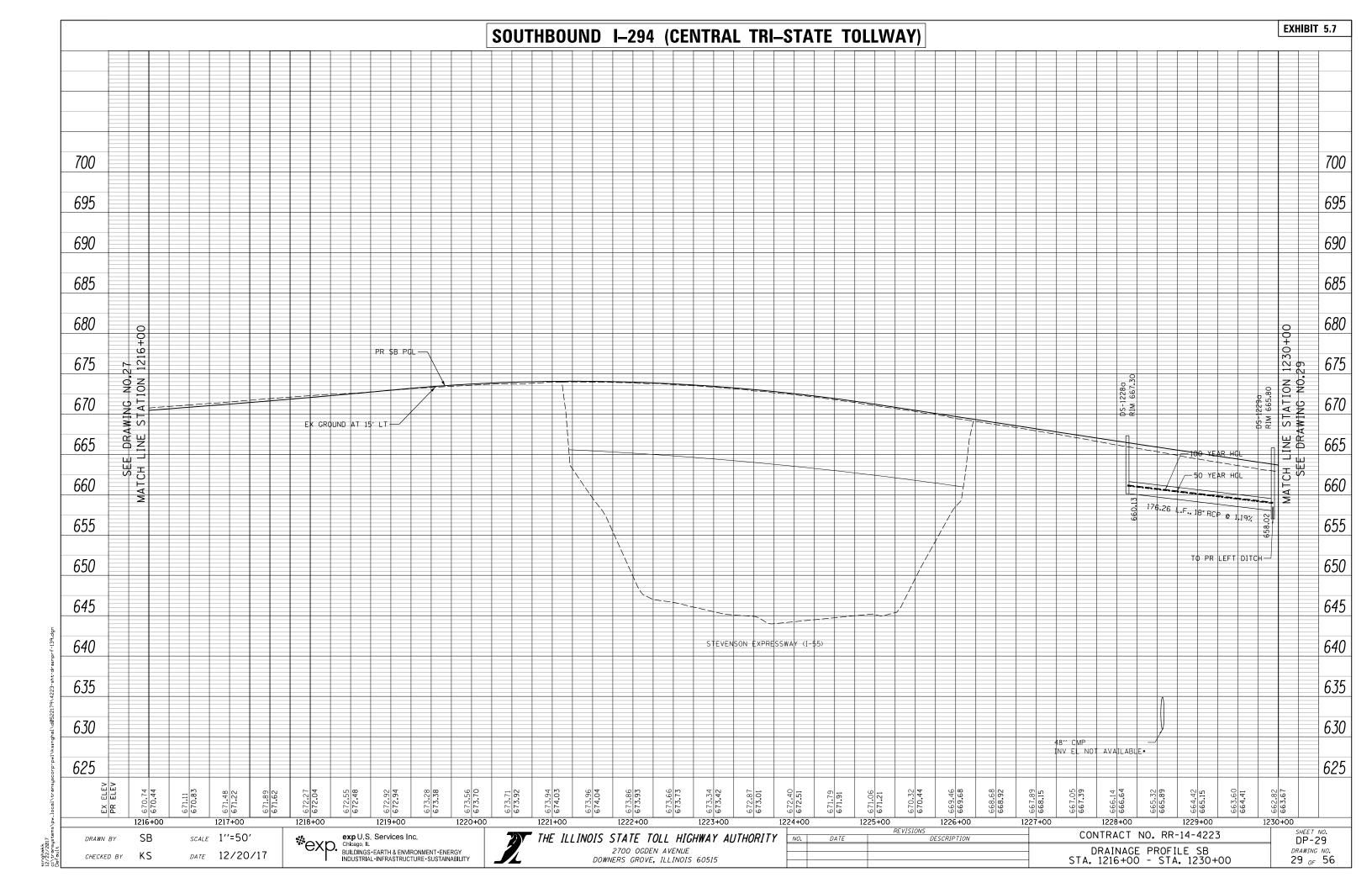




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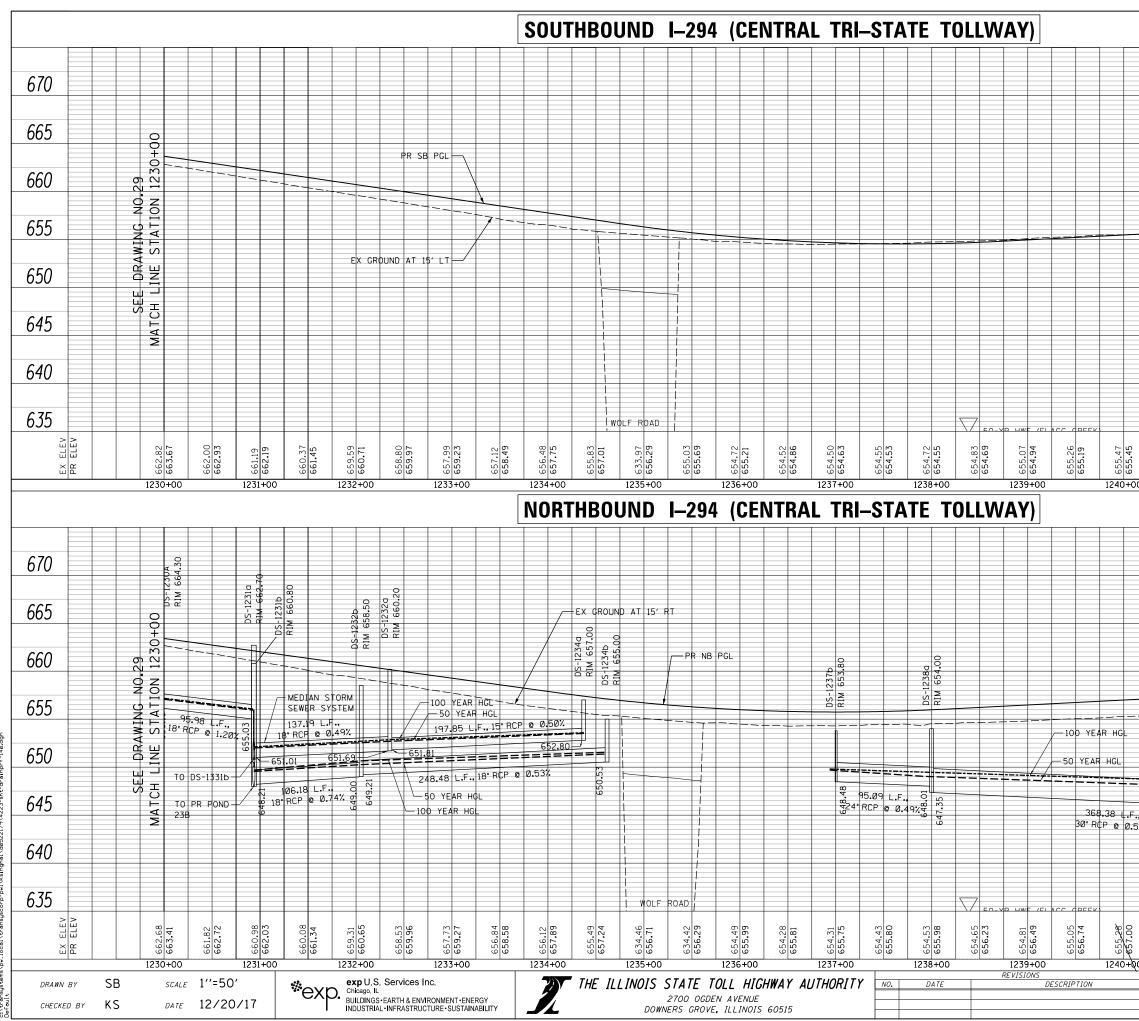
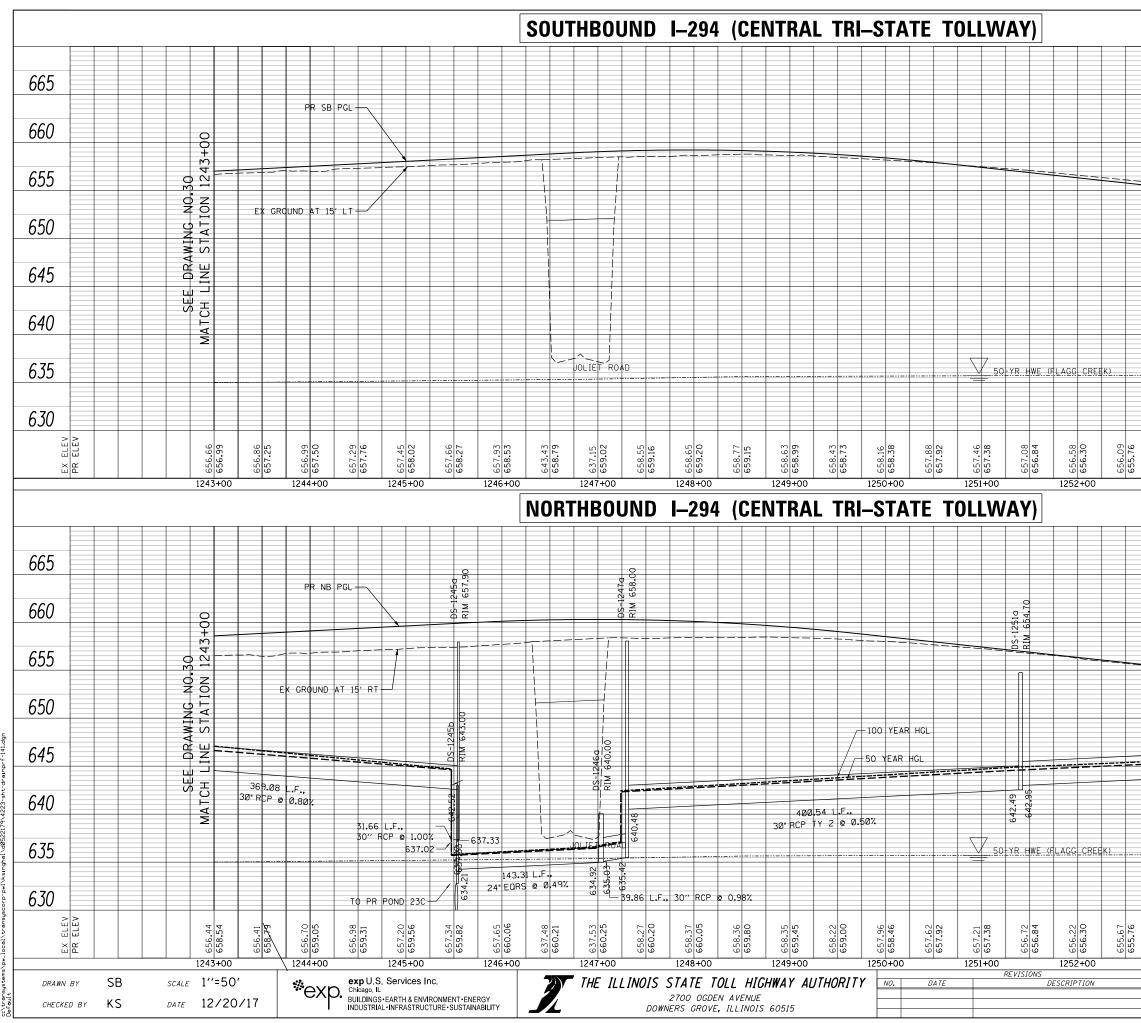
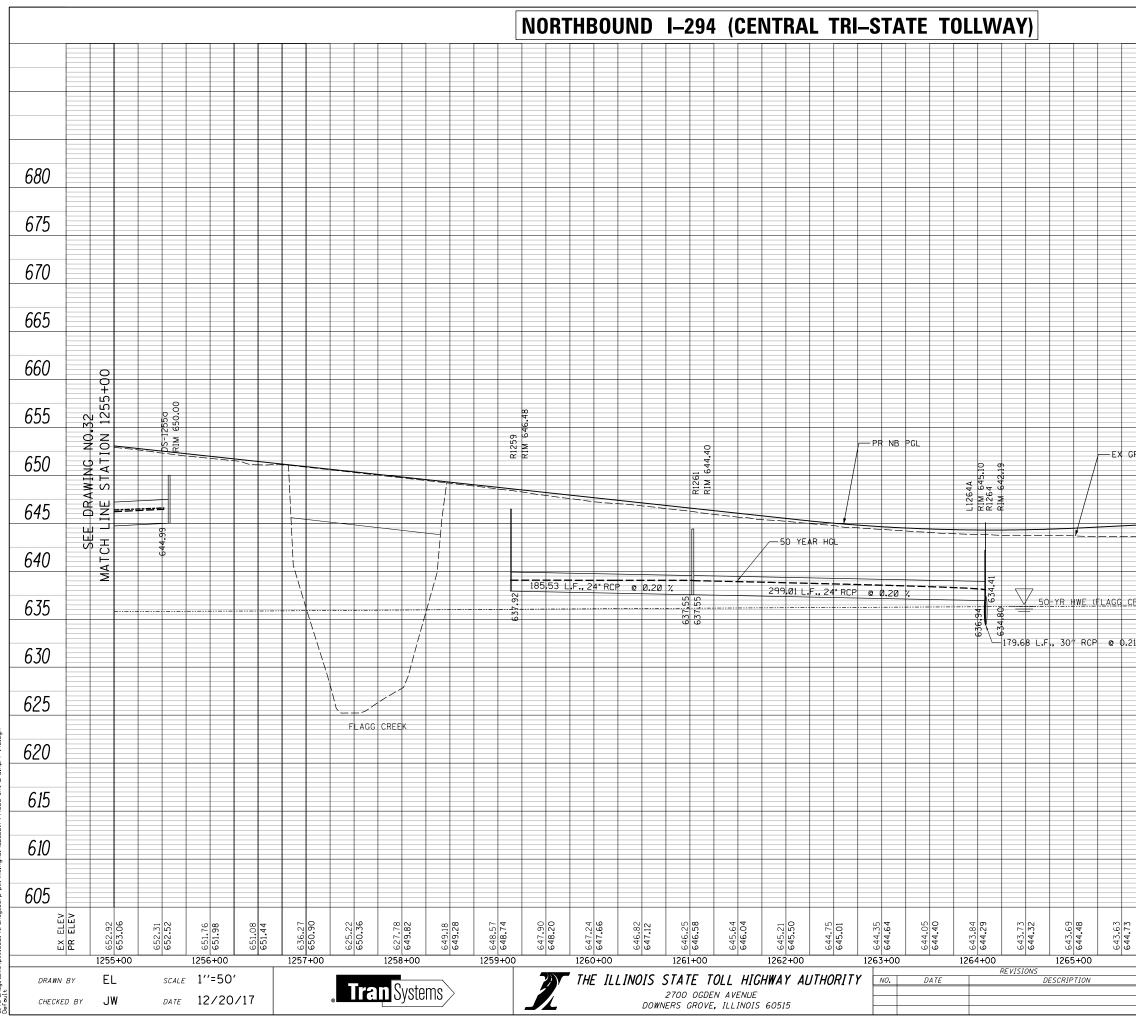


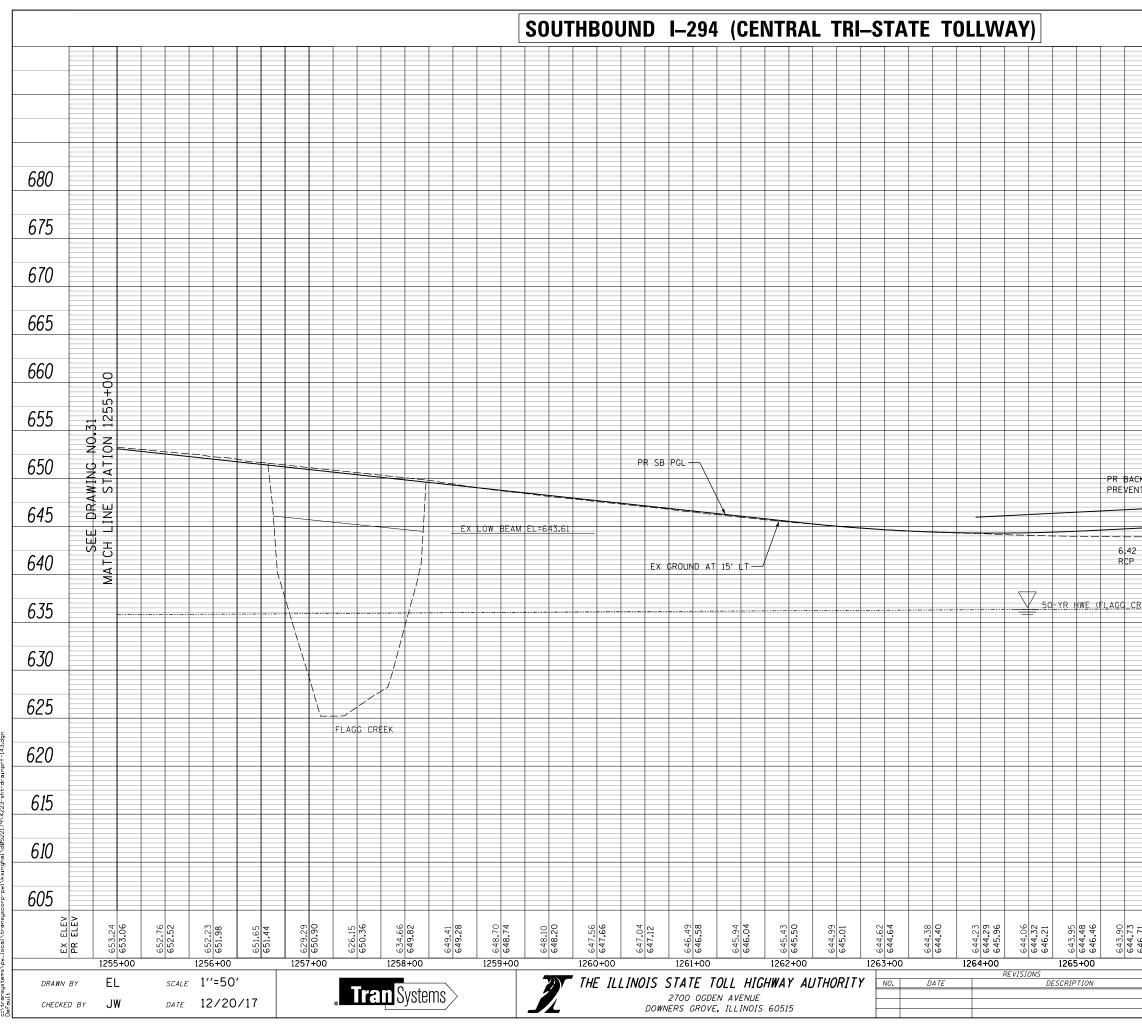
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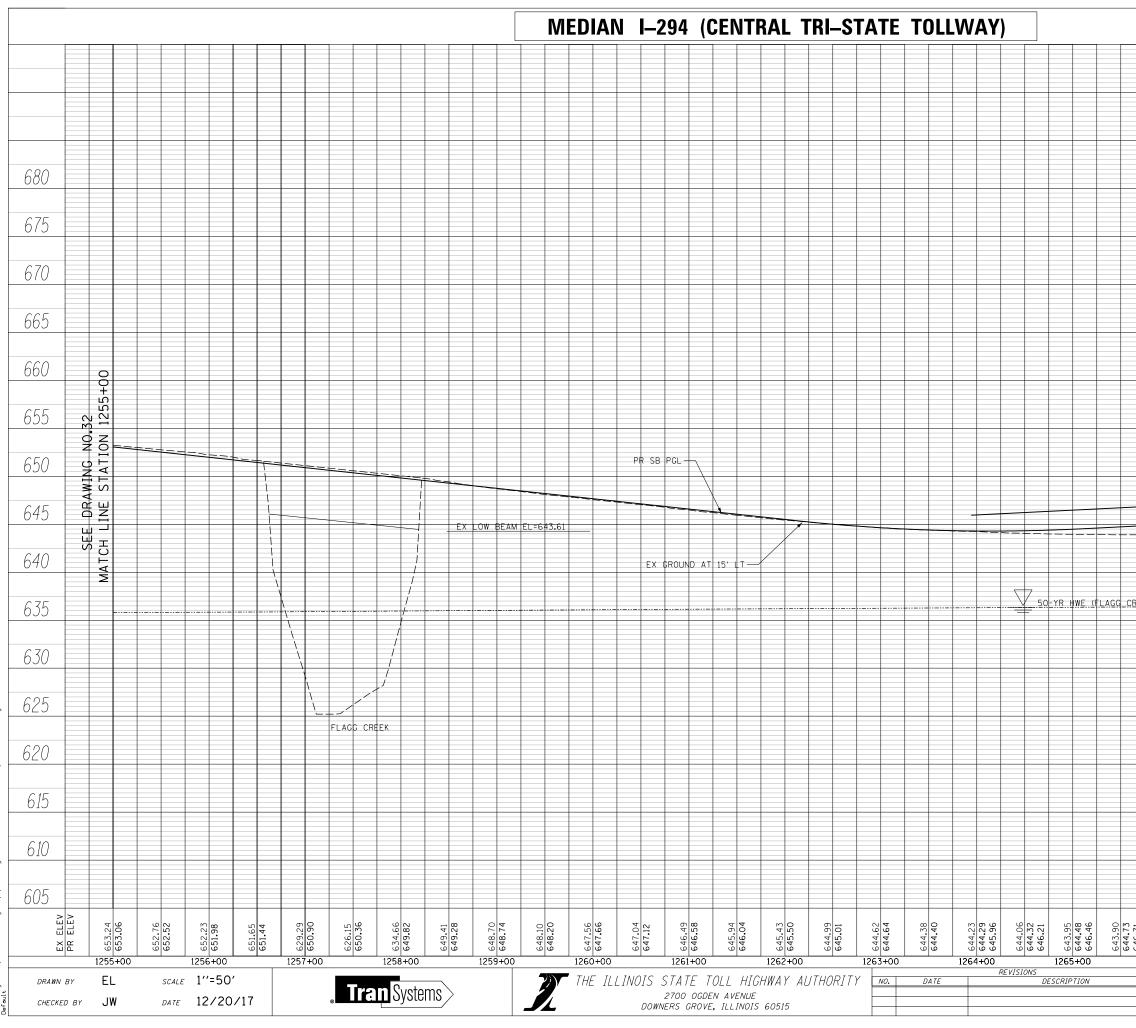
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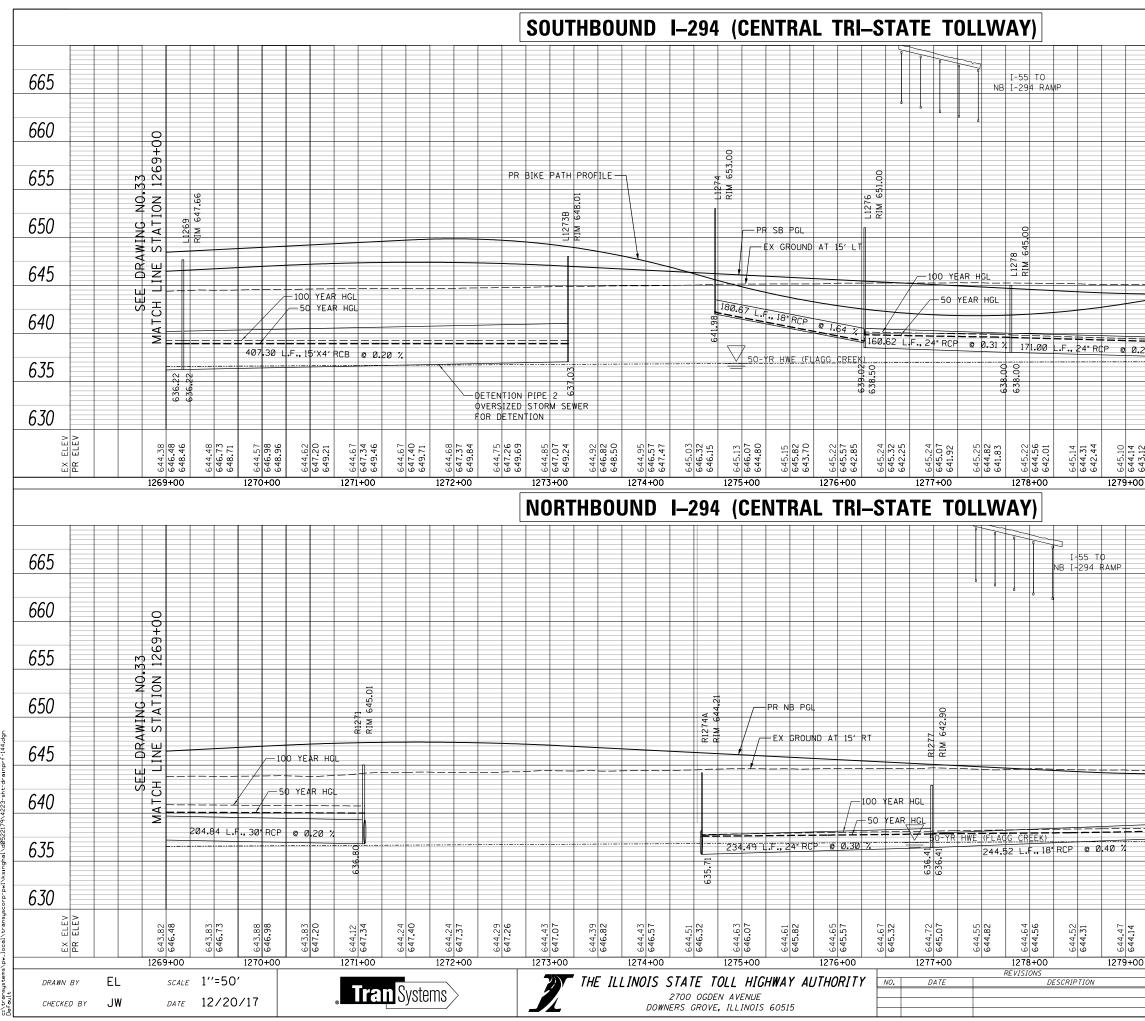


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THE ILLINOIS STATE TOLL HIGHWAY AUTHORITY 2700 OGDEN AVENUE DOWNERS GROVE, ILLINOIS 60515

			REVISIONS
Y	NO.	DATE	DESCRIPTION

CONTRACT NO. RR-14-4223	^{SHEET} NO. DP-34А
 DRAINAGE PROFILE STA. 1269+00 - STA. 1282+00	DRAWING NO. 34A OF 56

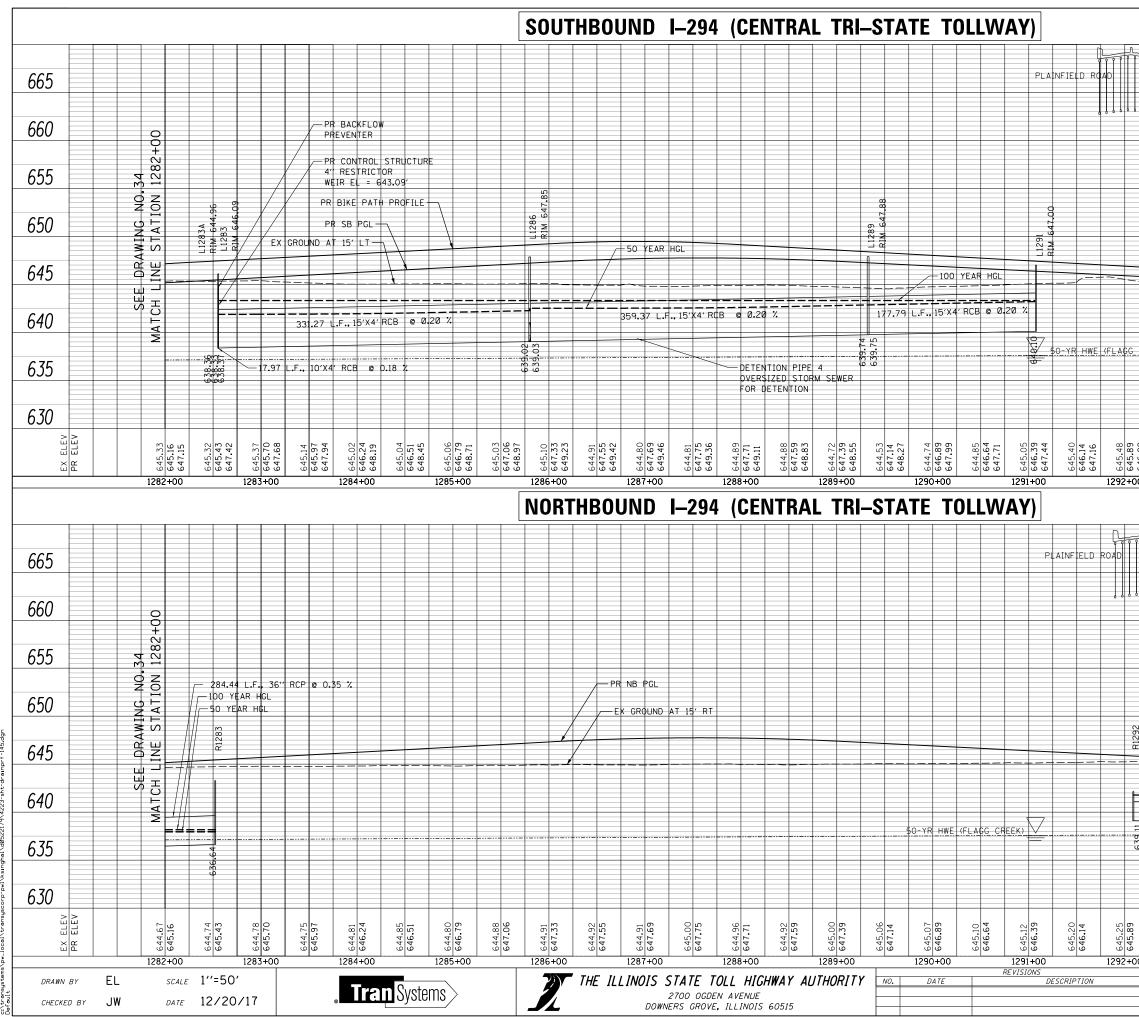


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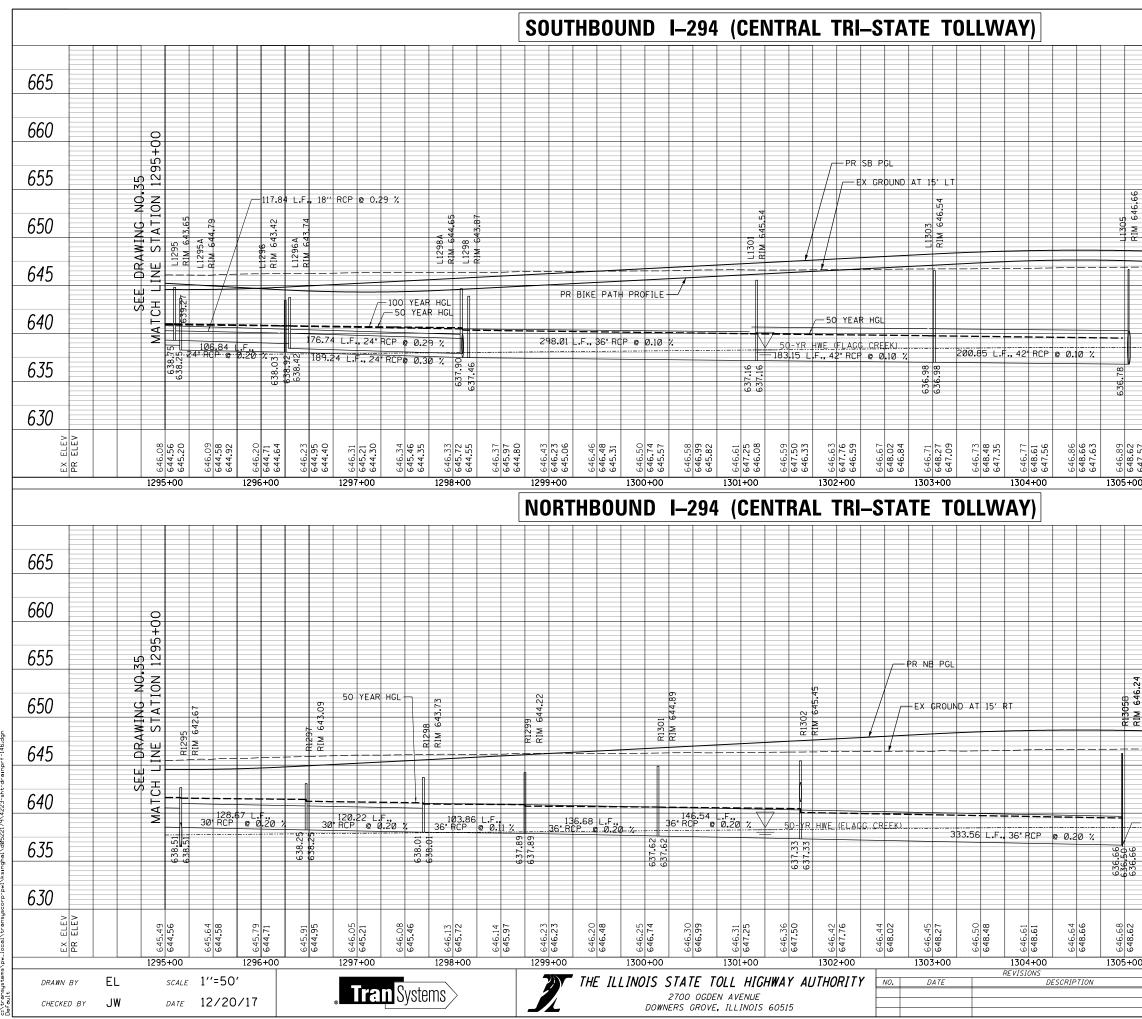


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			S						FILE					DP-3 DRAWING 36 OF	NO.

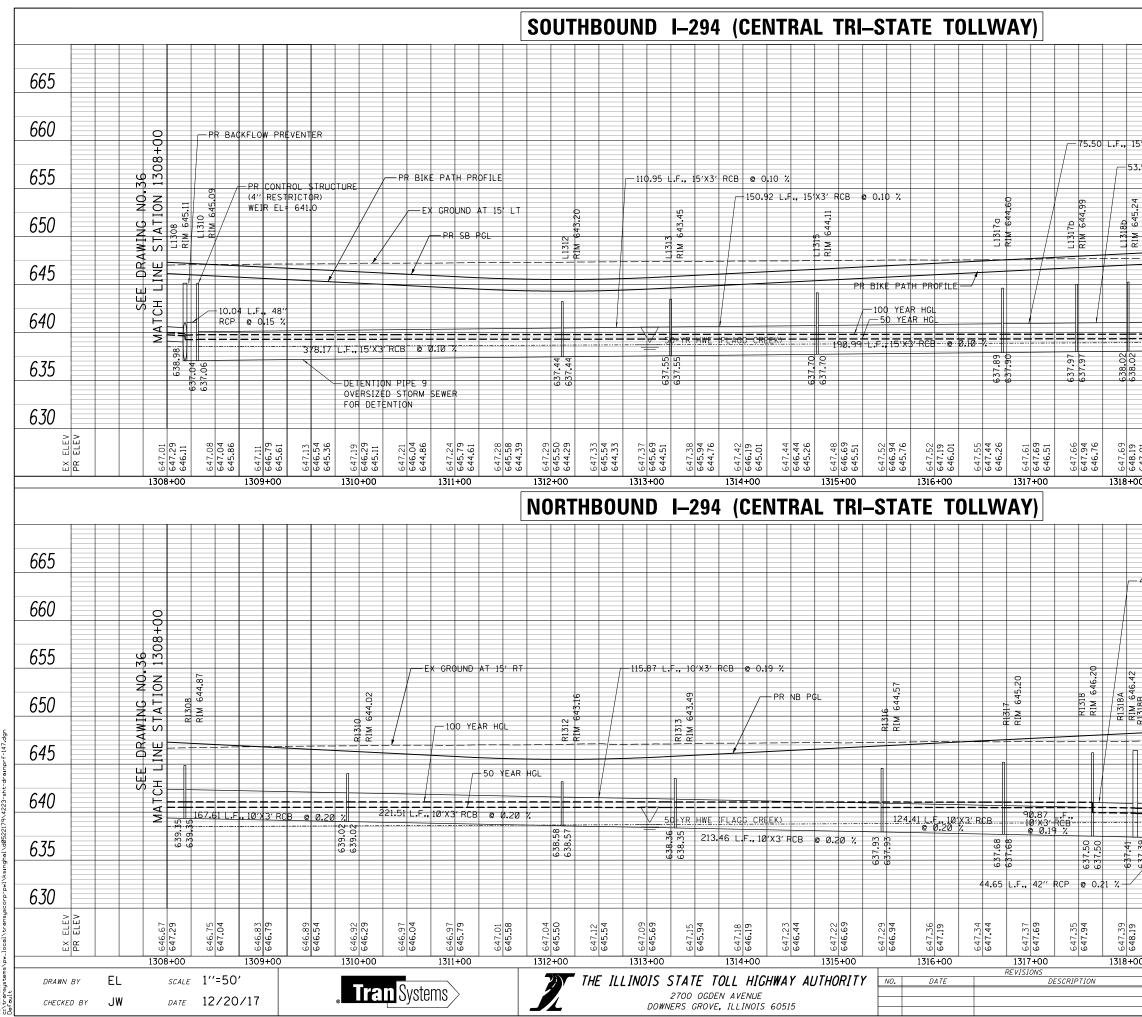
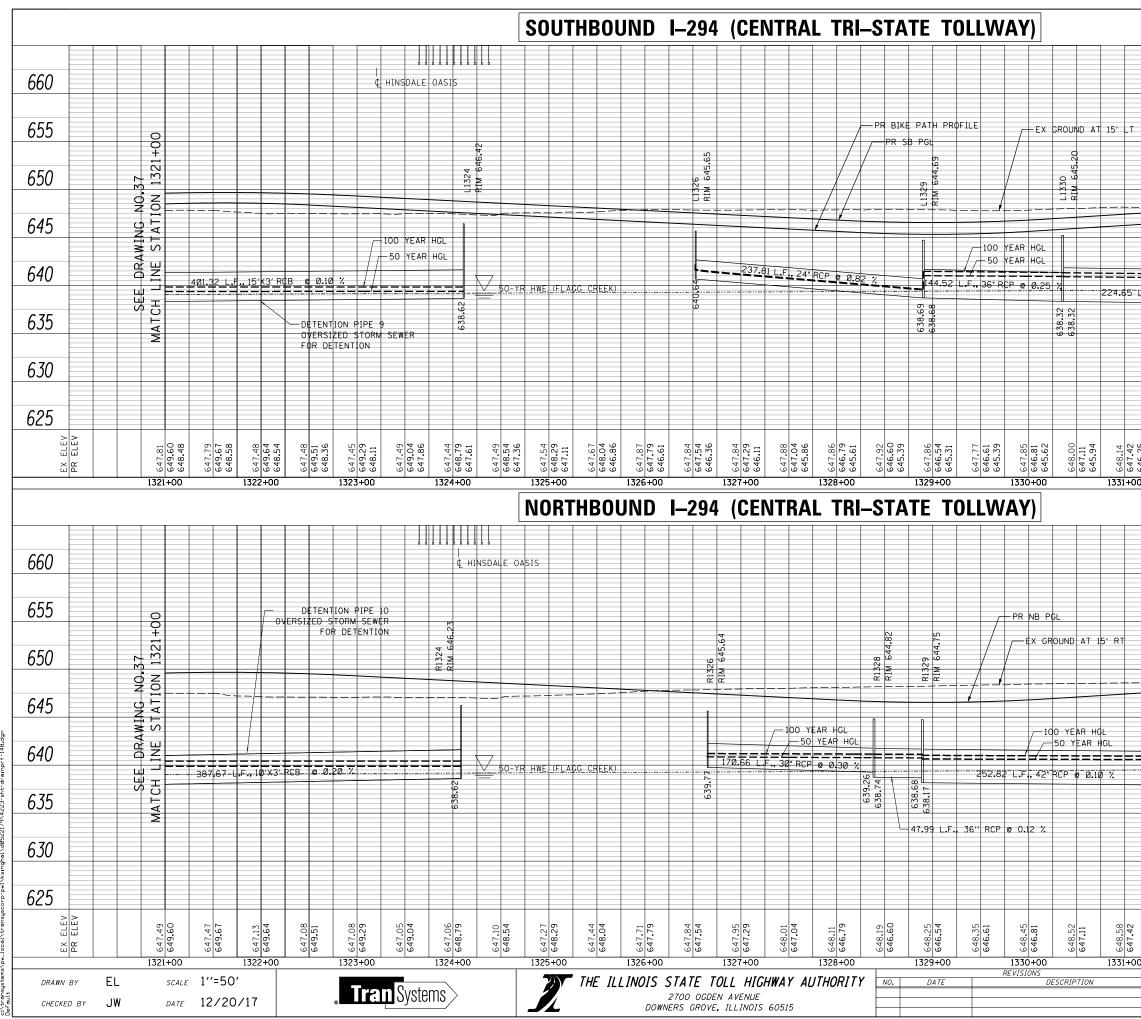
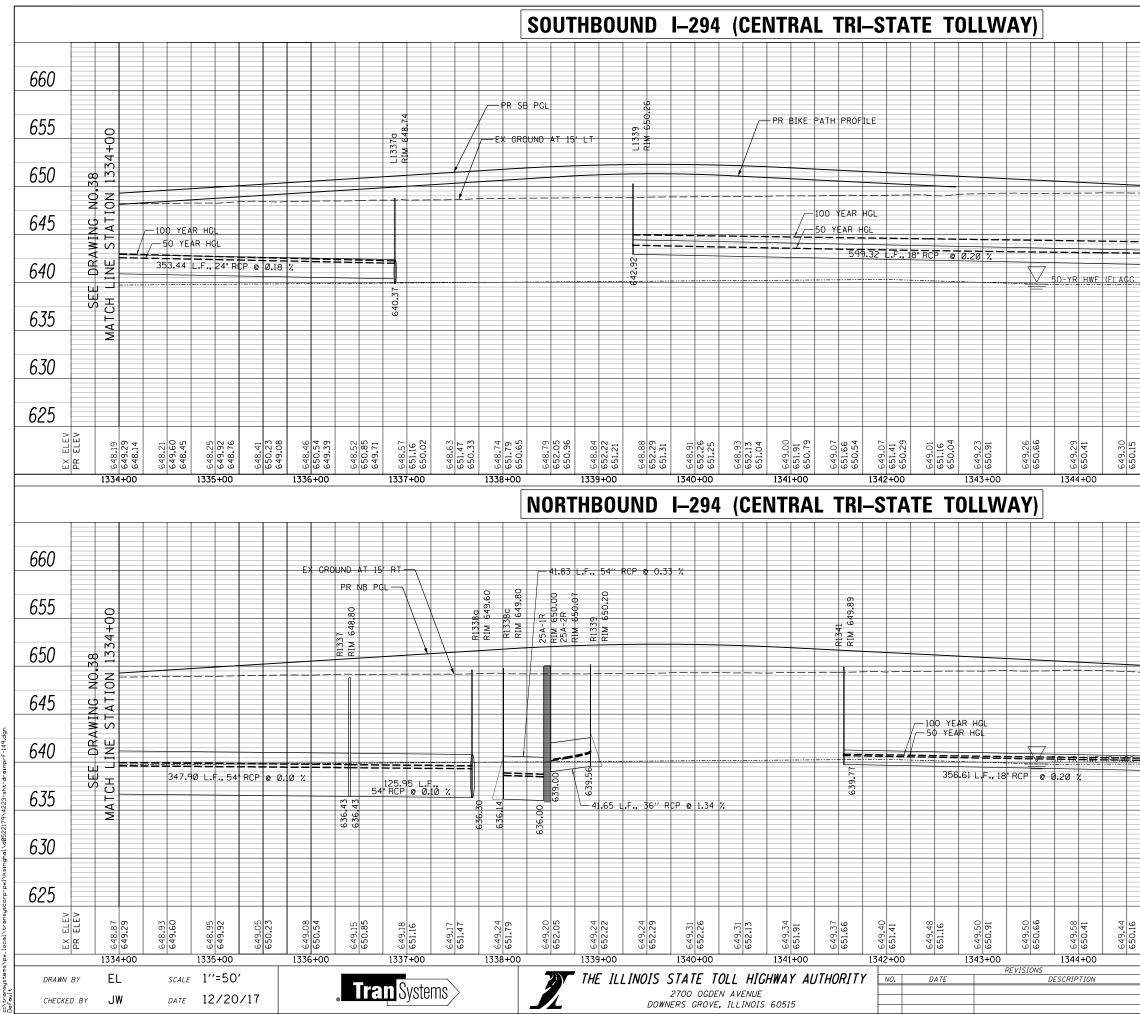


														EXHIBIT	5.7
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3.55 L.	.F., 58	15'X	3′ RC	B@	0.10 RCB	% @ 0.	10 %	2				1321	۰. رو		655
47°C49 WIX	L1318a	RIM 646.55						L1320 RIM 646.67				01.	ON DNIN		650
	-											LINE LINE	SEE UKAV		645
	1	6 <u>1.35</u>	<u>L.F.</u>	<u>15'X3</u>	* RCB	0		2		==		MATCH	5		640
	638.Uc							638.22	•						635
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			R BAC	KFLO	— — W PRE	VENT	ER		RIN_			4	E UKAW		645
		174.2	==		(3' RC	н В – М	==					- 1			640
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	-		S		DRA 130	INA	GE	PRO	FILE					SHEET N DP-3 DRAWING 37 OF	7 NO.

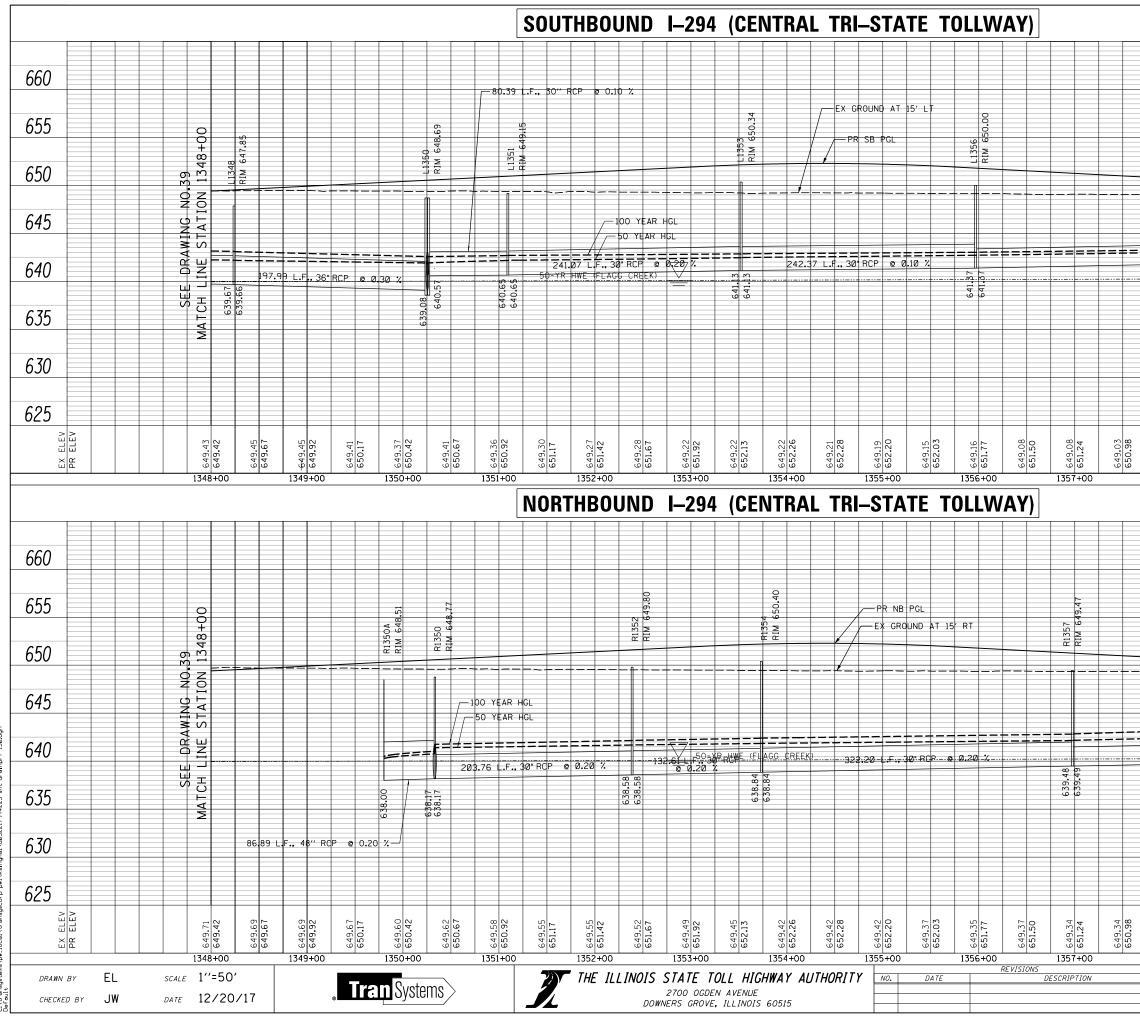


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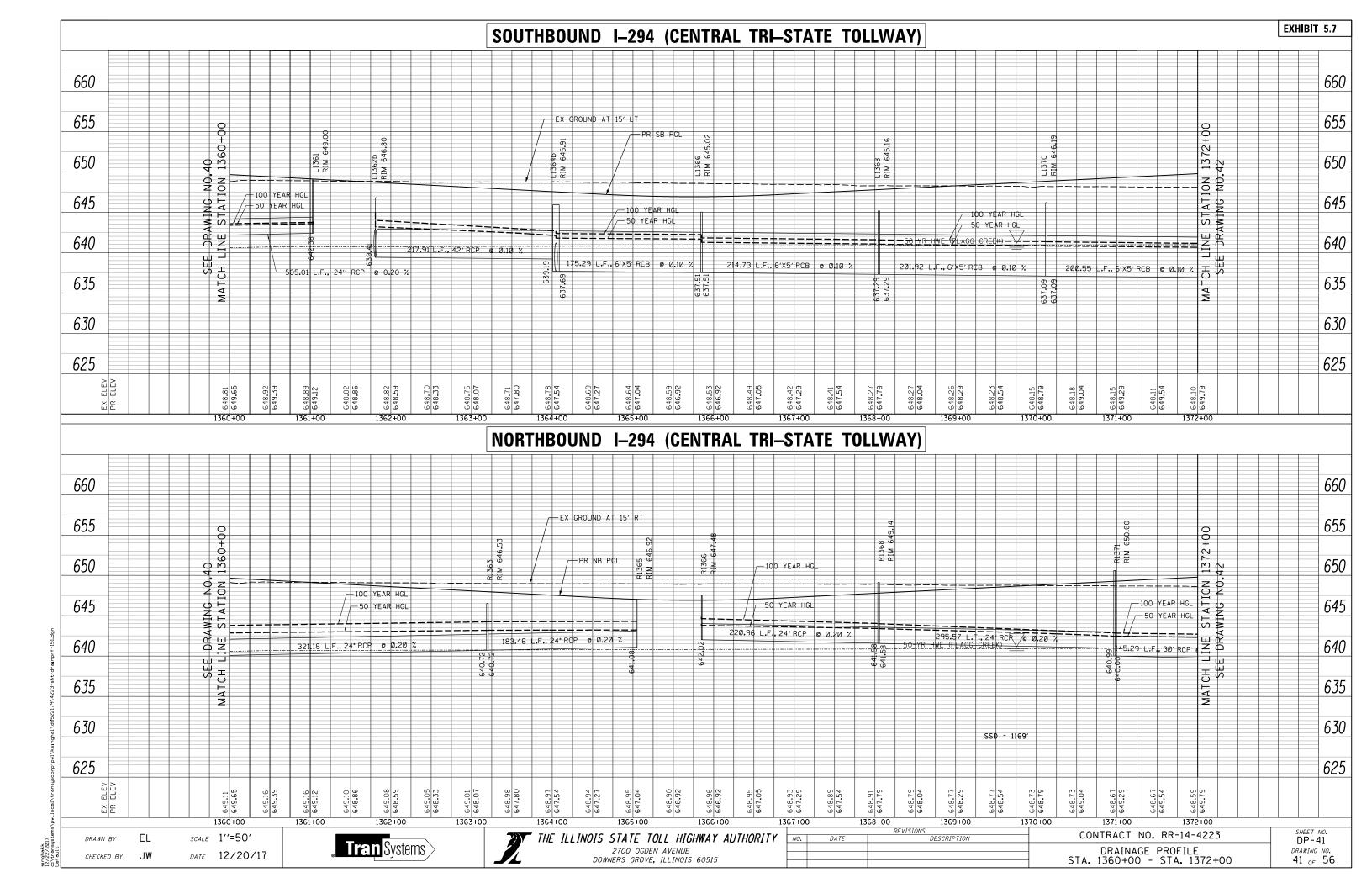
														EXHIBIT	5.7
															660
-							8		42			00+			655
						L1332	RIM 646.88		L1333 RIM 646.42			DN 1334+00	40.39		650
												LINE STATION			645
: -			e 0.		==:	= 1			641.00			LINE	EDRA		640
						638.01			6			МАТСН I	SEE		635
			35	3.44	L.F.,	24" f	CP C	0.18	×						630
															625
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							ۍ ا								630
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)	648.63	647.73	648.70	648.05	648.74	648.36	648.79		648.81	648.98	648.87				
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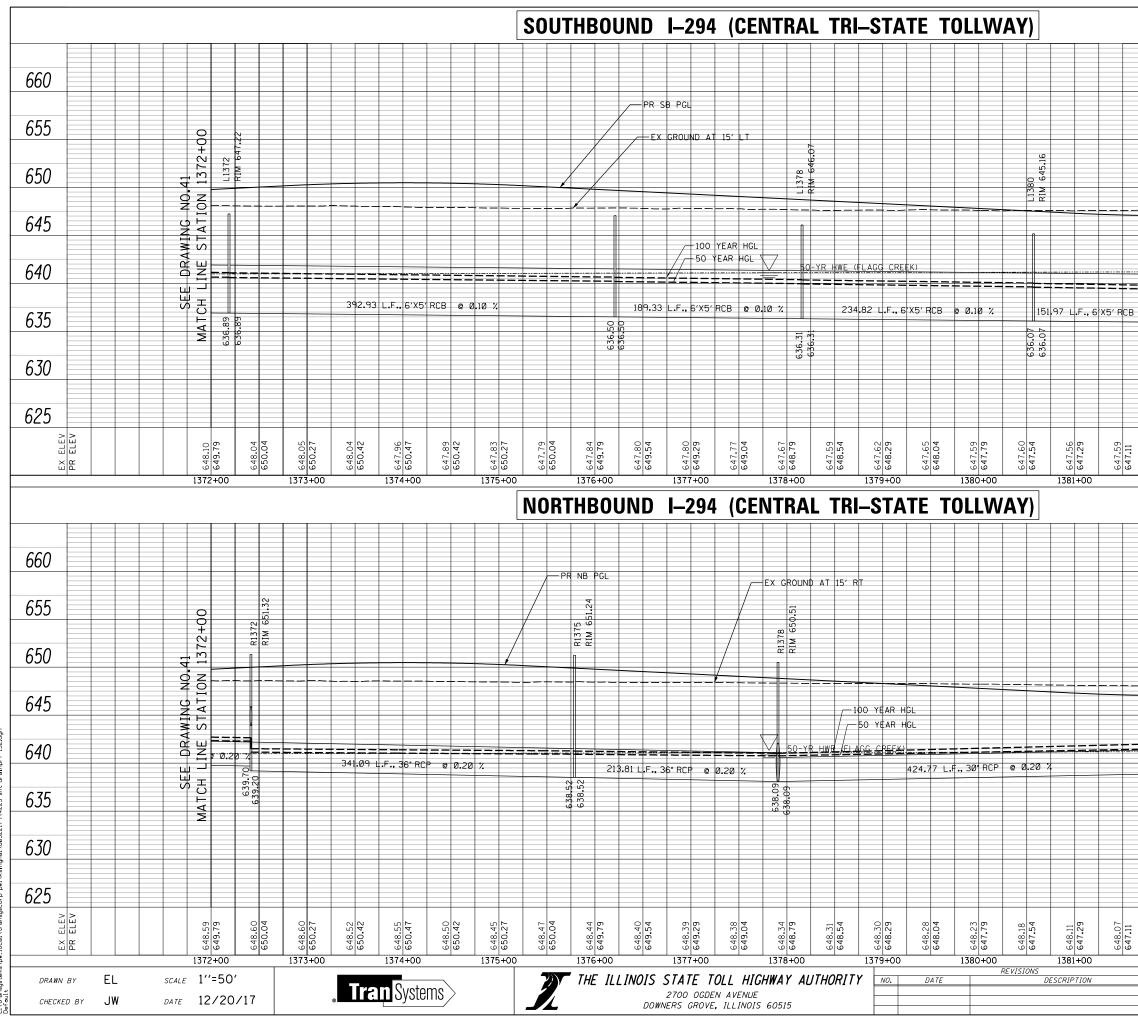


														EX	HIBIT	5.7
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			L13450 RIM 647.						 1347B	RIM 647.60		7		N 1348+00	0.40	650
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	134.	J+00	1		1540	+00	1		1347	-00	1		1540	+00		
																660
			648.08	96	.53 L	.F., 3	0" R	CP (0.20) %—		B .47 . 25		00+		655
		 R1345	I RIM 64						R1347			R1347B RIM 647.25		N 1348+00	0.40	650
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			S	TA.	DR/ 1334	4+00	.GE D -	PRO STA	FILE	48+	-00			D	DRAWING 39 OF	NO.

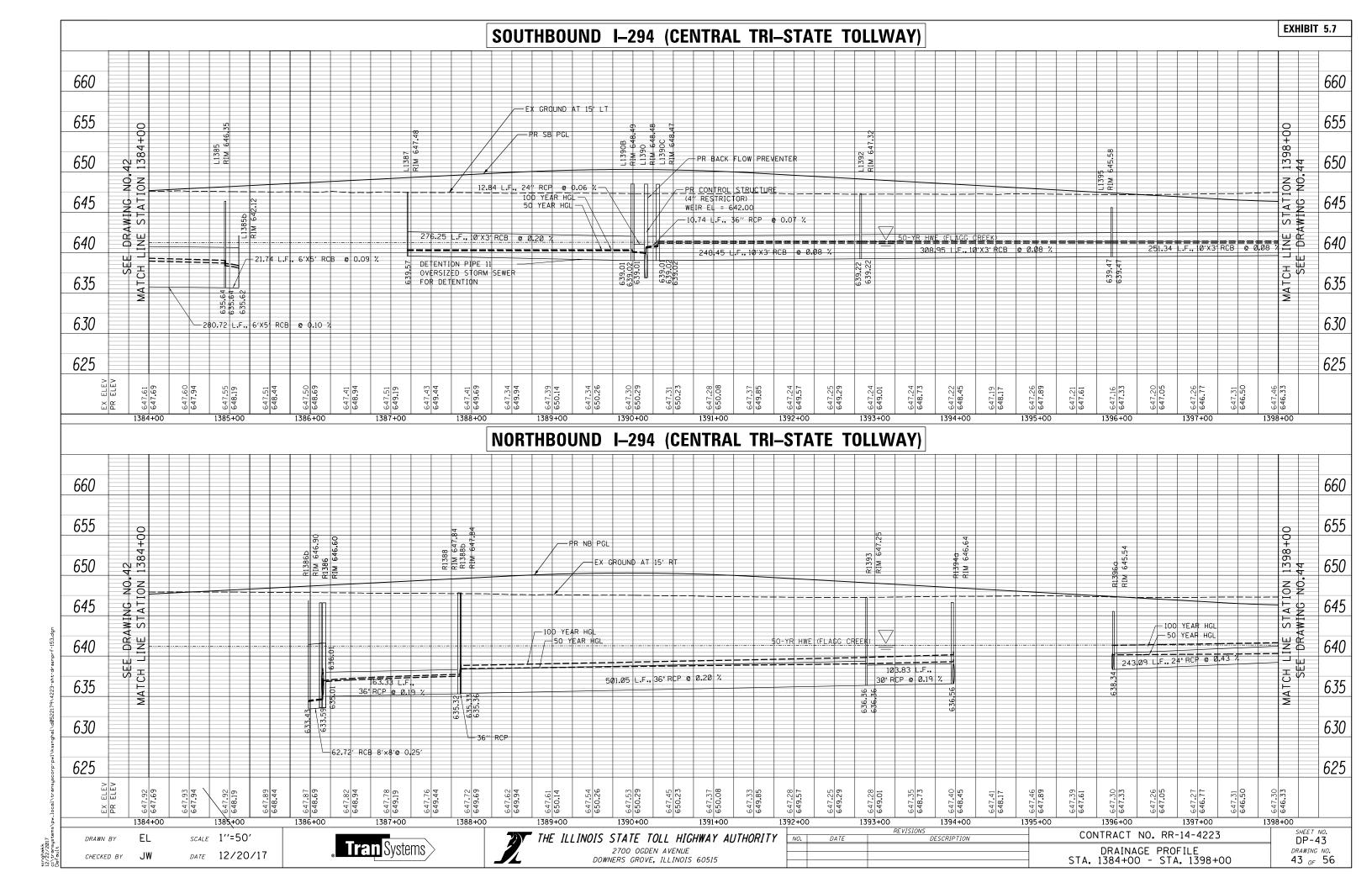


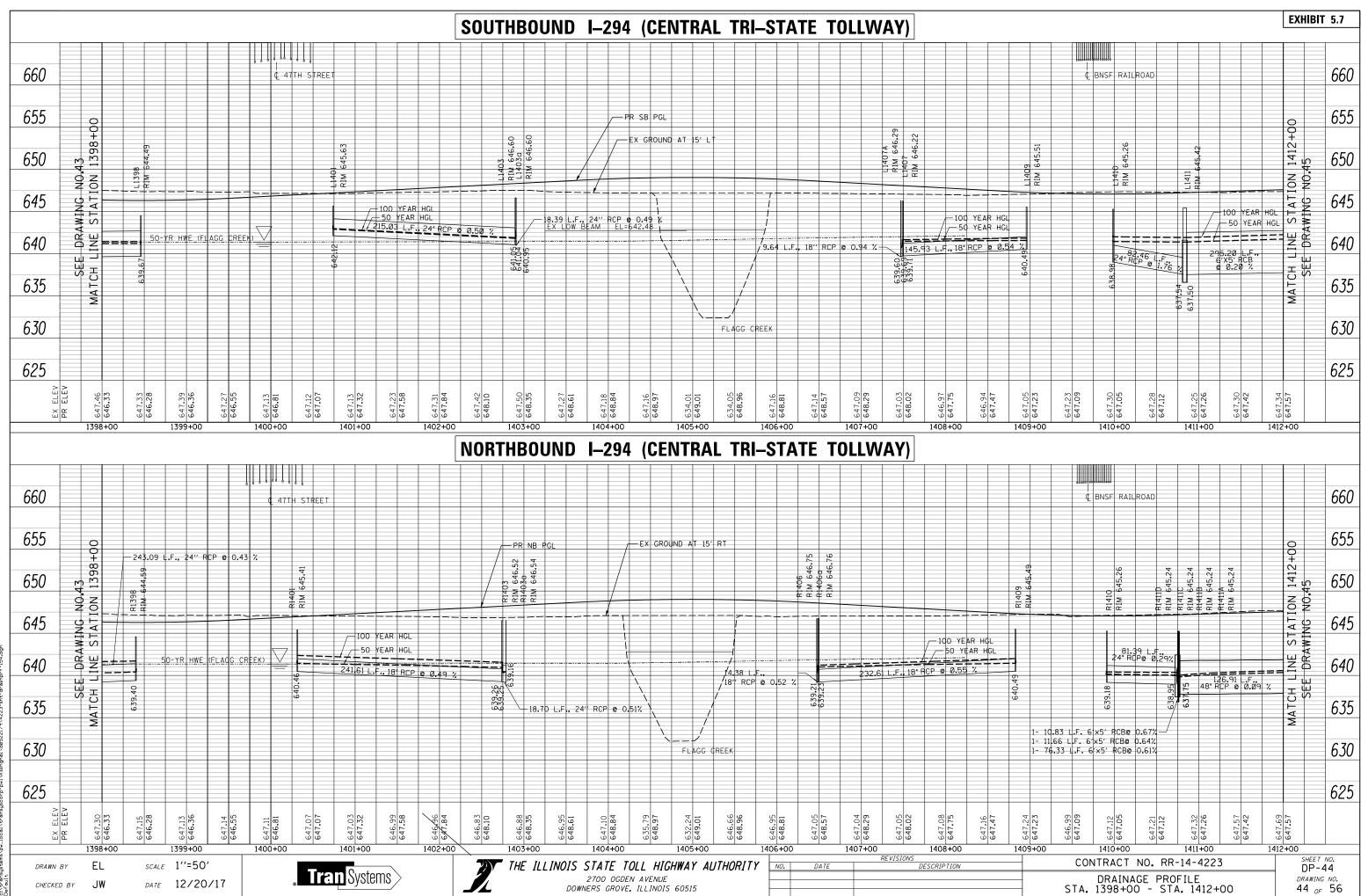
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						0.00
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L1382 RIM 645.24						650
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63 63						630
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		647.68 647.21	647.63 647.44	647.61 647.69		
+00	1	1383+00		1384+00		
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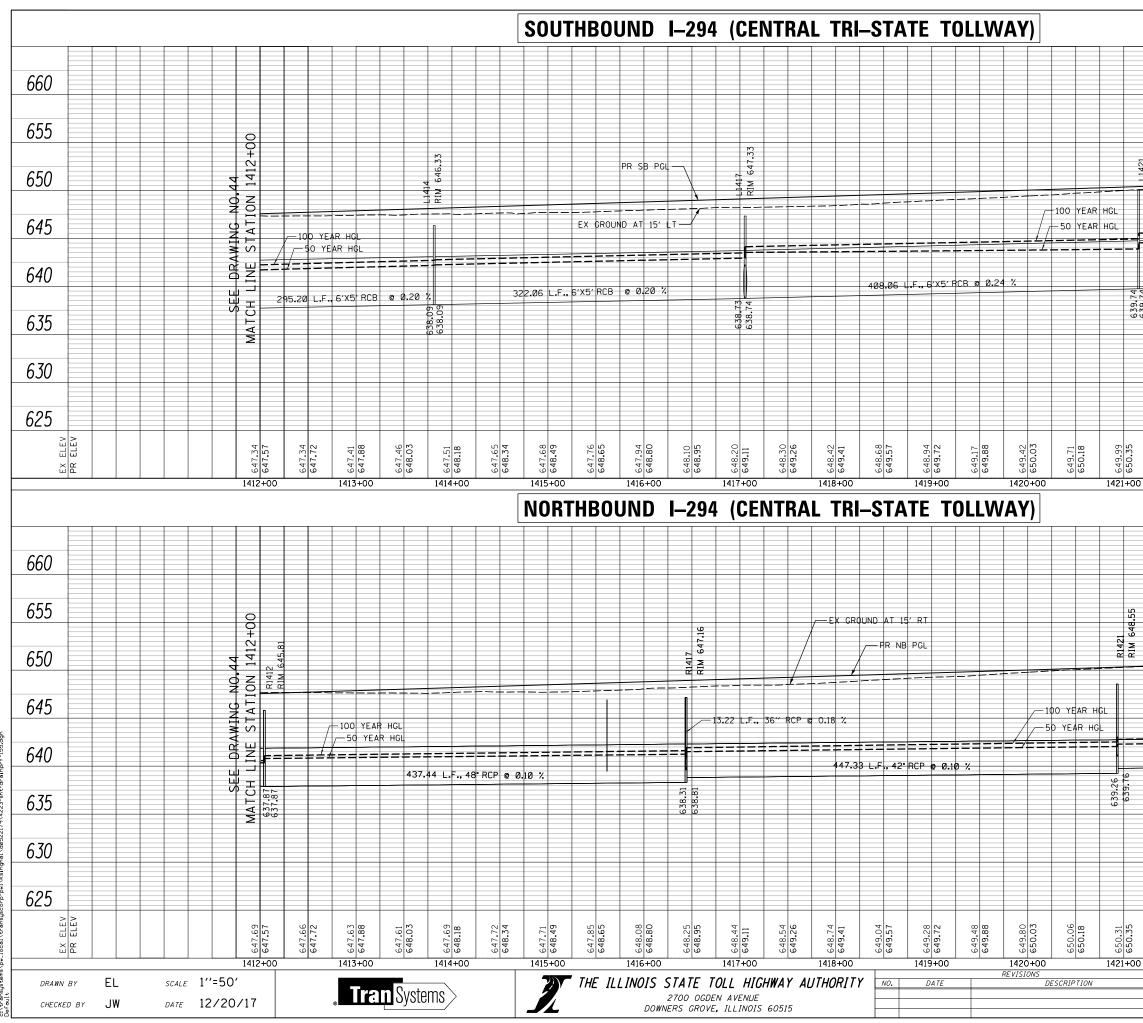


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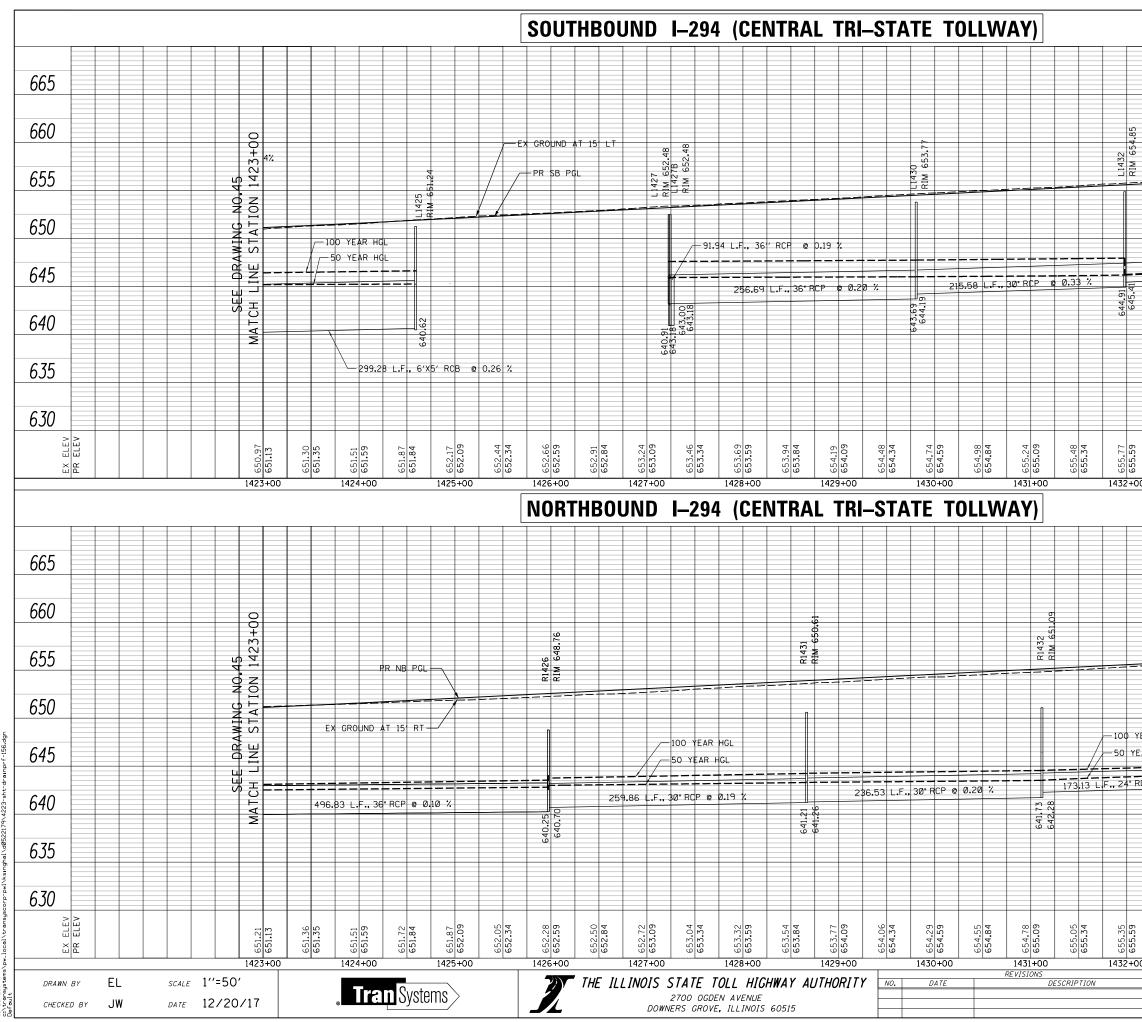


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AR HO			23.44 L.F.,	5	RAWI			0.45
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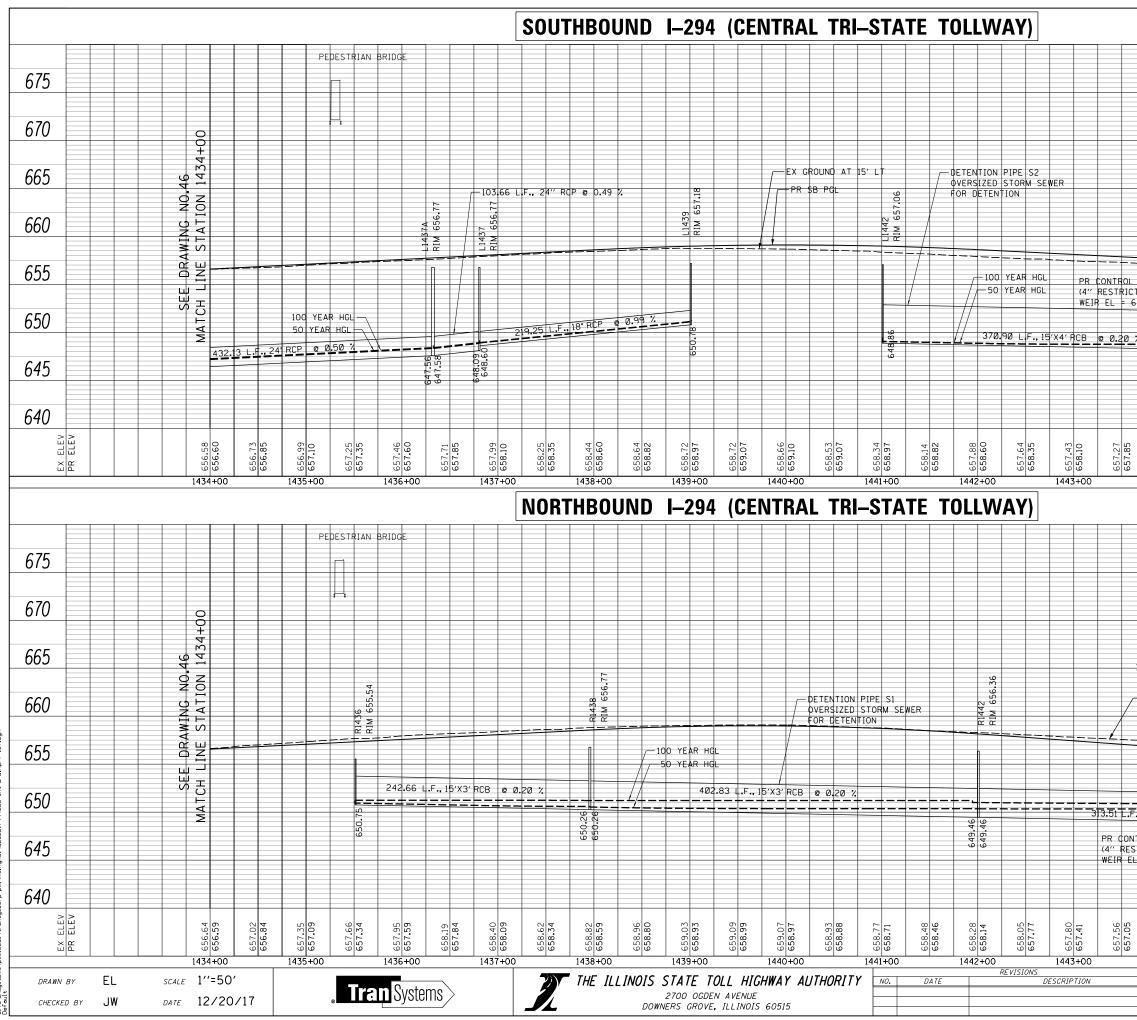
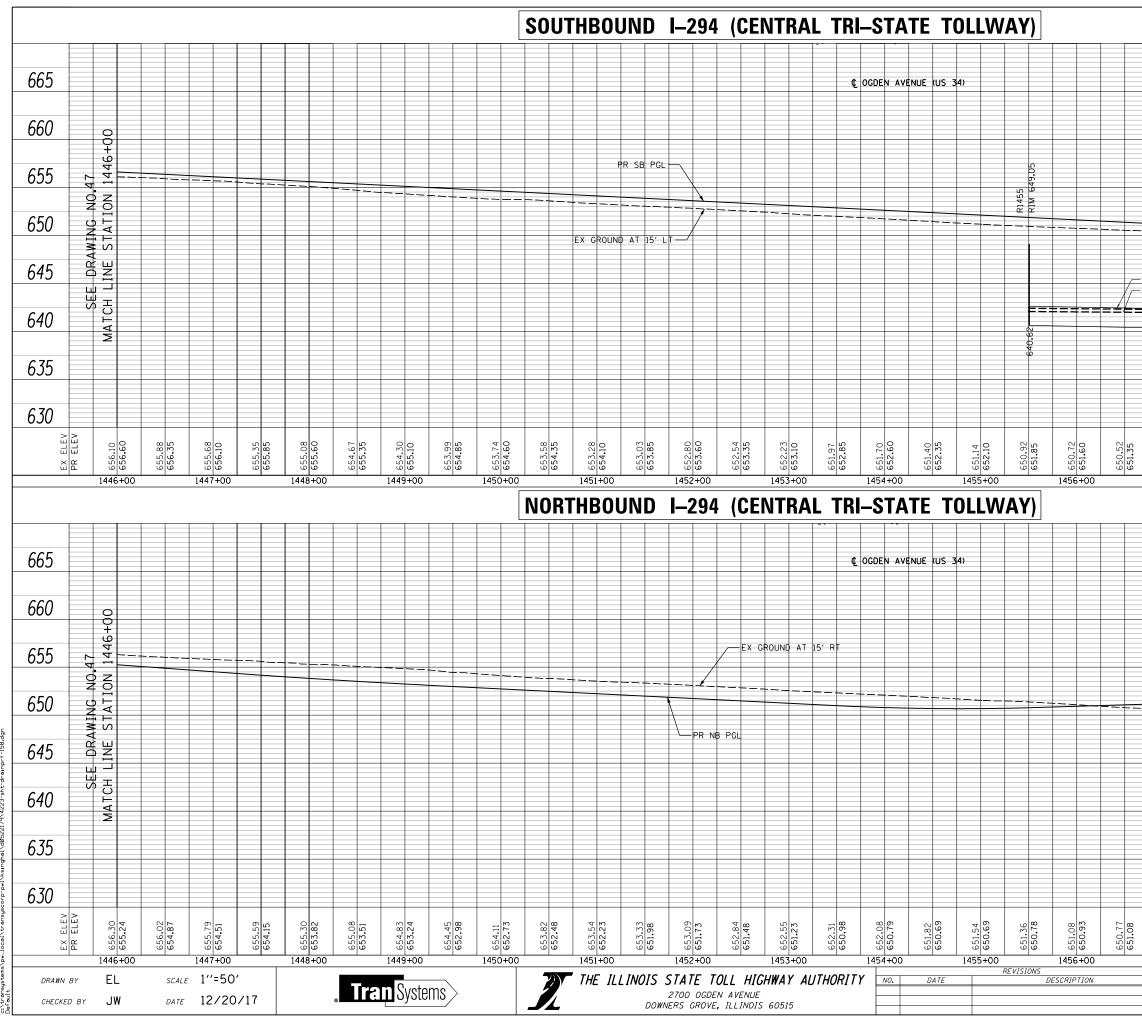


		EXHIBIT 5.7
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	0	670
	N 1446+00	665
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		675
	00	670
7.59 L.F., 42" RCP @ 1.04 %	1446	665
EX GROUND AT 15' RT 50 60 60 60 60 60 60 60 60 60 6	R1445C R14455 R144456 R144456 R144456 R1456 R1456	660
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F., 5'X3' RCB @ 0,20 %	MATCH	650
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657.33 656.69 656.32 656.33 656.33 655.33 655.33 655.33 655.33 655.33 655.33 655.33 655.33 655.33 655.33 655.55 655.55 65	656.59 655.24 655.24	
1444+00 1445+00 CONTRACT	1446+00 NO. RR-14-4223	SHEET NO. DP-47
DRAINA STA. 1434+00	GE PROFILE) - STA. 1446+00	DRAWING NO. 47 _{OF} 56



														EXH	IBIT	5.7
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1-	-				ITRA	CT			-14-	4223				<u> </u>	SHEET N DP-4	<i>io.</i> 8
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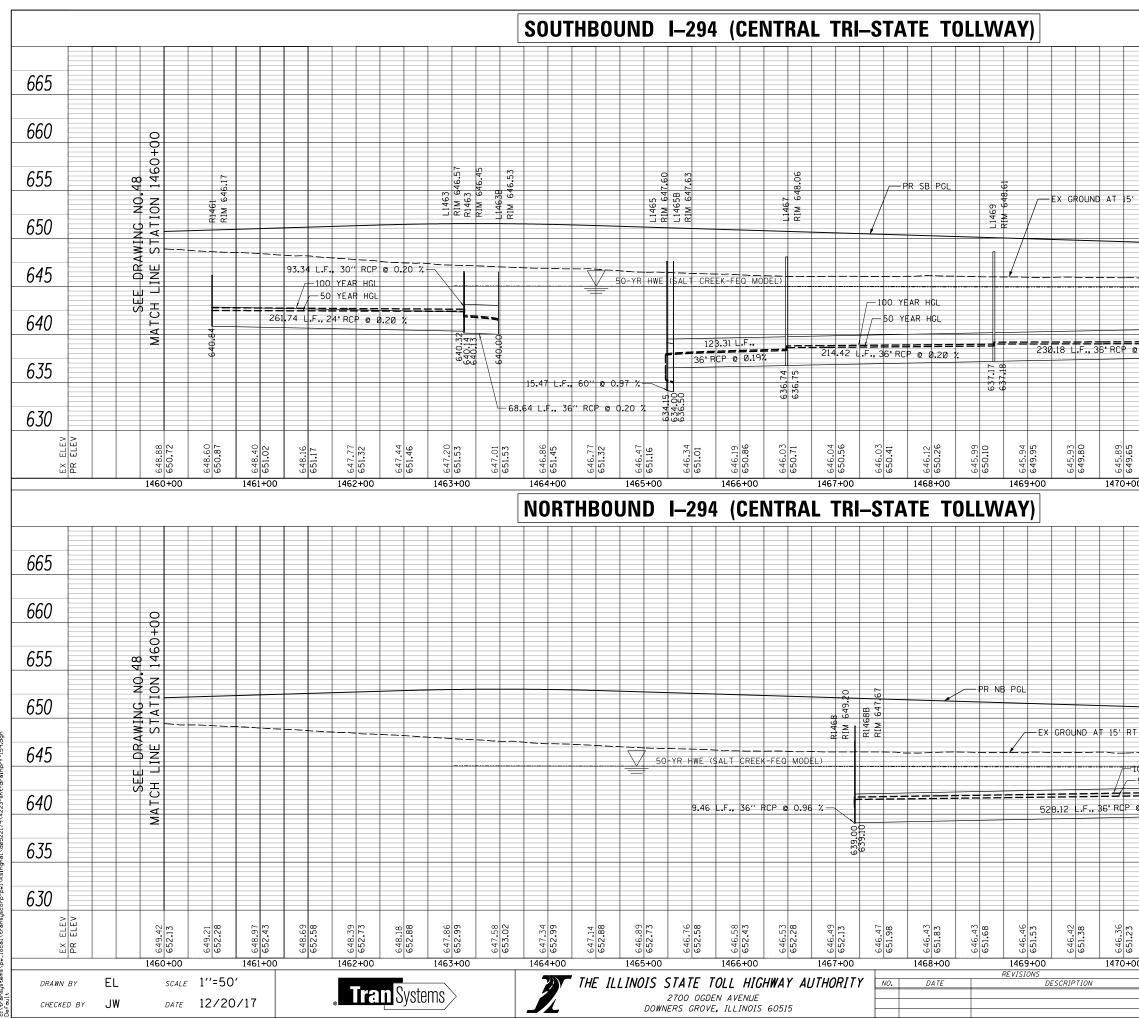
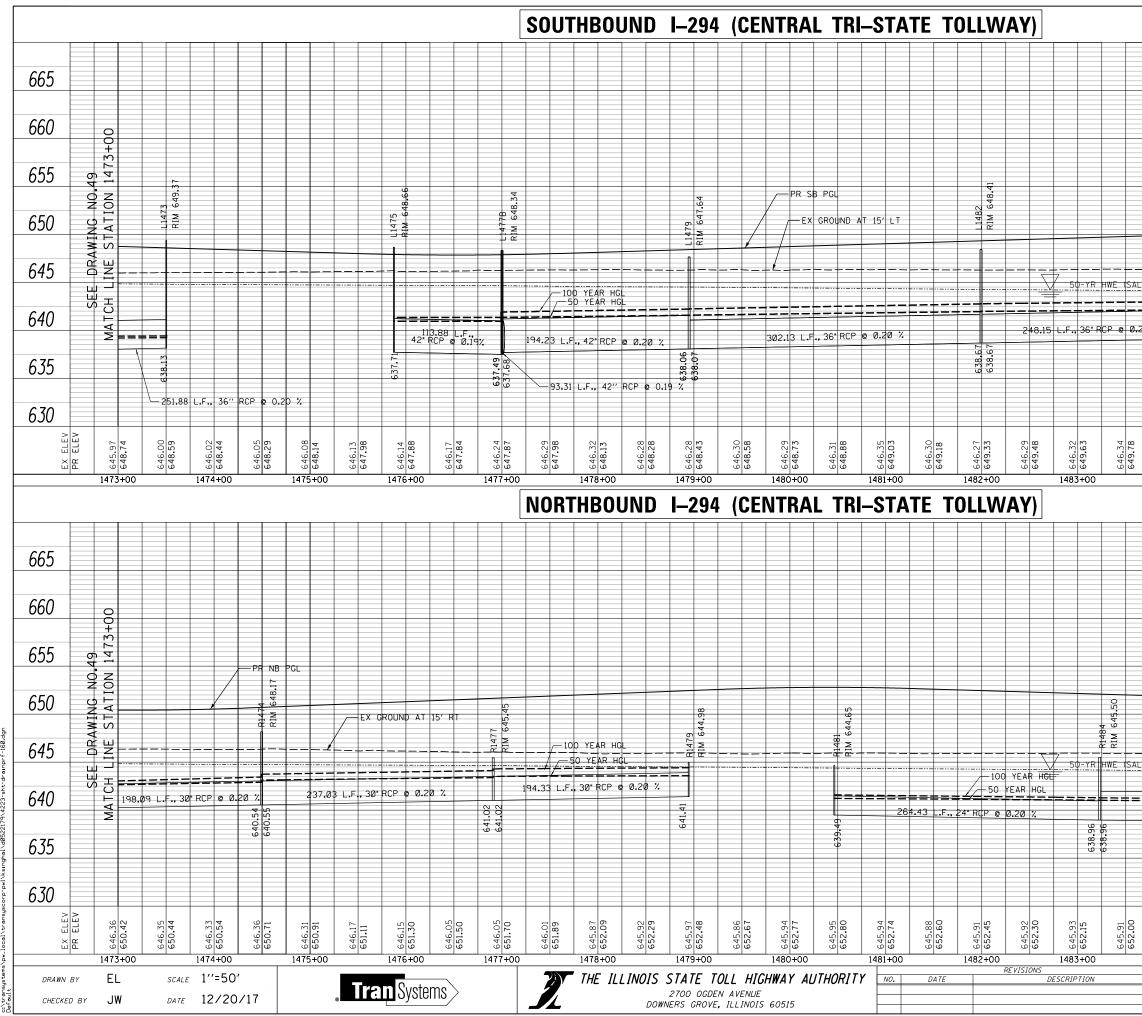
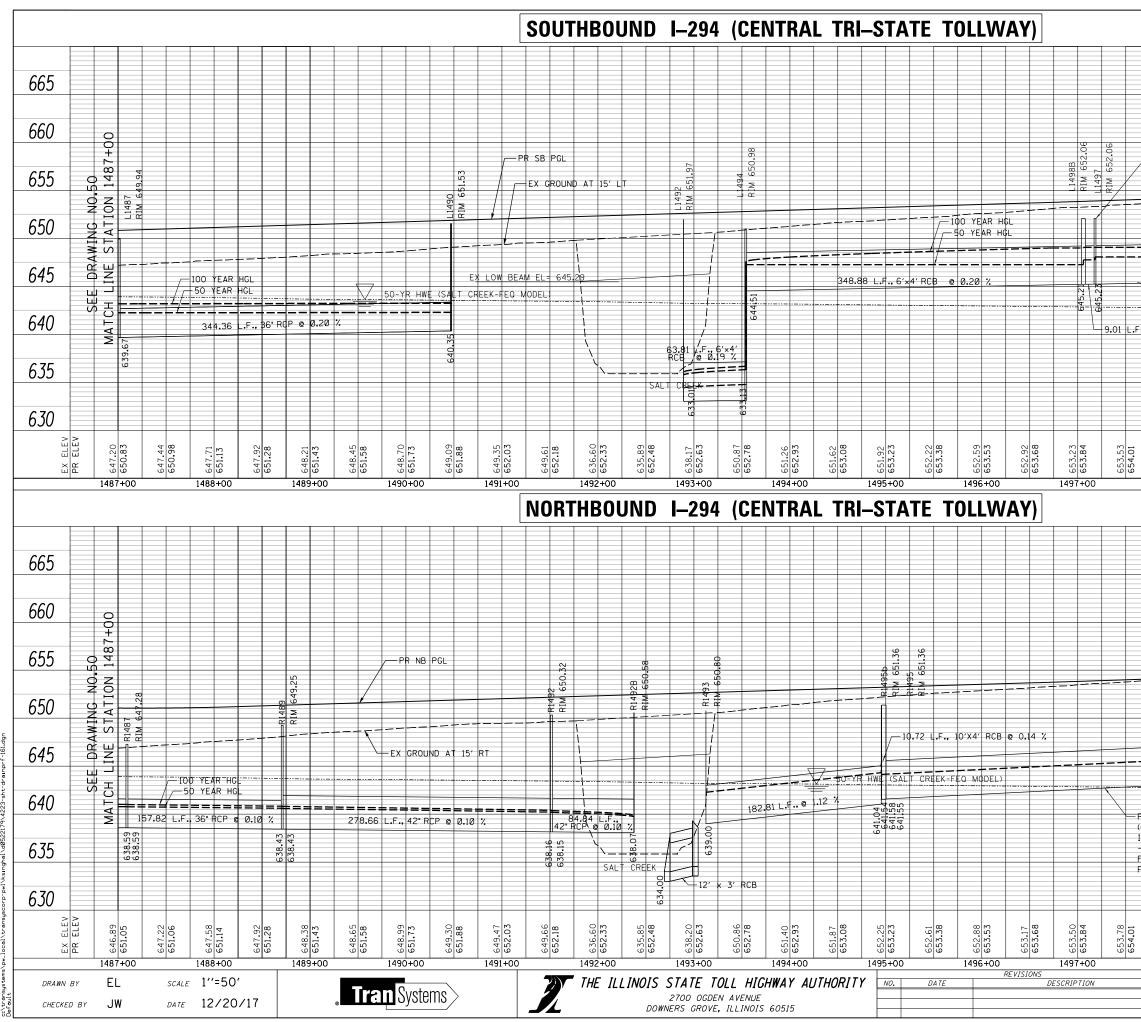


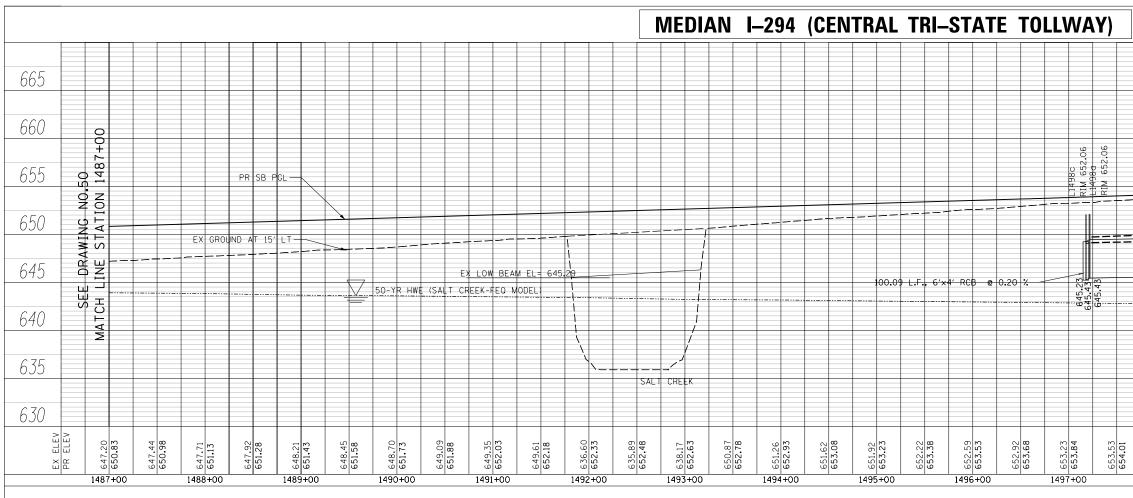
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														EX	HIBIT	5.7
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AL T	CREE	к-FEC	— — 2 мос	=				YEAF						-	SEE DRAWI	645
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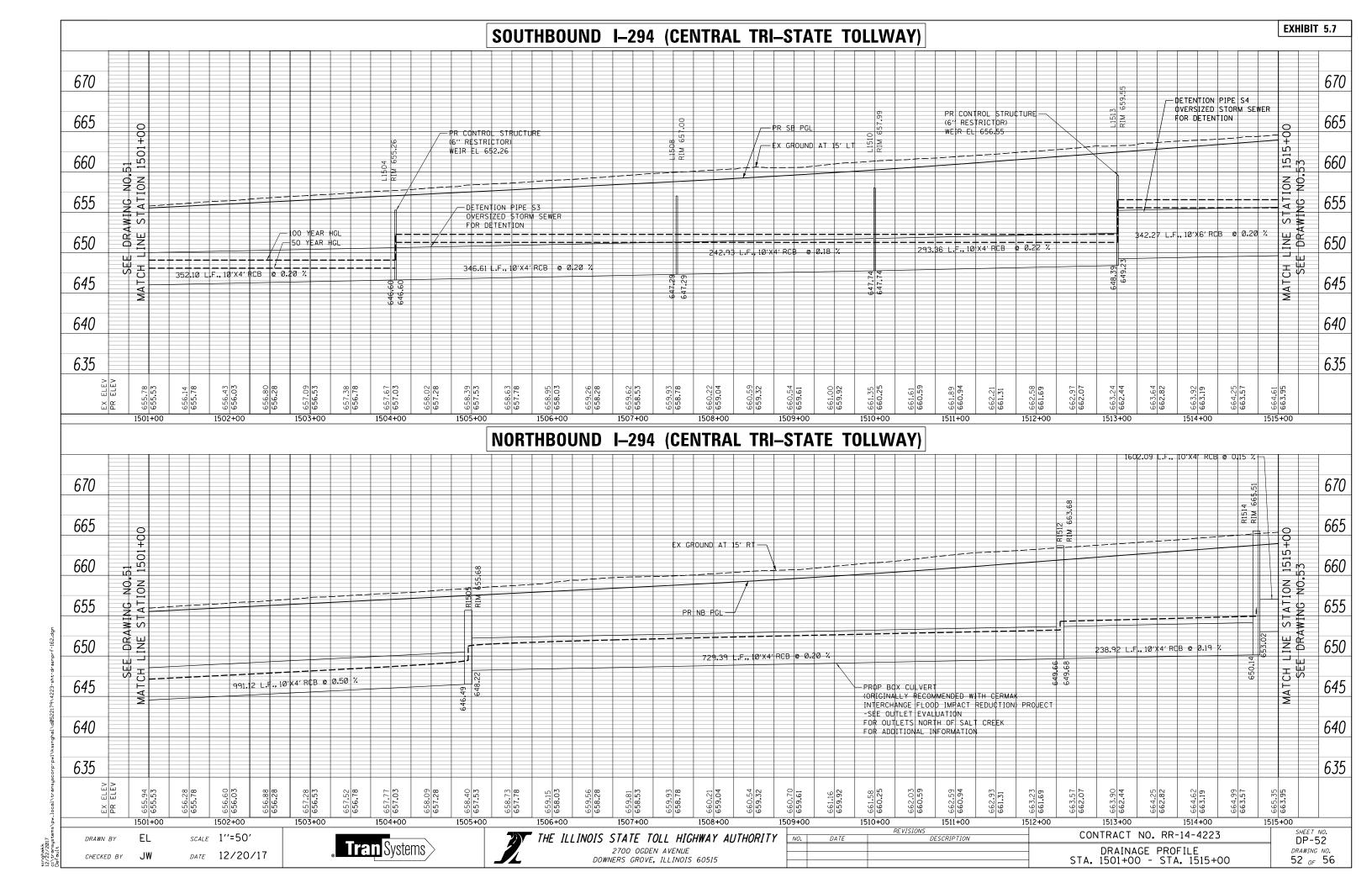


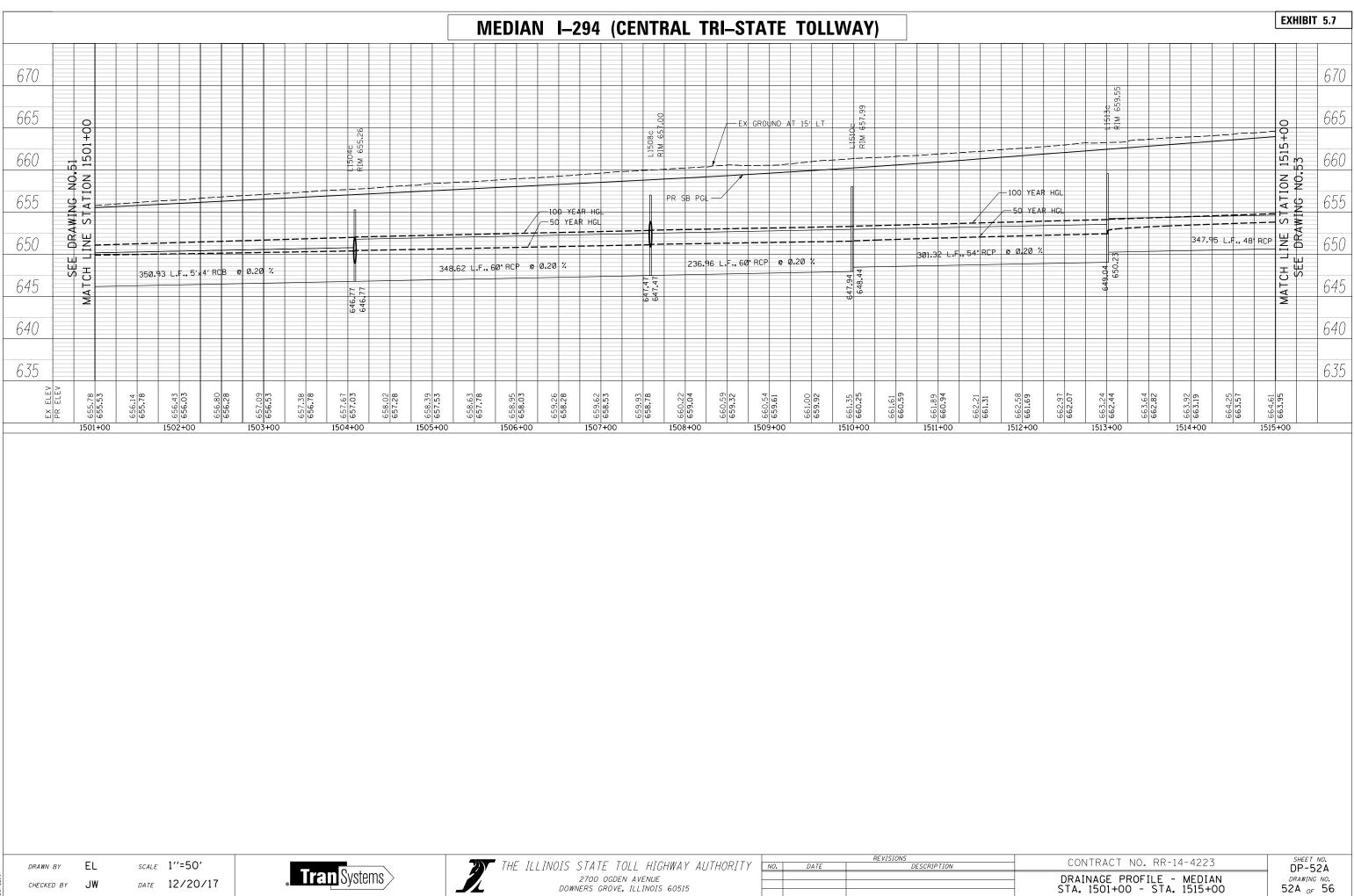
THE ILLINOIS STATE TOLL HIGHWAY AUTHORITY 2700 OGDEN AVENUE DOWNERS GROVE, ILLINOIS 60515

		REVISIONS
NO.	DATE	DESCRIPTION

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CONTRACT NO. RR-14-4223	SHEET NO. DP-51A
DRAINAGE PROFILE STA. 1487+00 - STA. 1501+00	DRAWING NO. 51A _{OF} 56







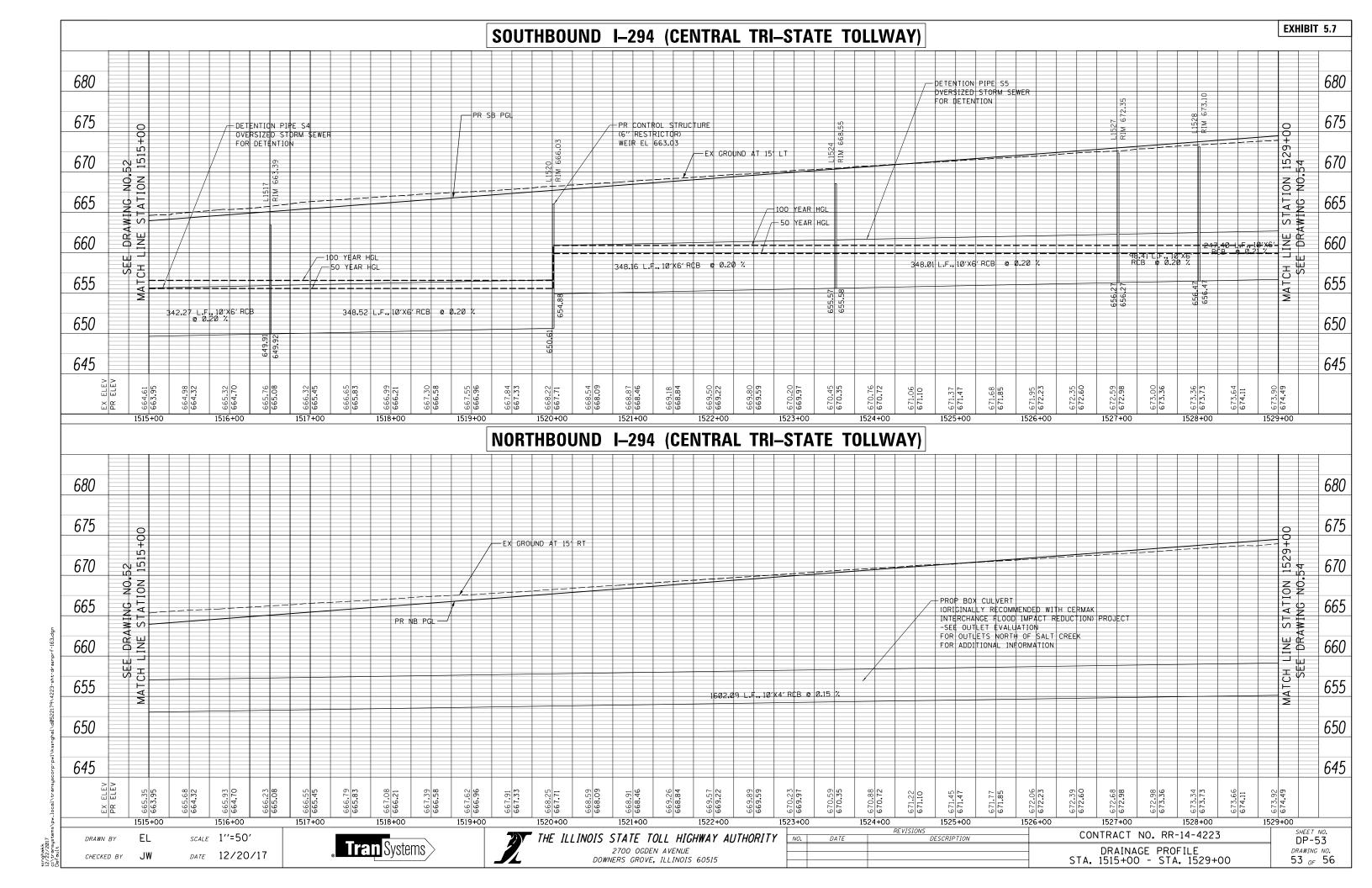


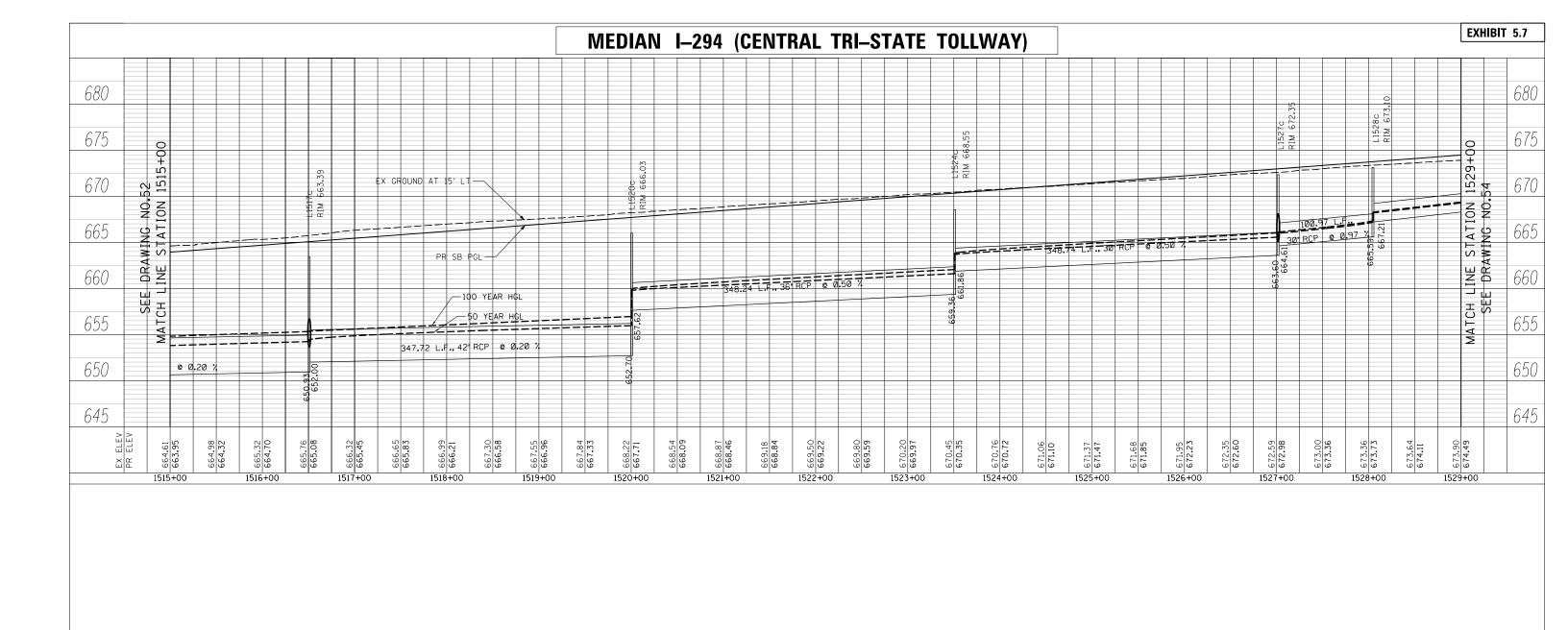


2700 OGDEN AVENUE DOWNERS GROVE, ILLINOIS 60515

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THE ILLINOIS STATE TOLL HIGHWAY AUTHORIT 2700 OGDEN AVENUE DOWNERS GROVE, ILLINOIS 60515

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CONTRACT NO. RR-14-4223	SHEET NO.
DRAINAGE PROFILE STA. 1515+00 - STA. 1529+00	DRAWING NO. 53A OF 56

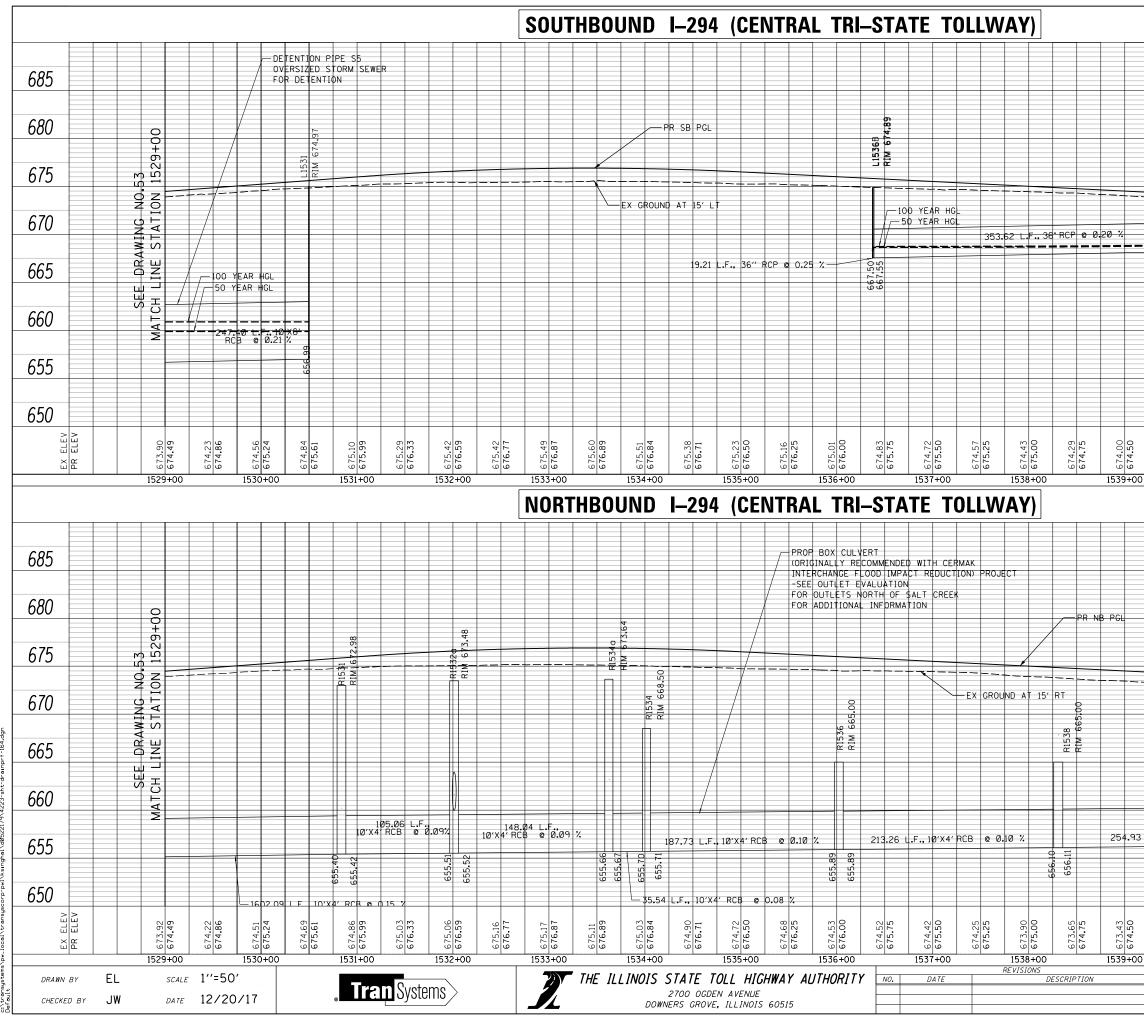
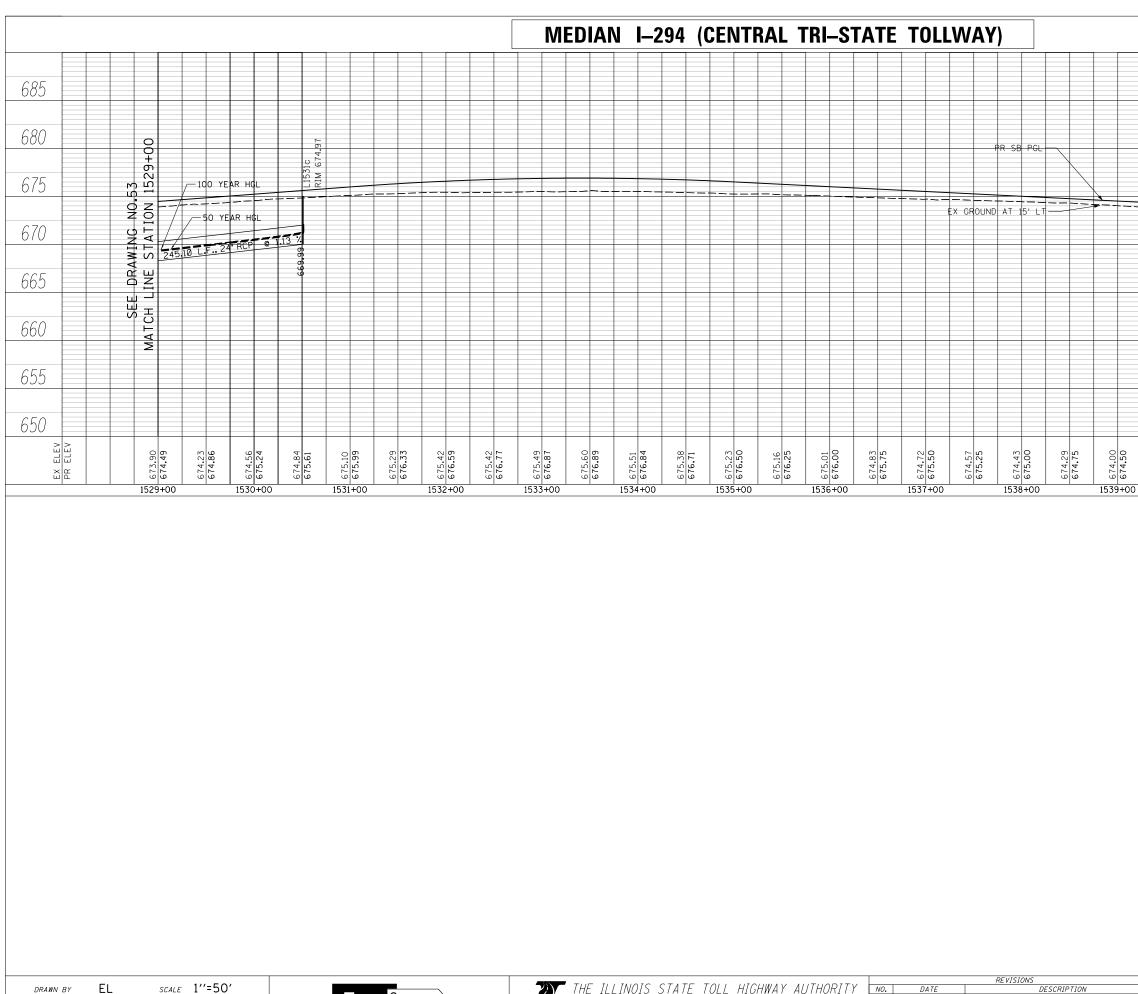


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CHECKED BY	JW	DATE	12/20/17

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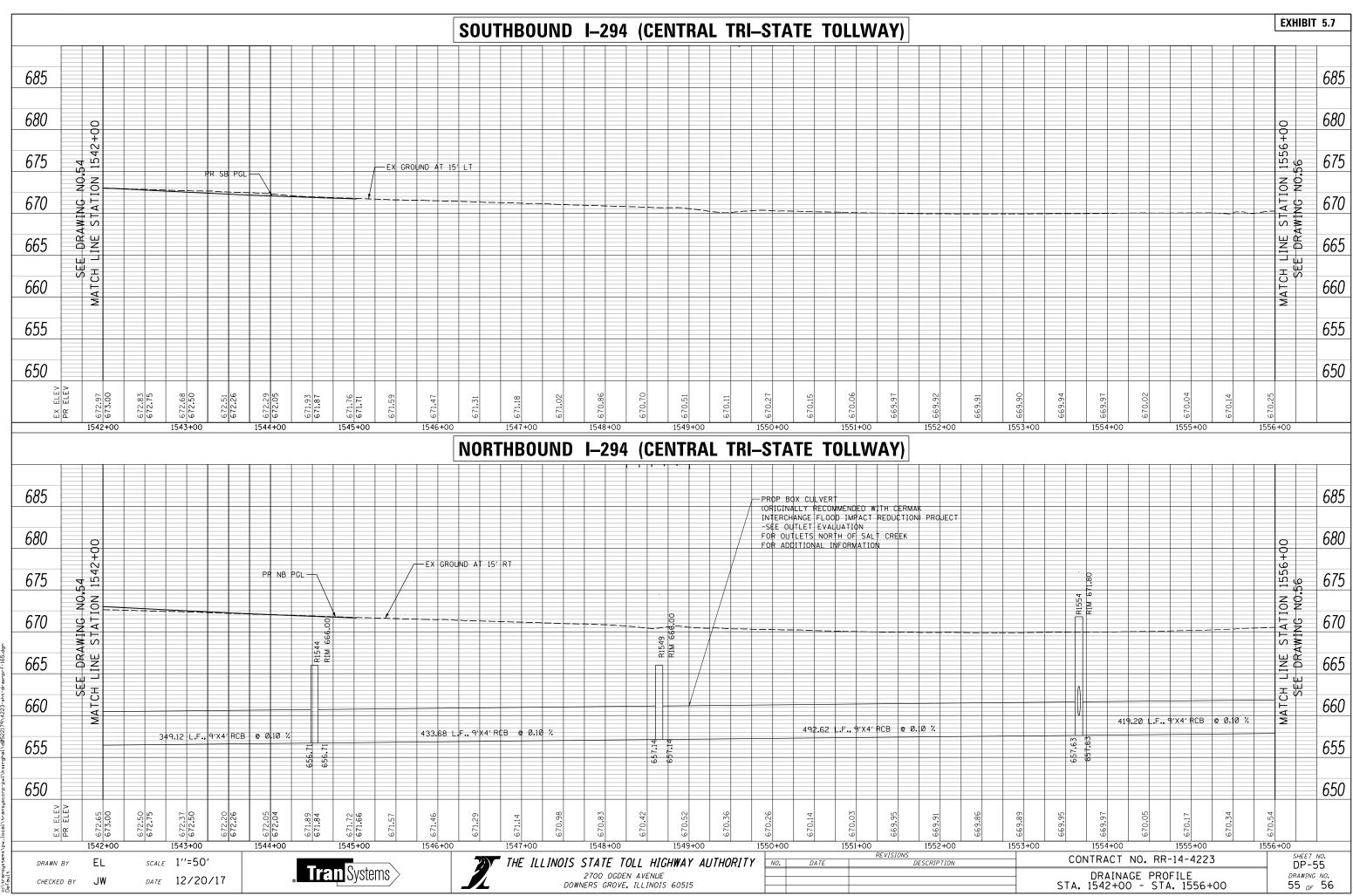


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CONTRACT NO. RR-14-4223	SHEET NO. DP-54A
DRAINAGE PROFILE STA. 1529+00 - STA. 1542+00	DRAWING NO. 54A _{OF} 56



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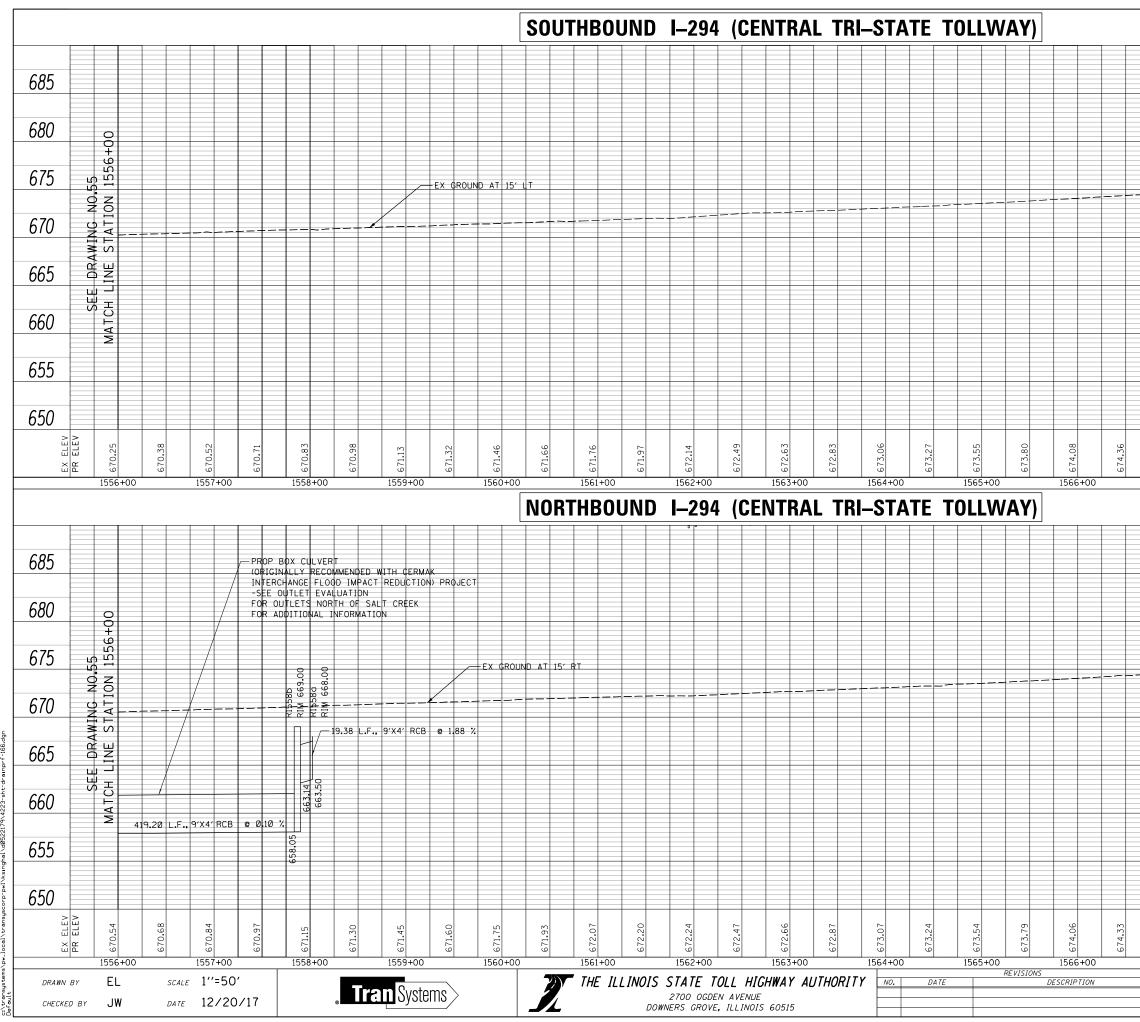
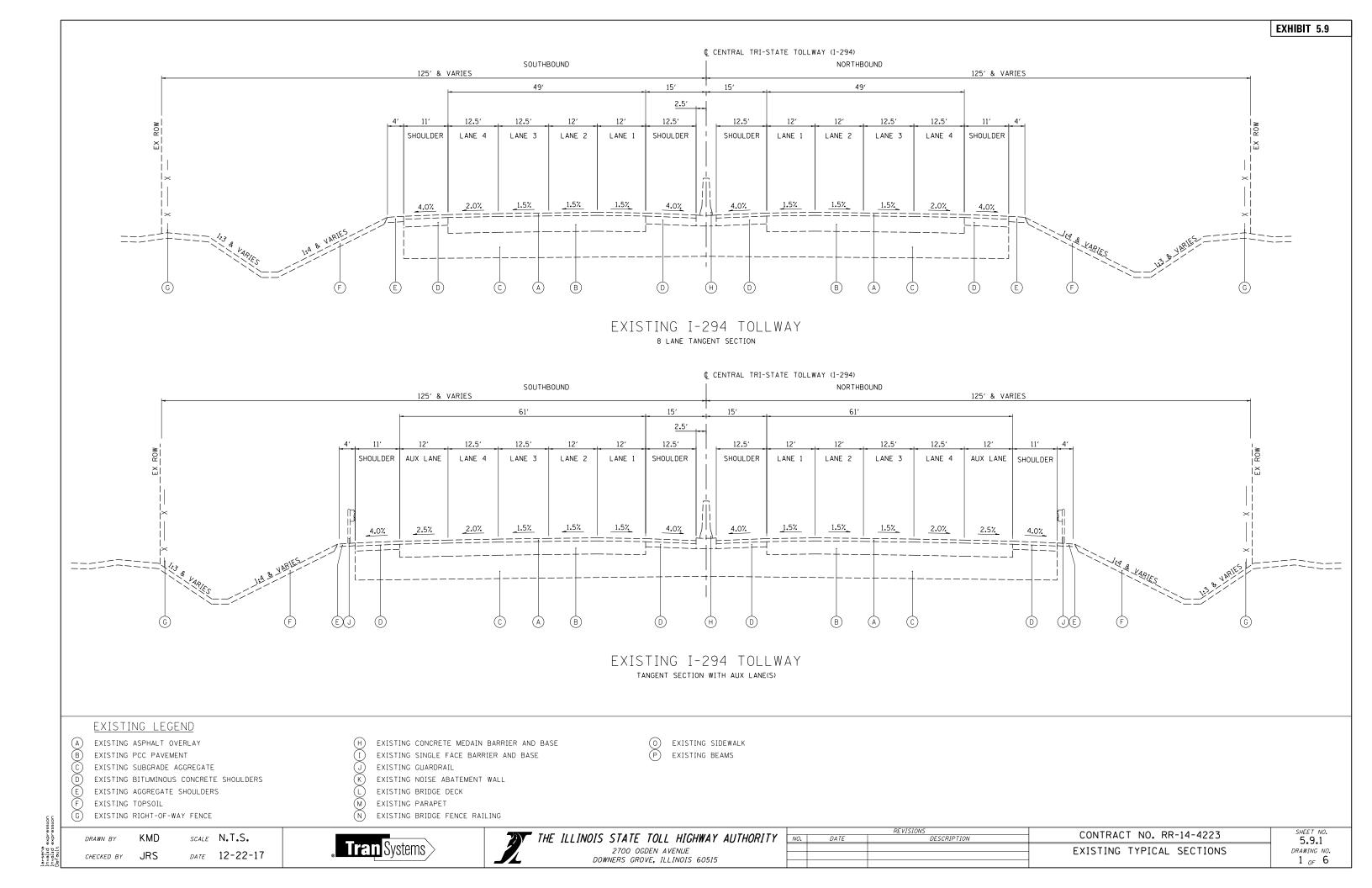
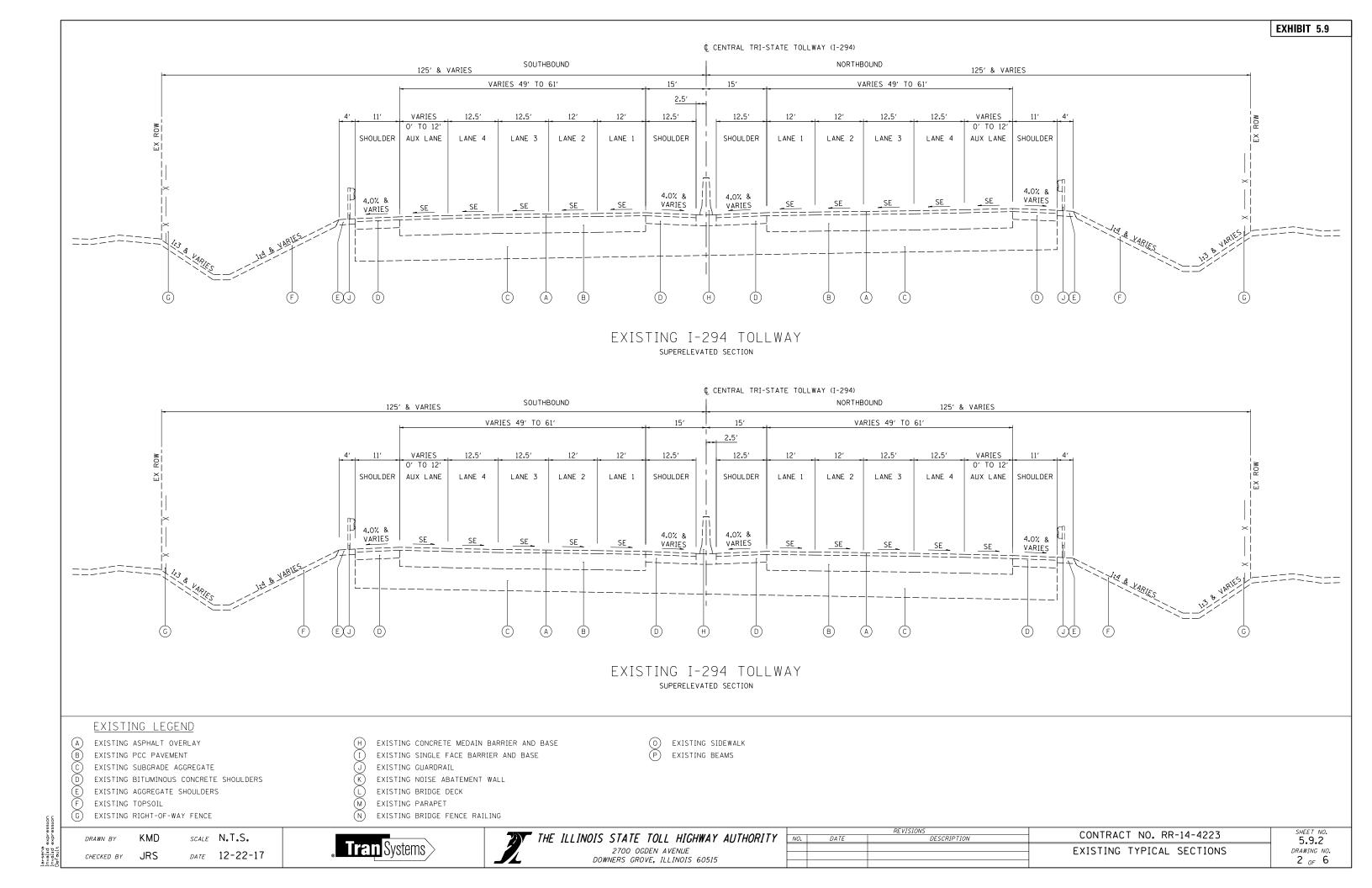


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## 5.9 EXISTING TYPICAL CROSS SECTIONS





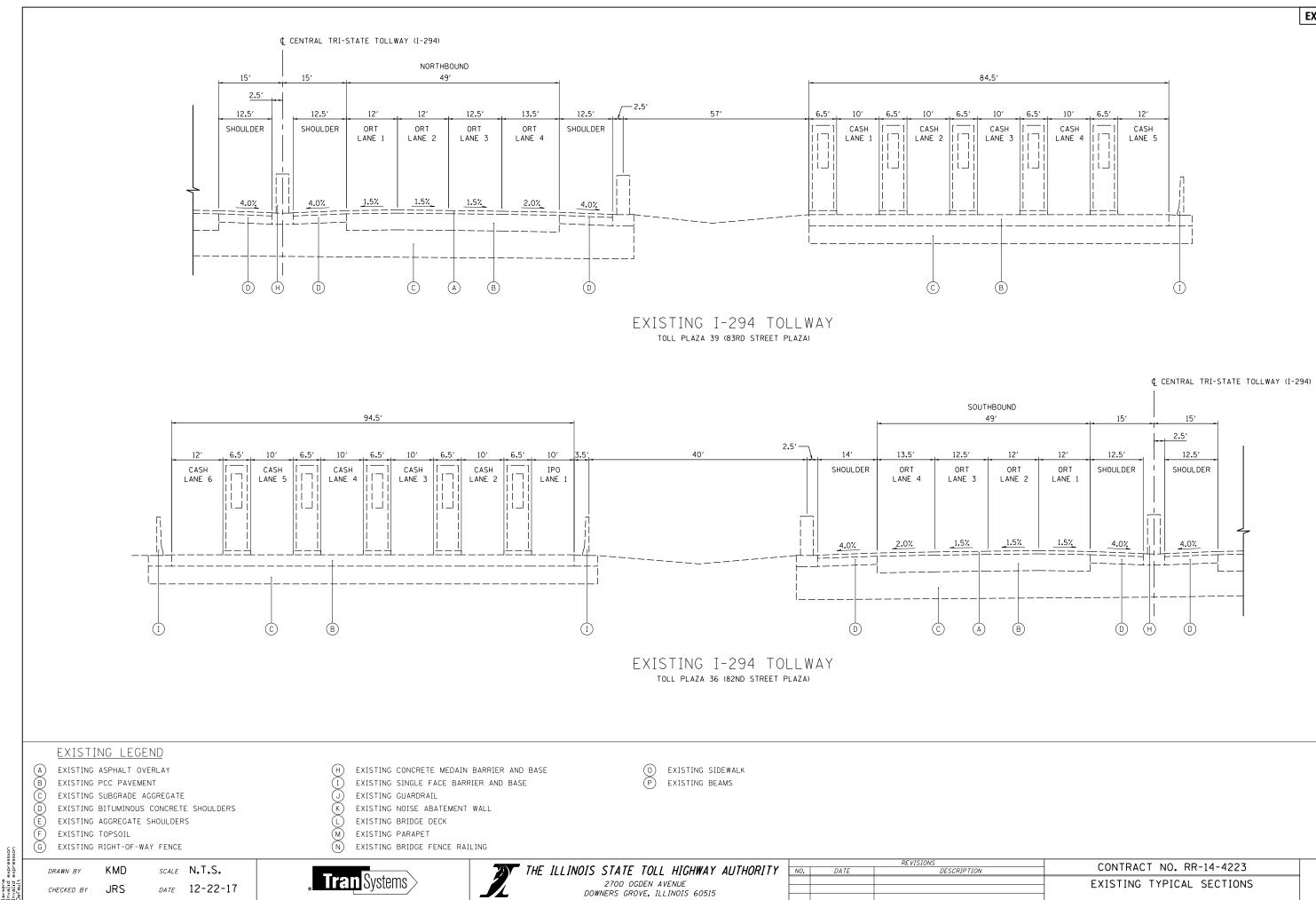
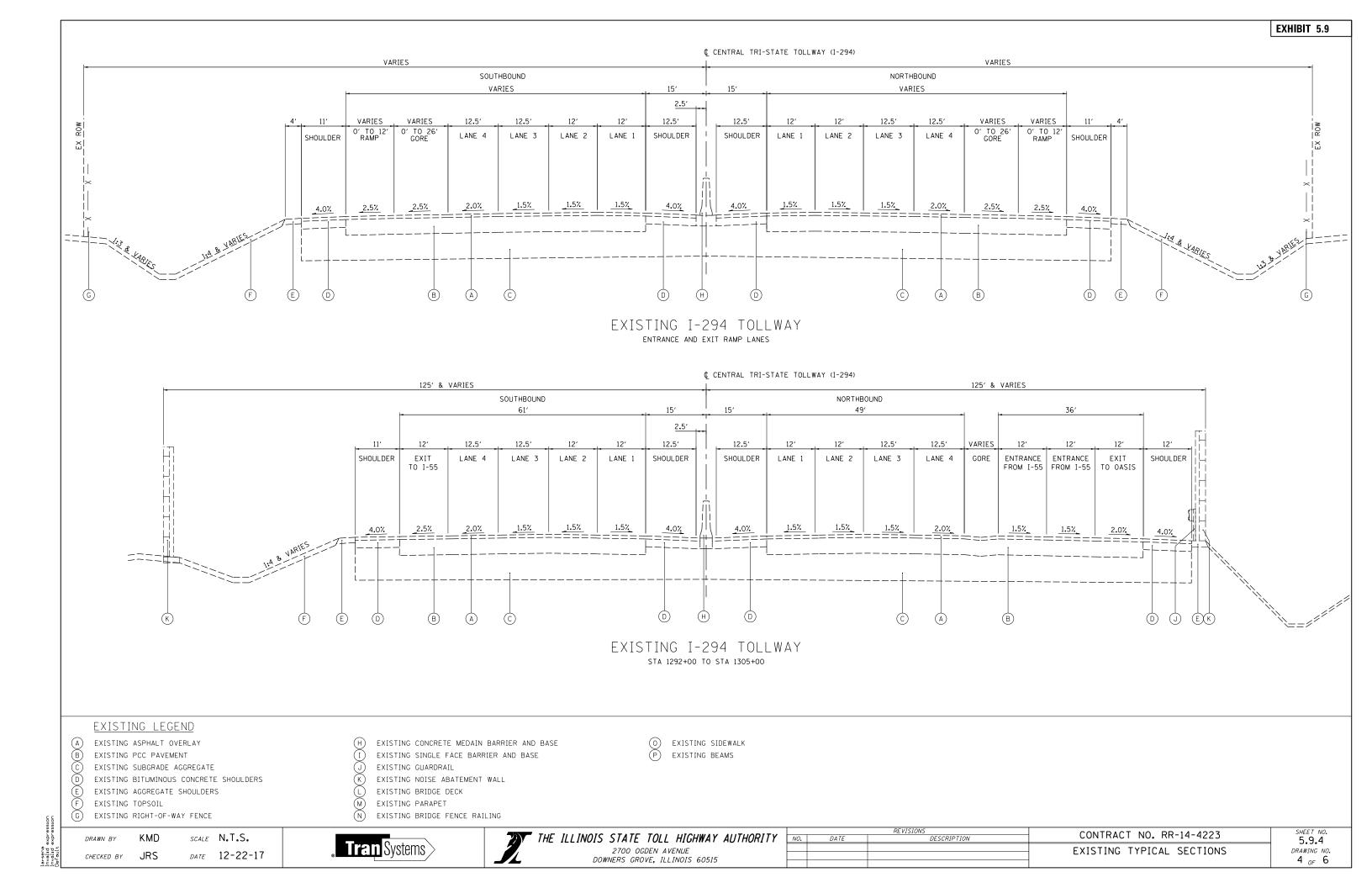
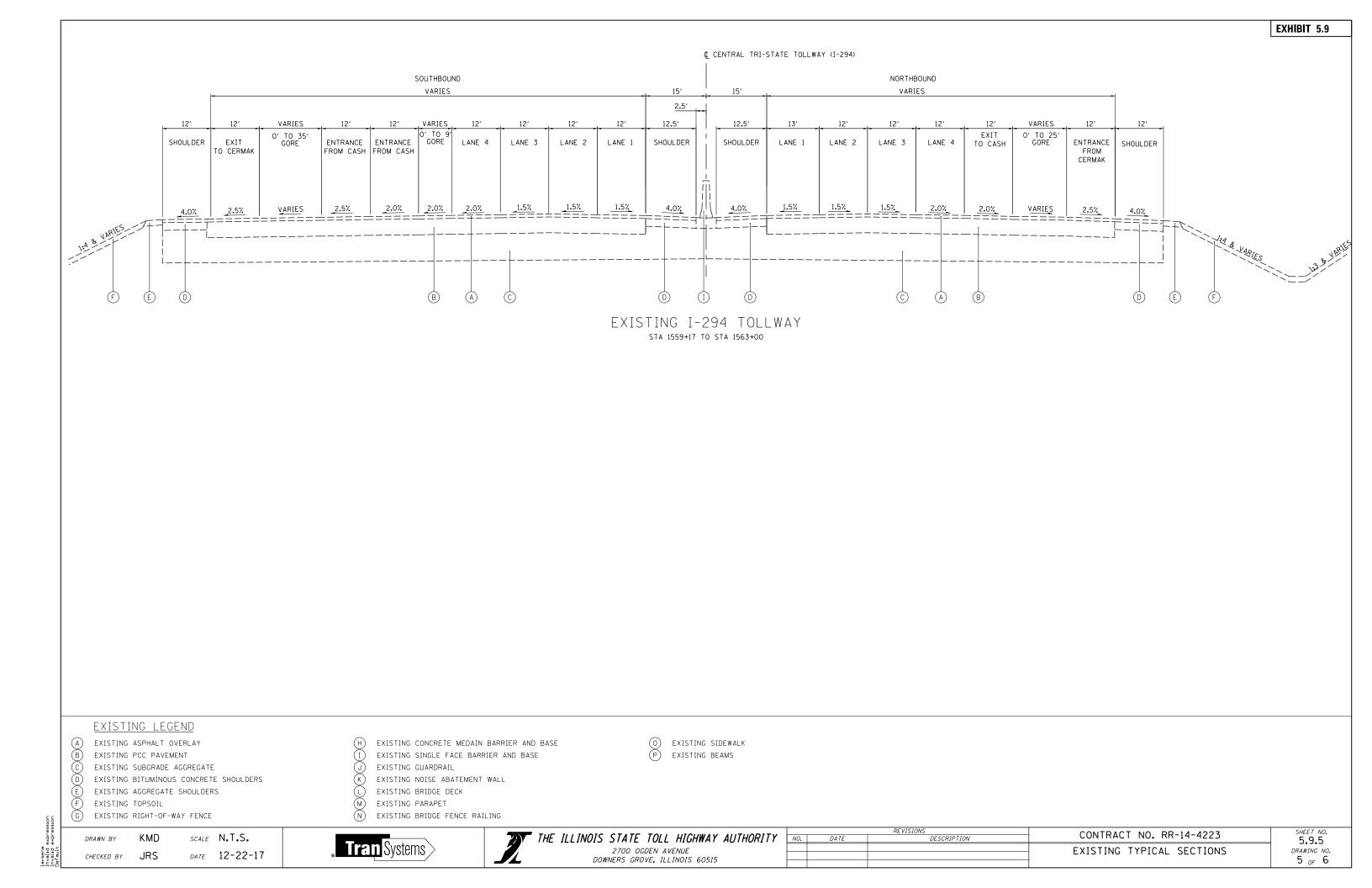
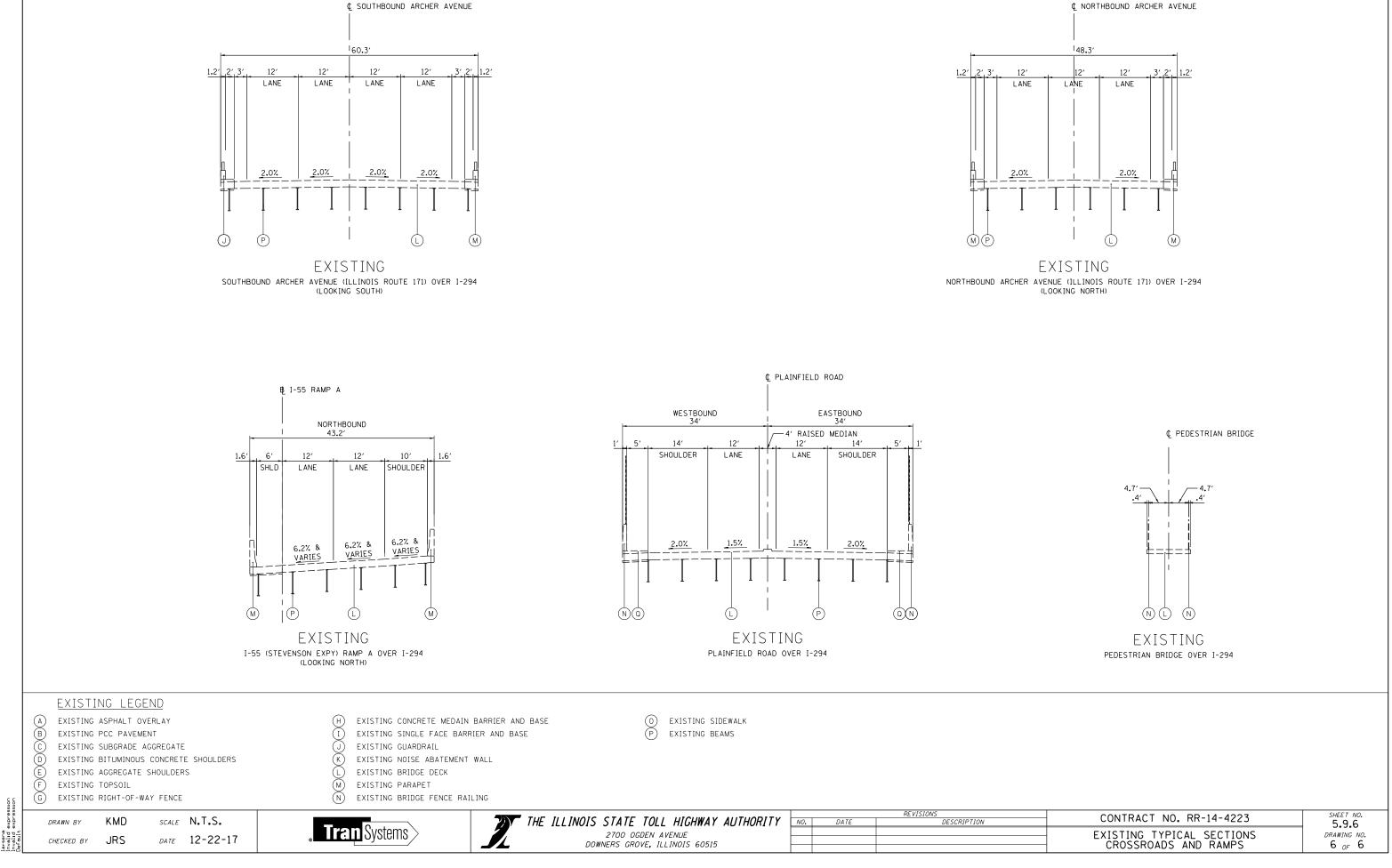


EXHIBIT 5.9

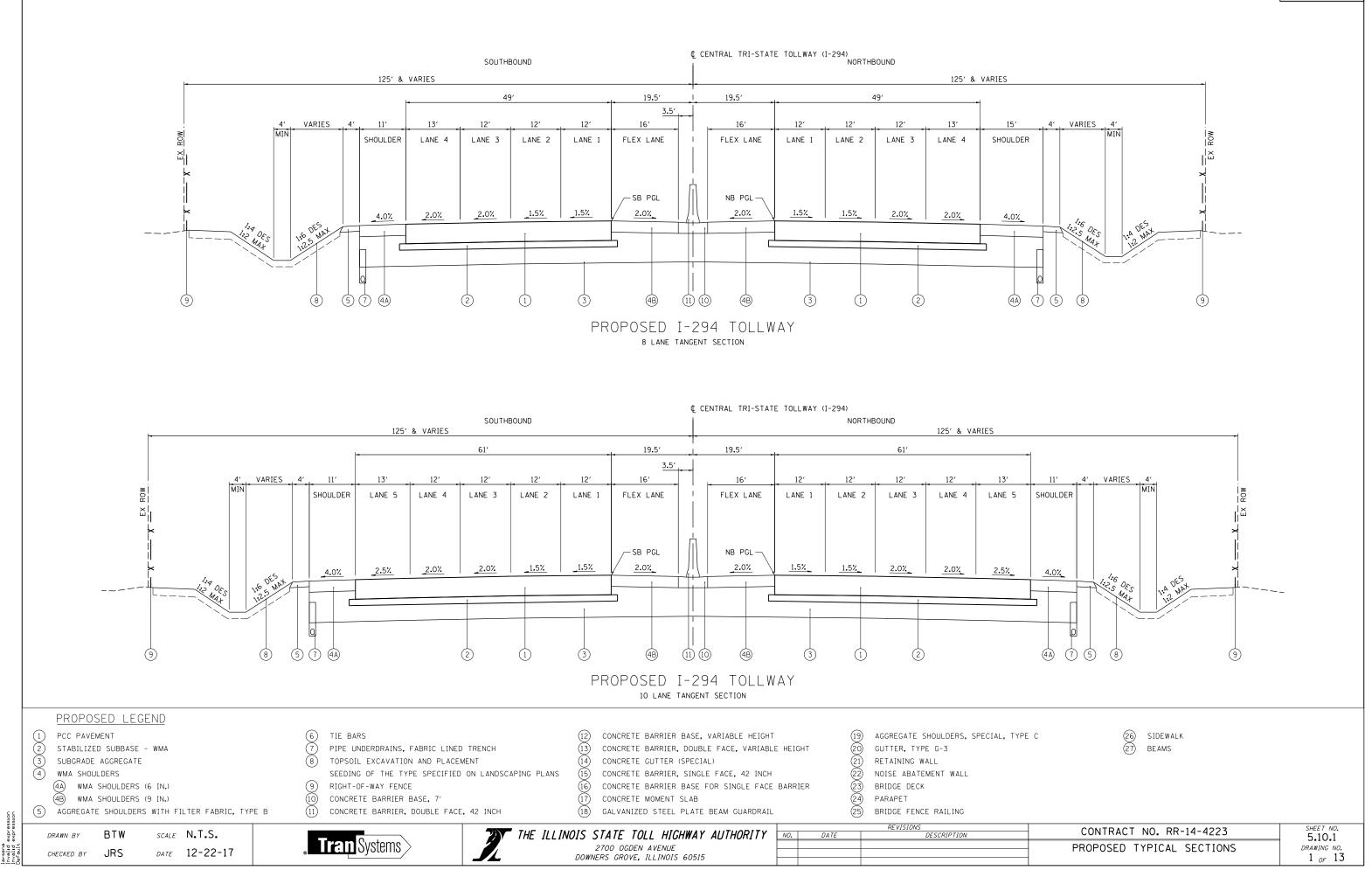
CONTRACT NO. RR-14-4223	SHEET NO.
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EXISTING TYPICAL SECTIONS	DRAWING NO.
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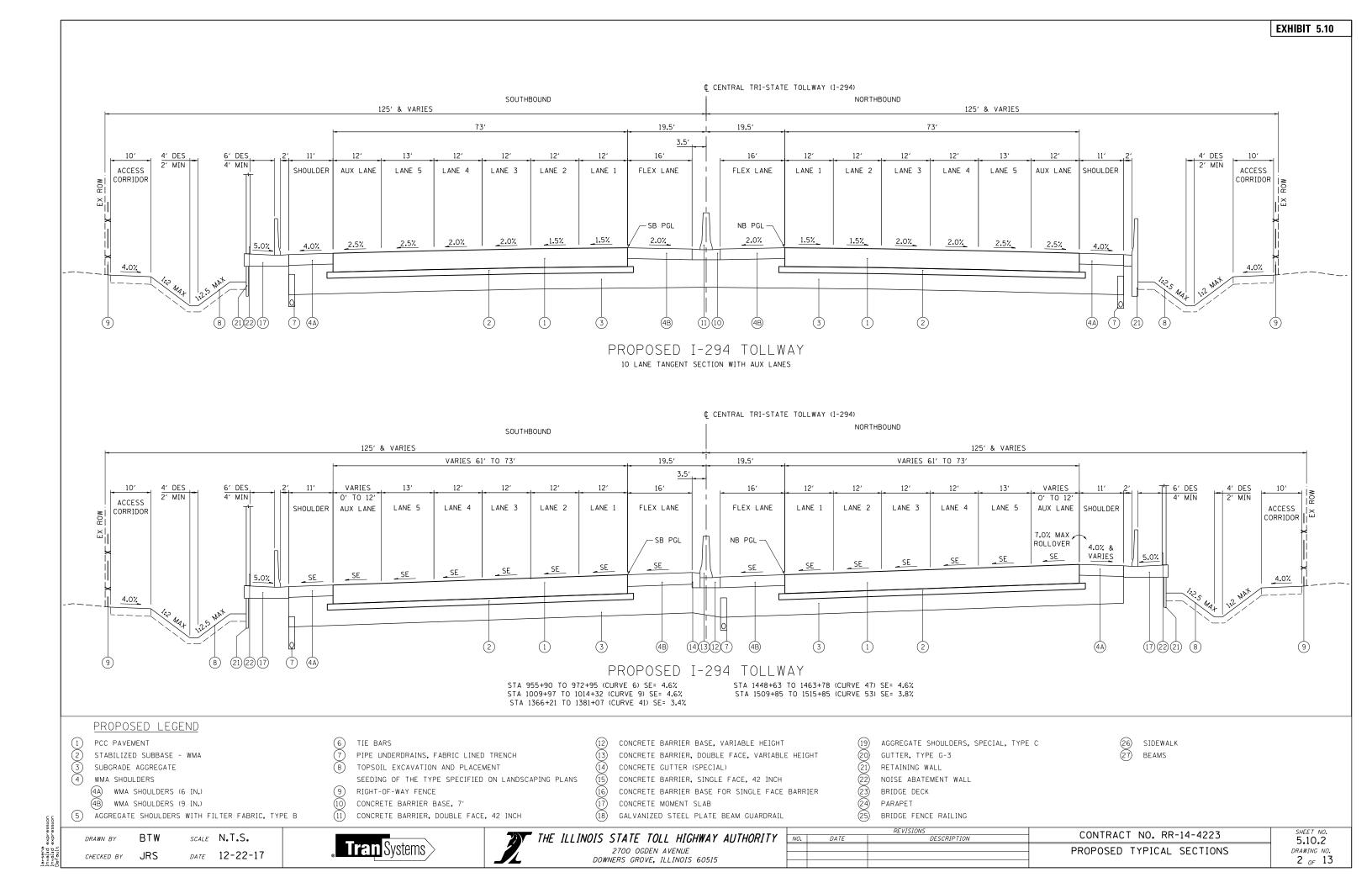


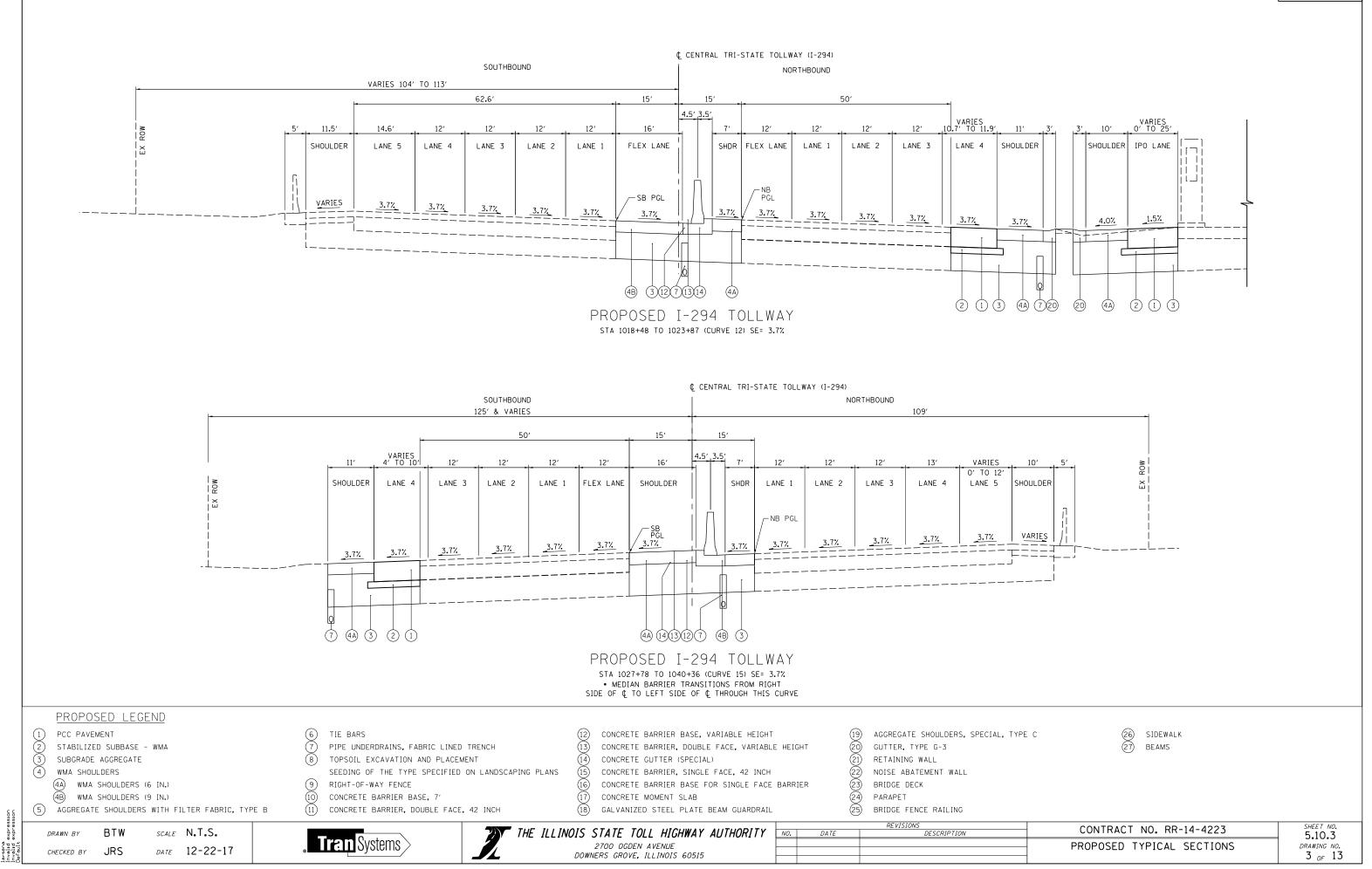


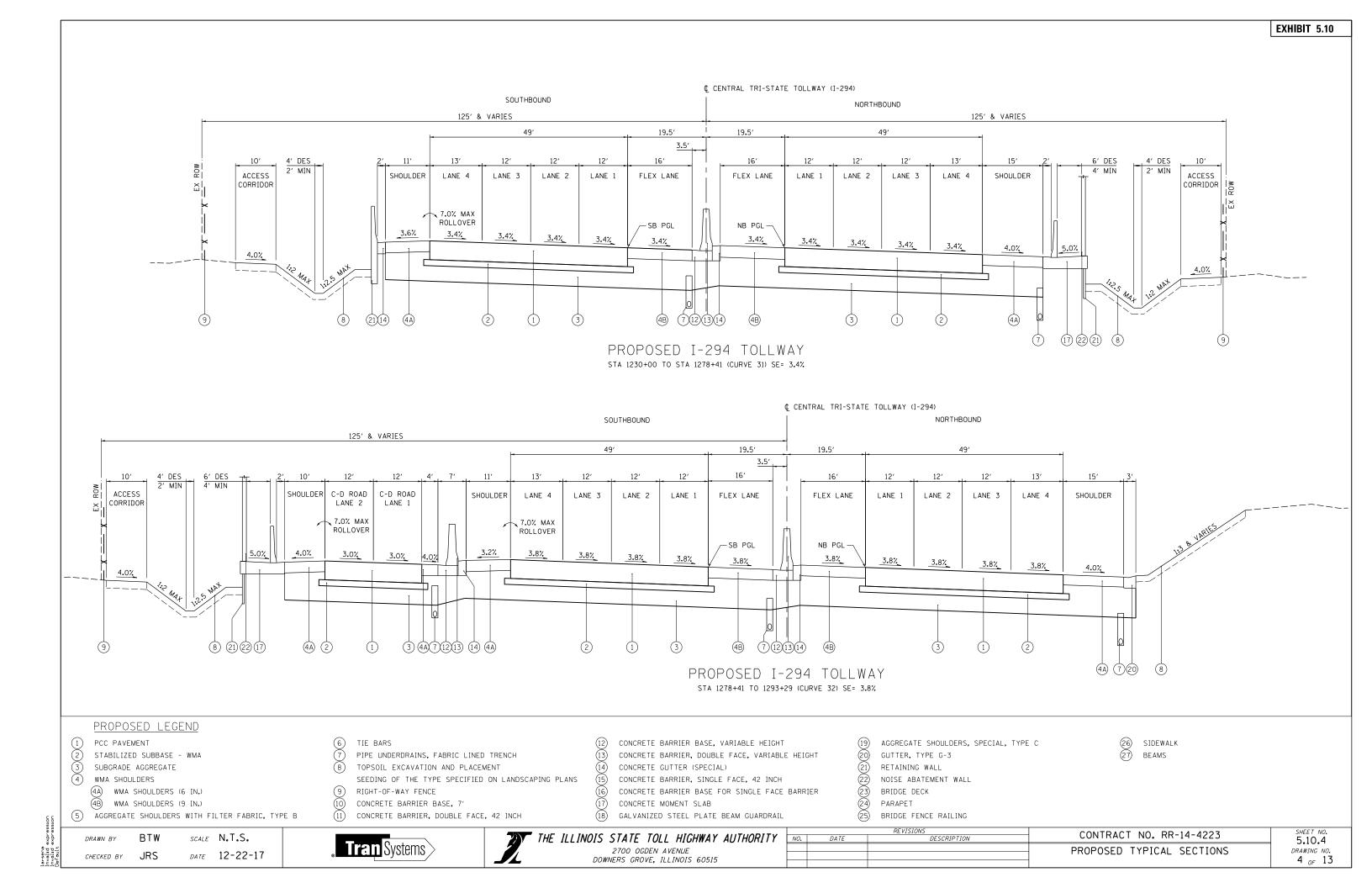
## 5.10 PROPOSED TYPICAL CROSS SECTIONS

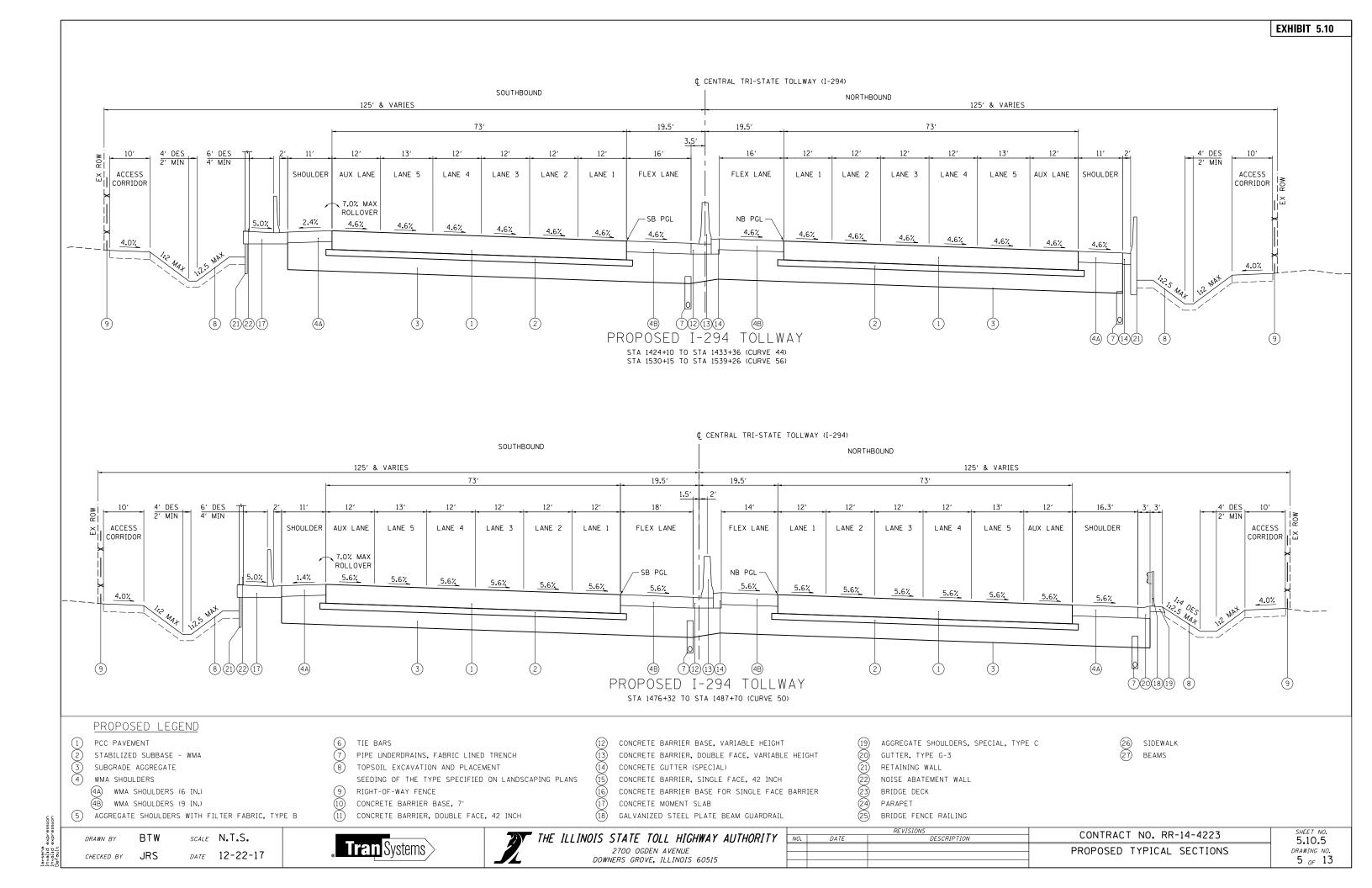


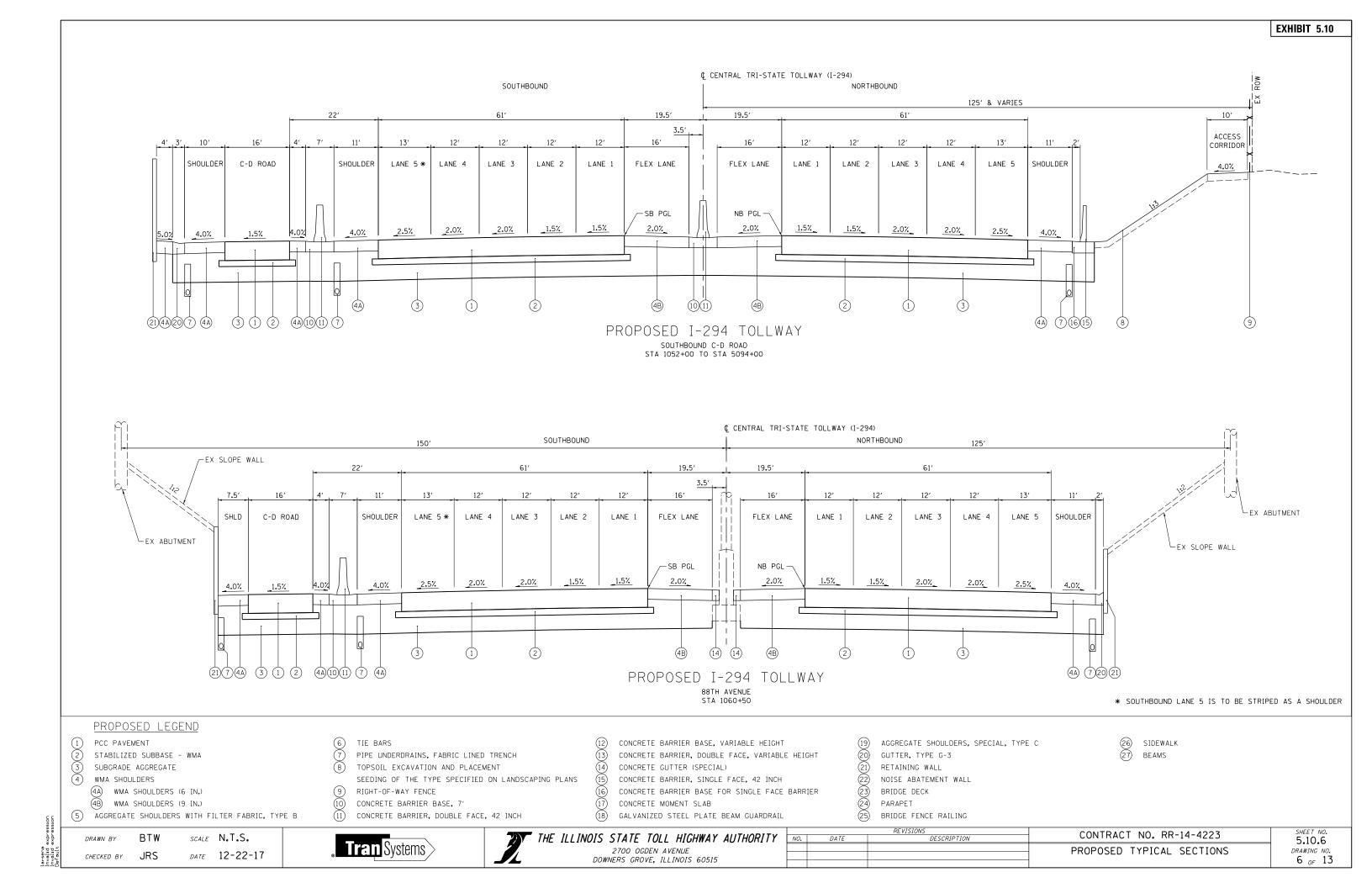


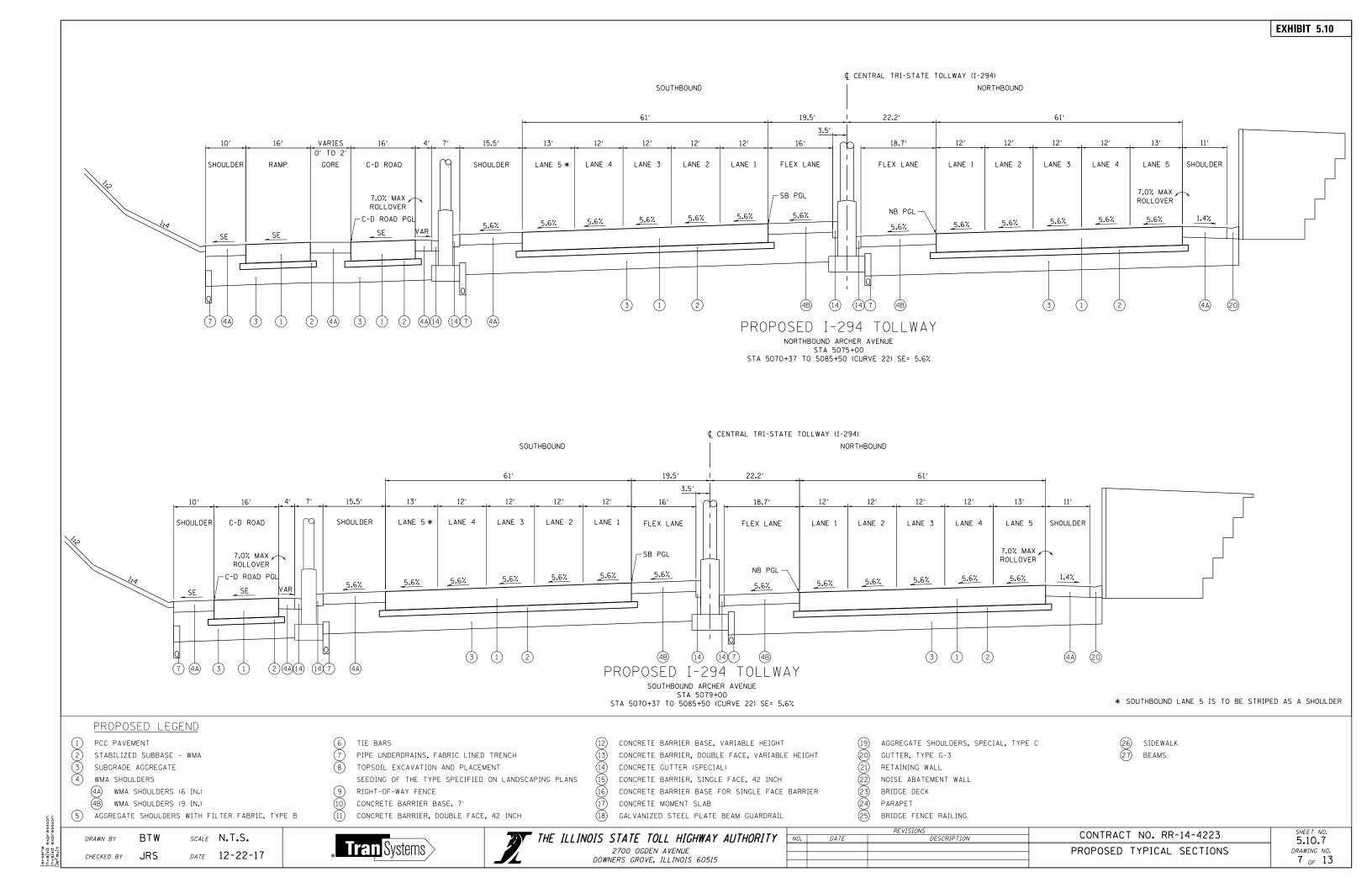


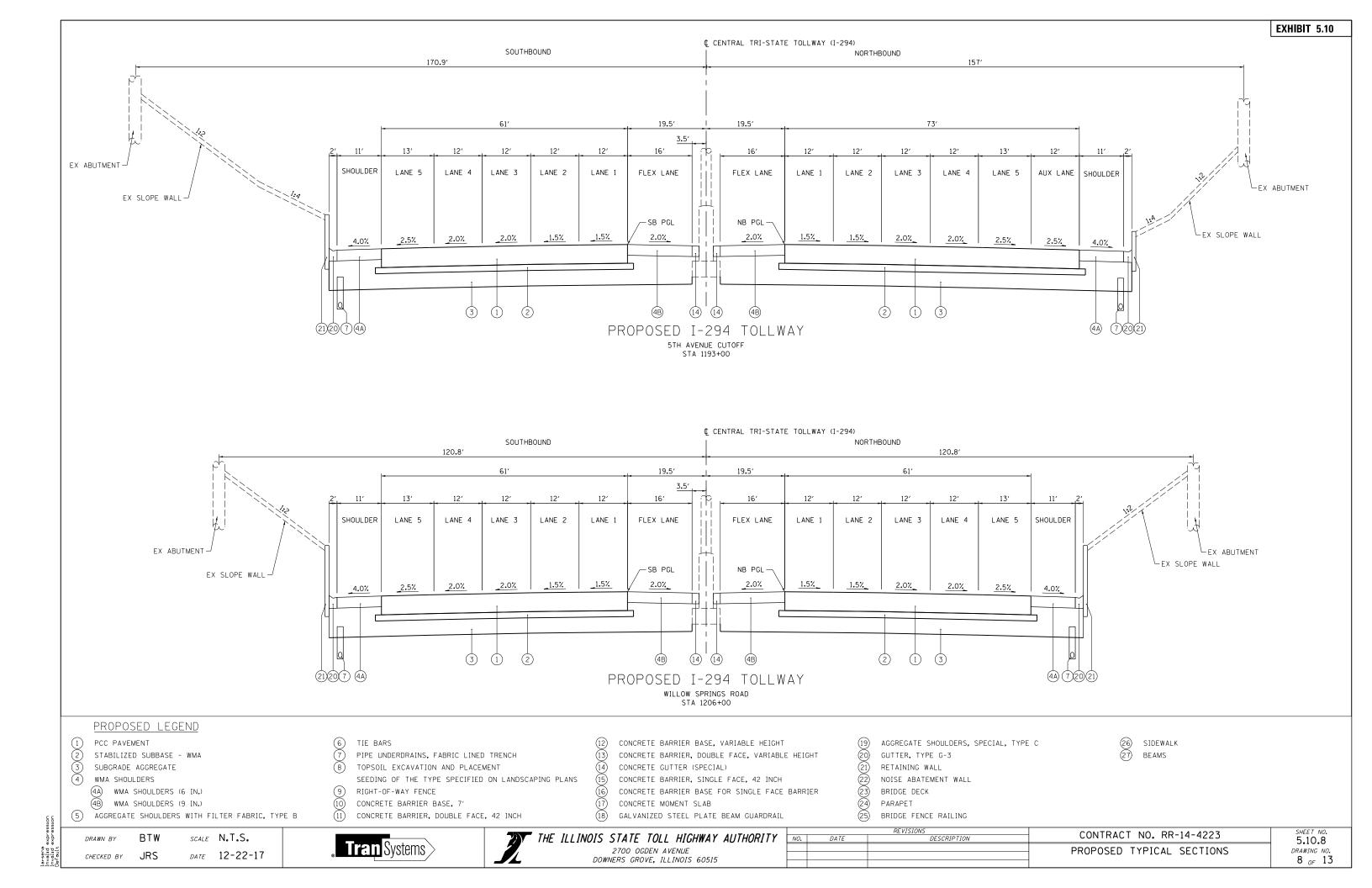












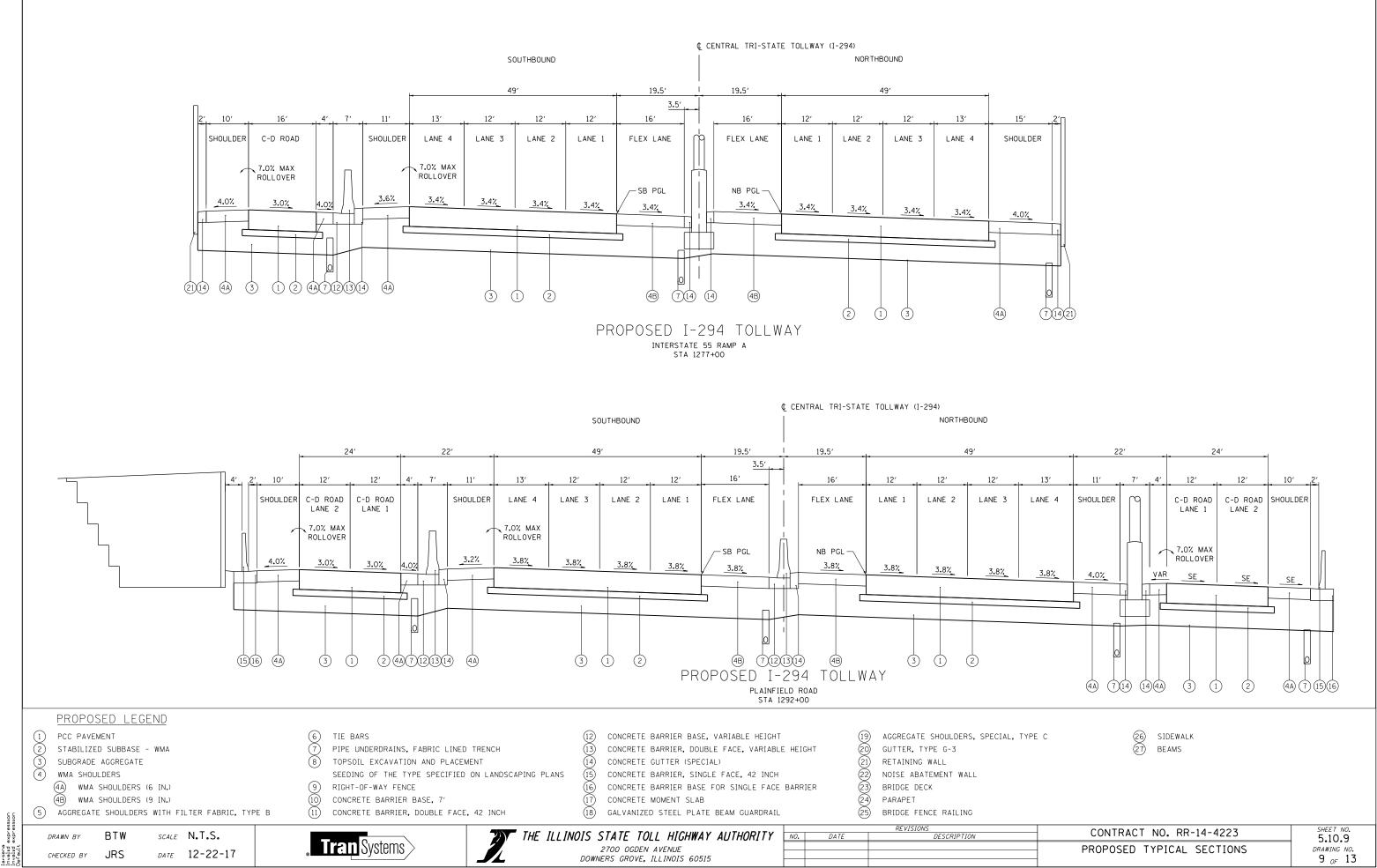
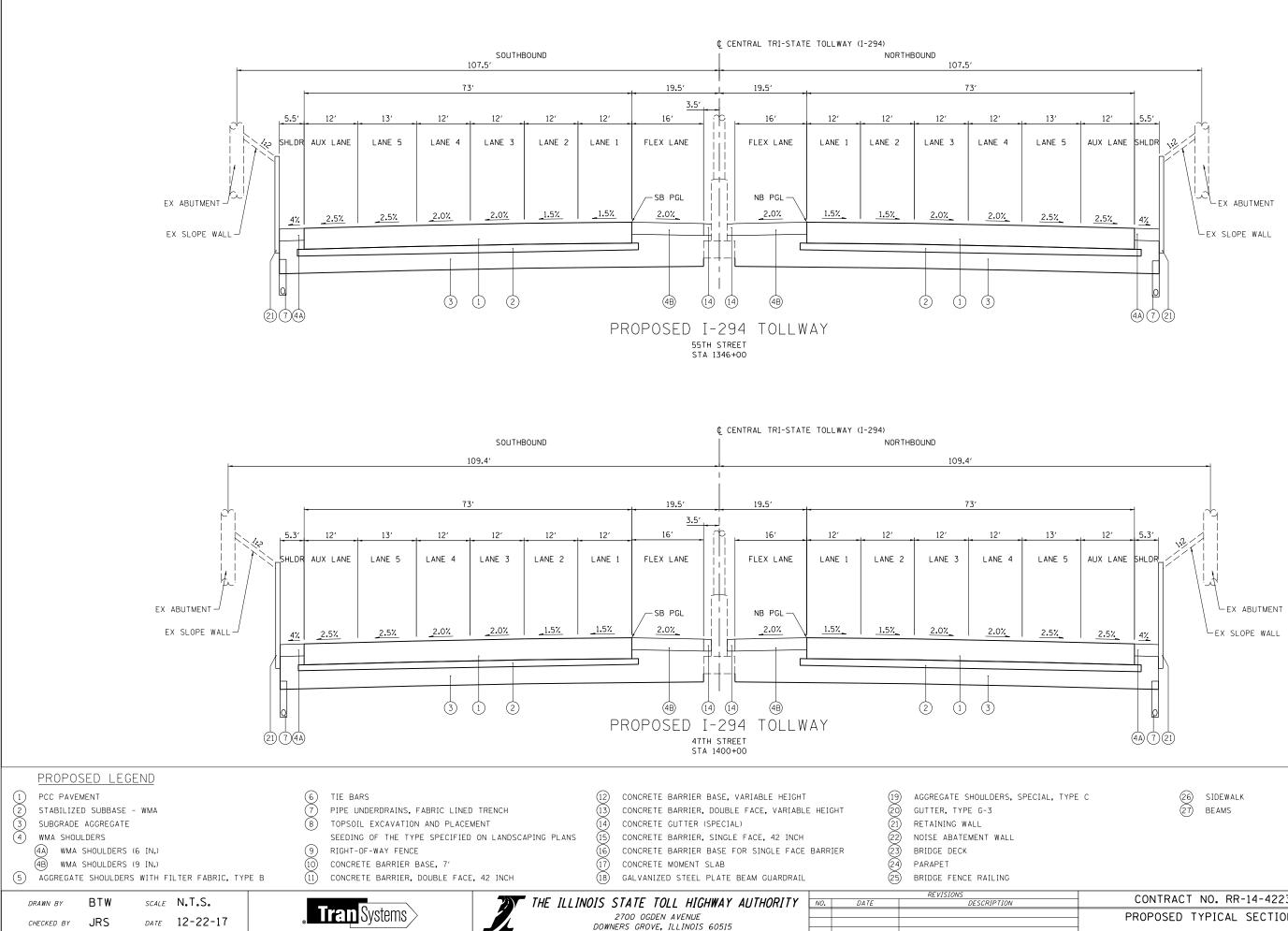


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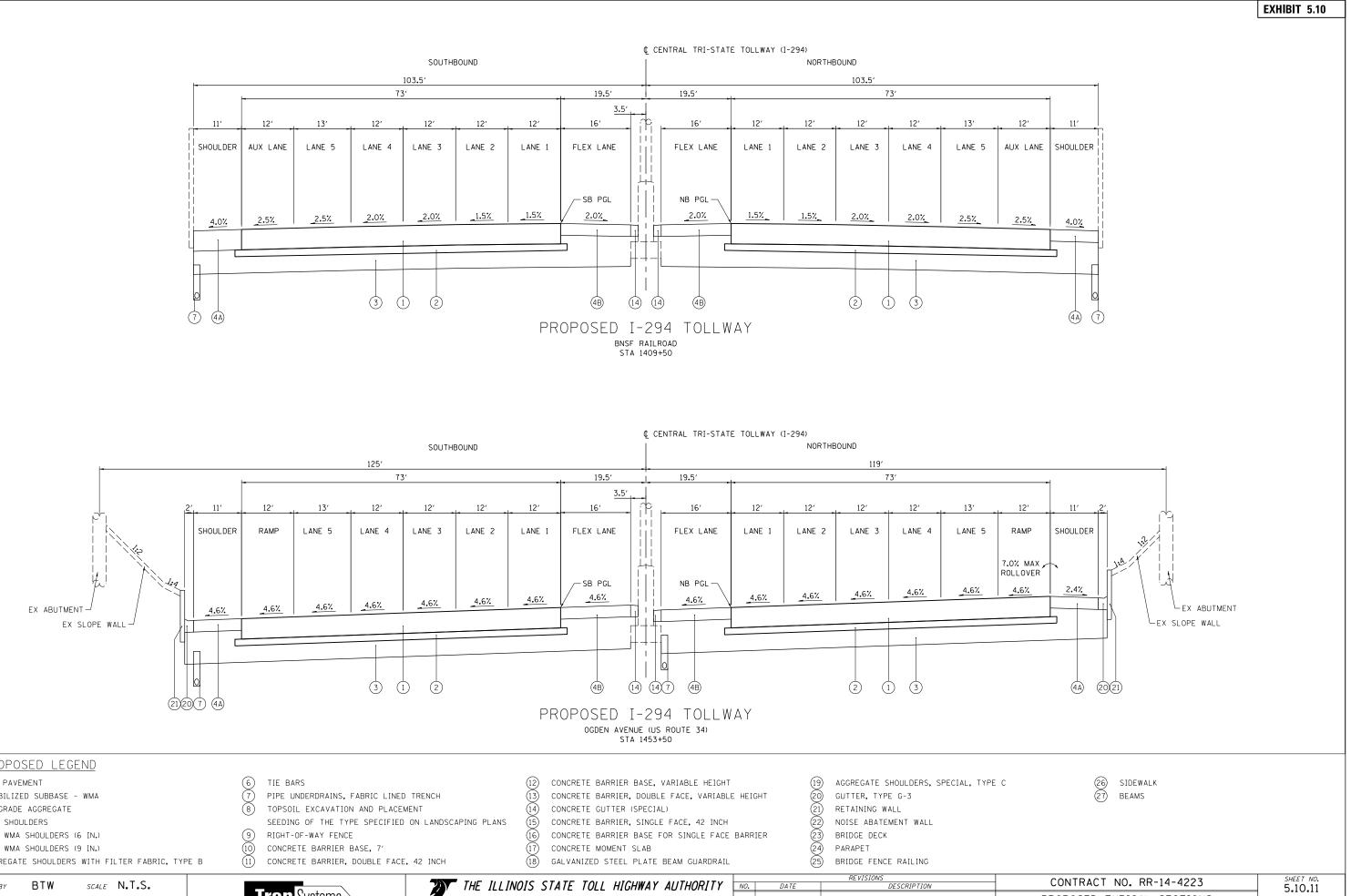


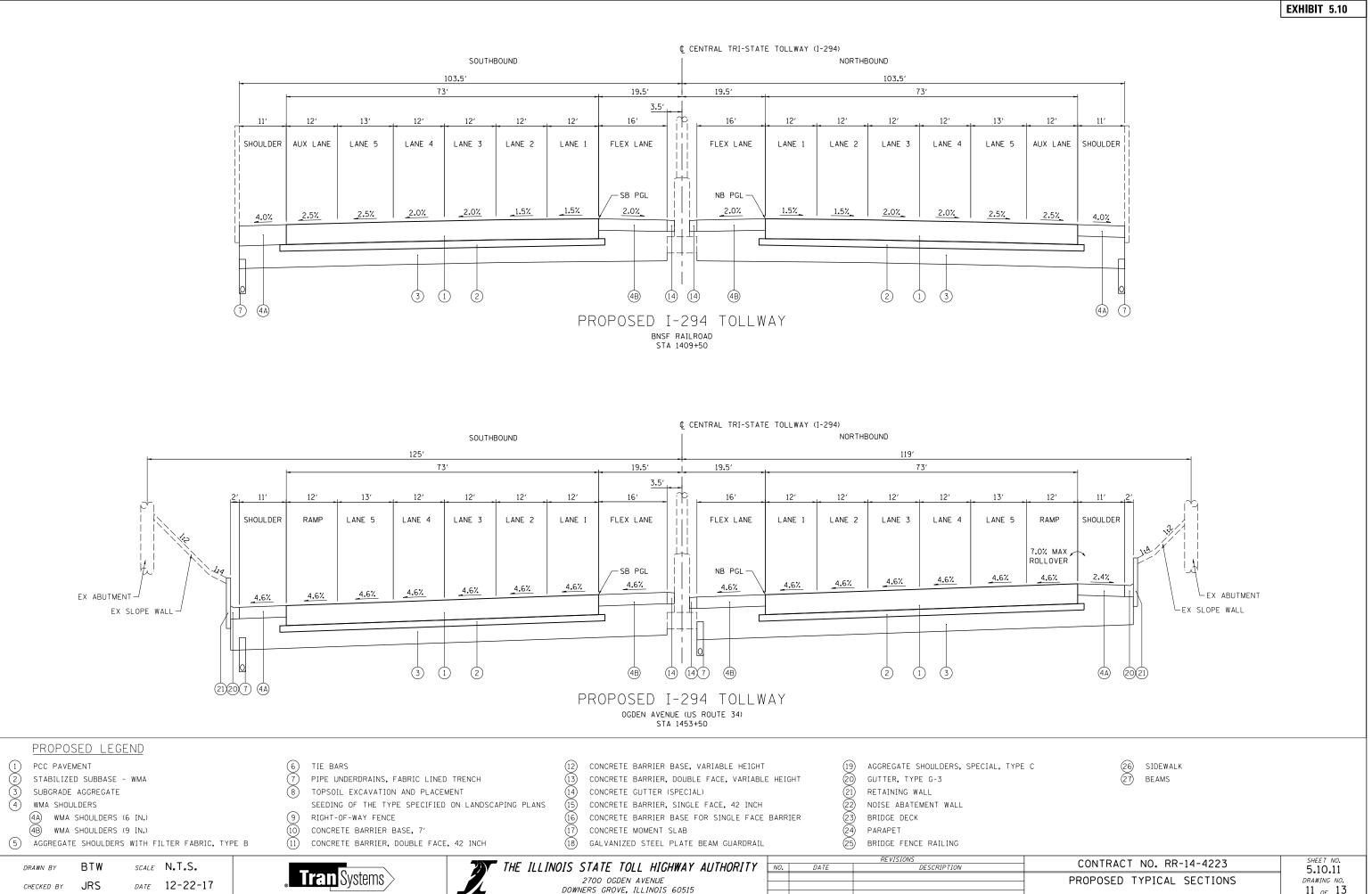
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EXHIBIT 5.10

CONTRACT NO. RR-14-4223	SHEET NO. 5.10.10
PROPOSED TYPICAL SECTIONS	DRAWING NO. 10 OF 13

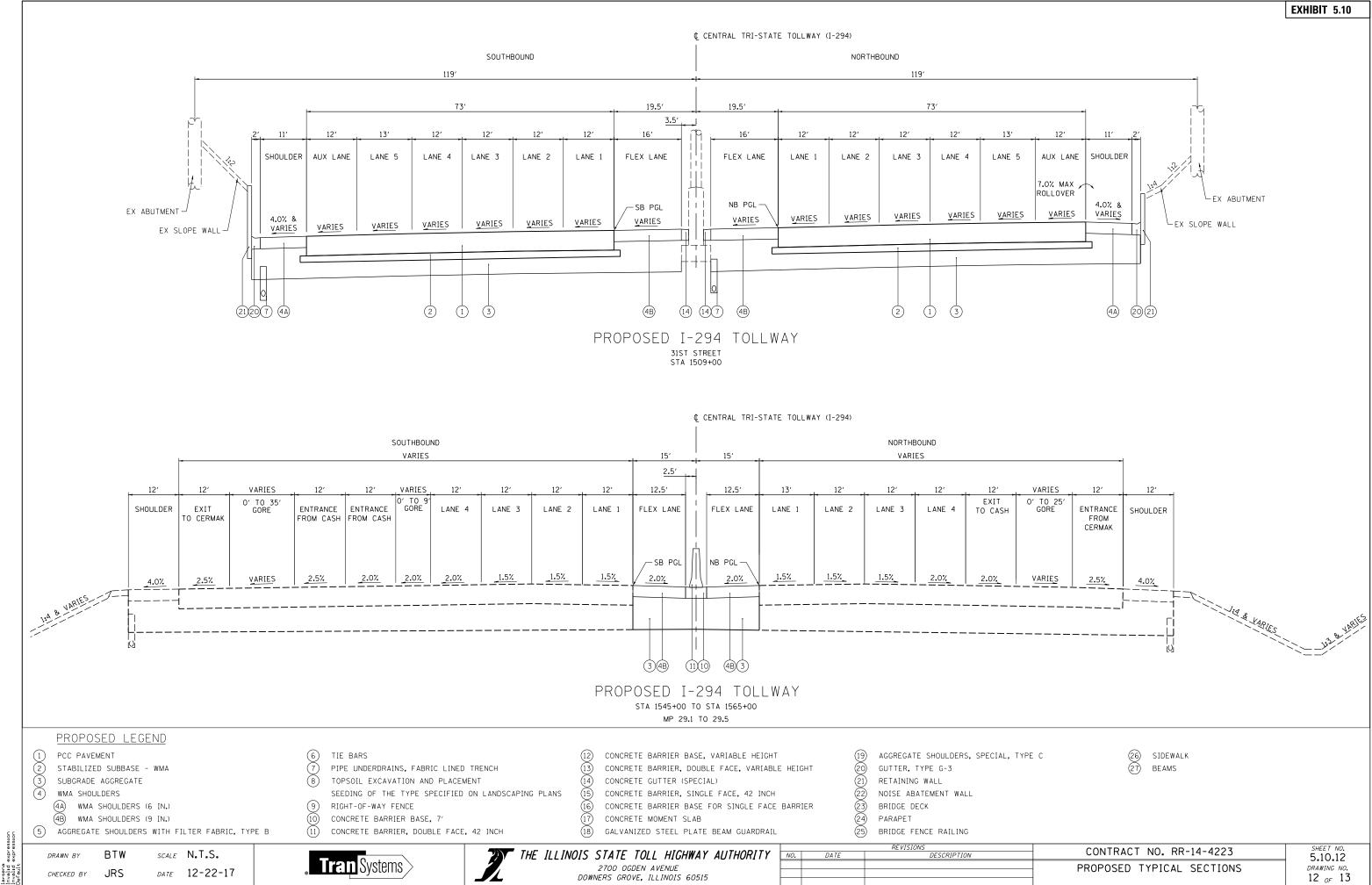




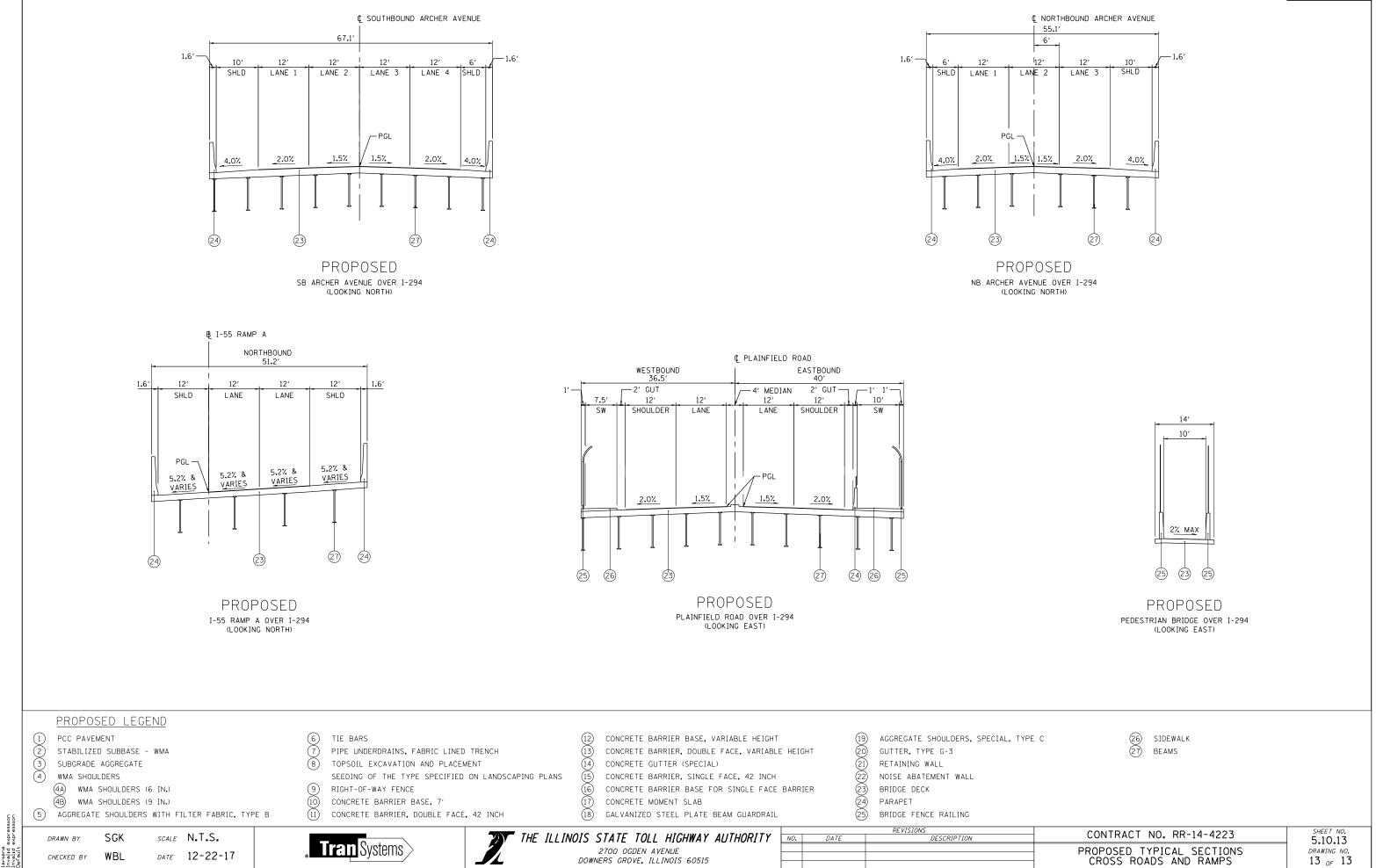
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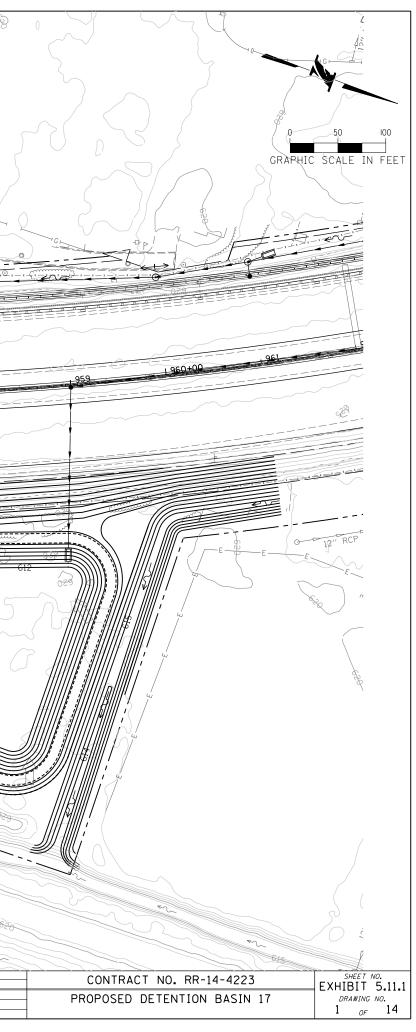


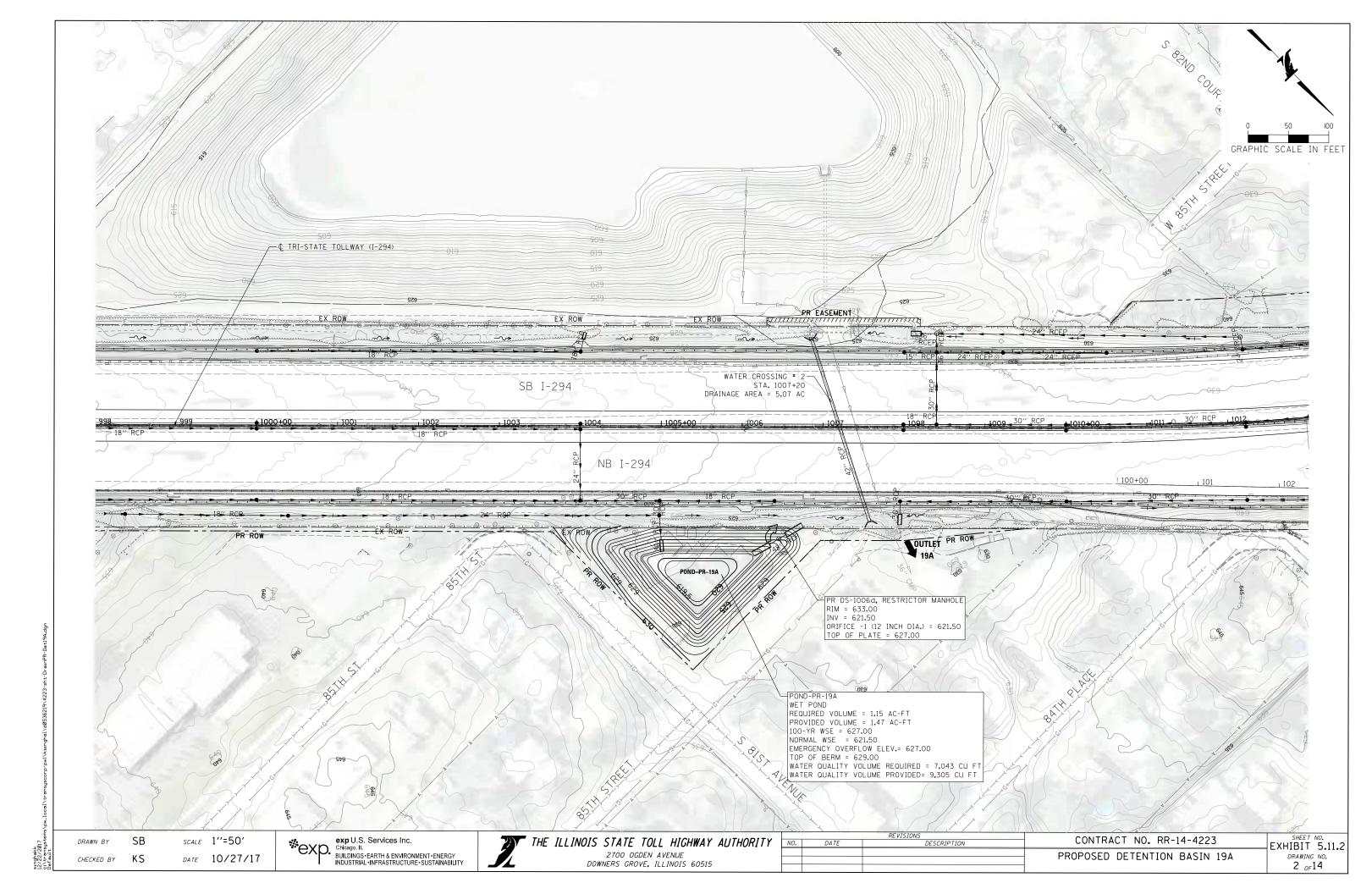
CONTRACT NO. RR-14-4223	SHEET NO. 5.10.13
PROPOSED TYPICAL SECTIONS CROSS ROADS AND RAMPS	drawing no. 13 _{of} 13

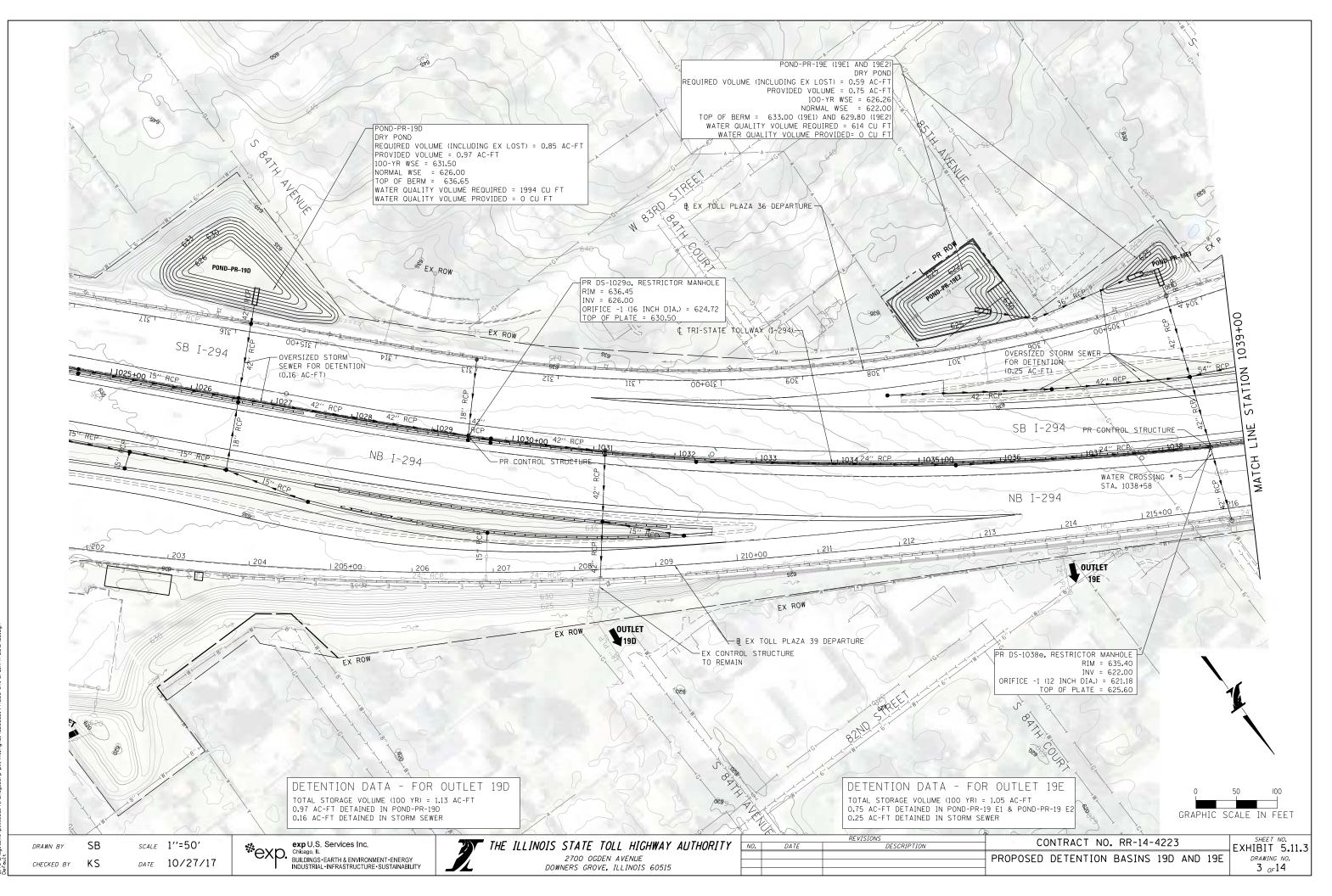
EXHIBIT 5.10

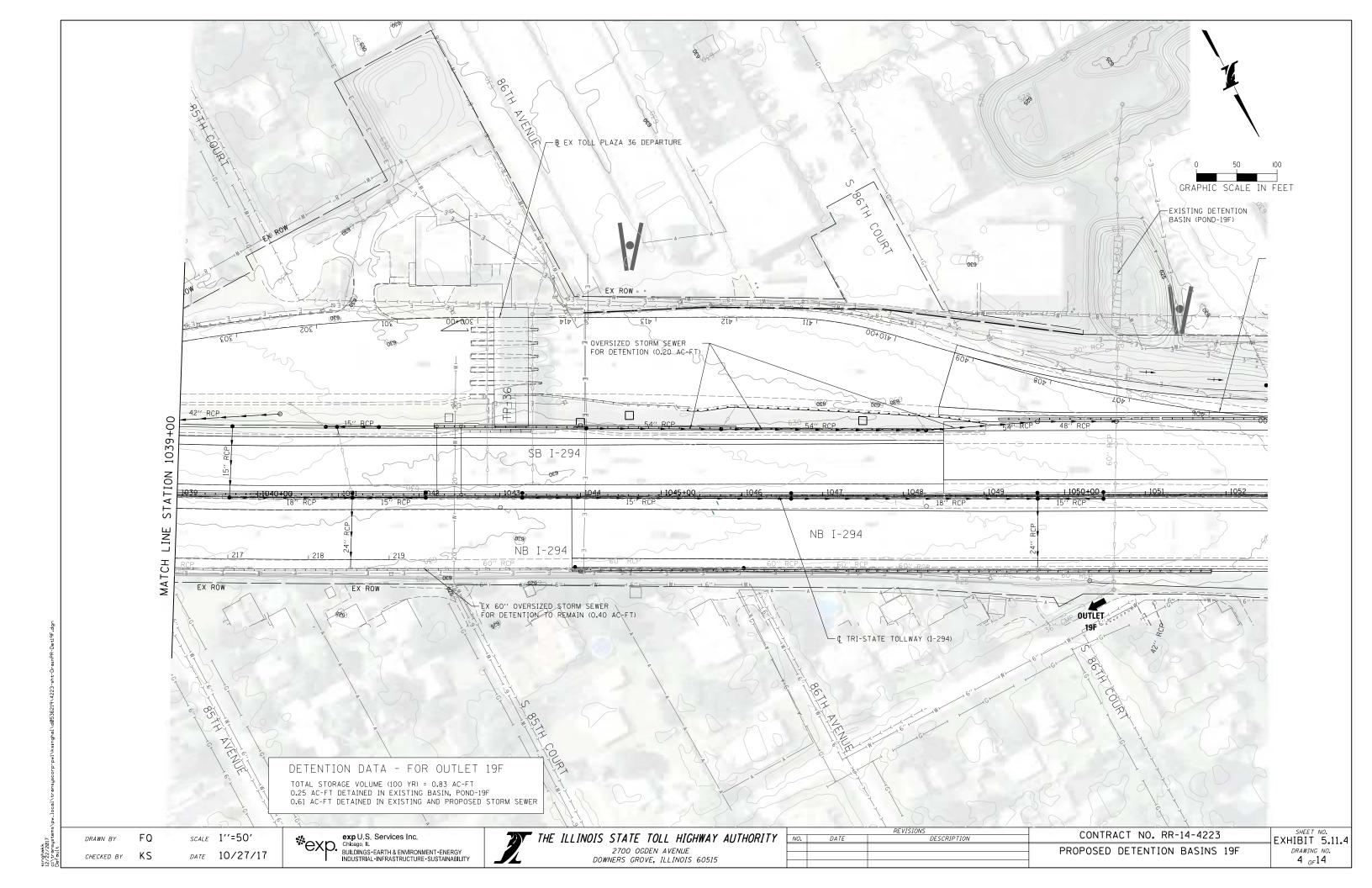
## 5.11 CONCEPTUAL DETENTION BASIN LAYOUTS

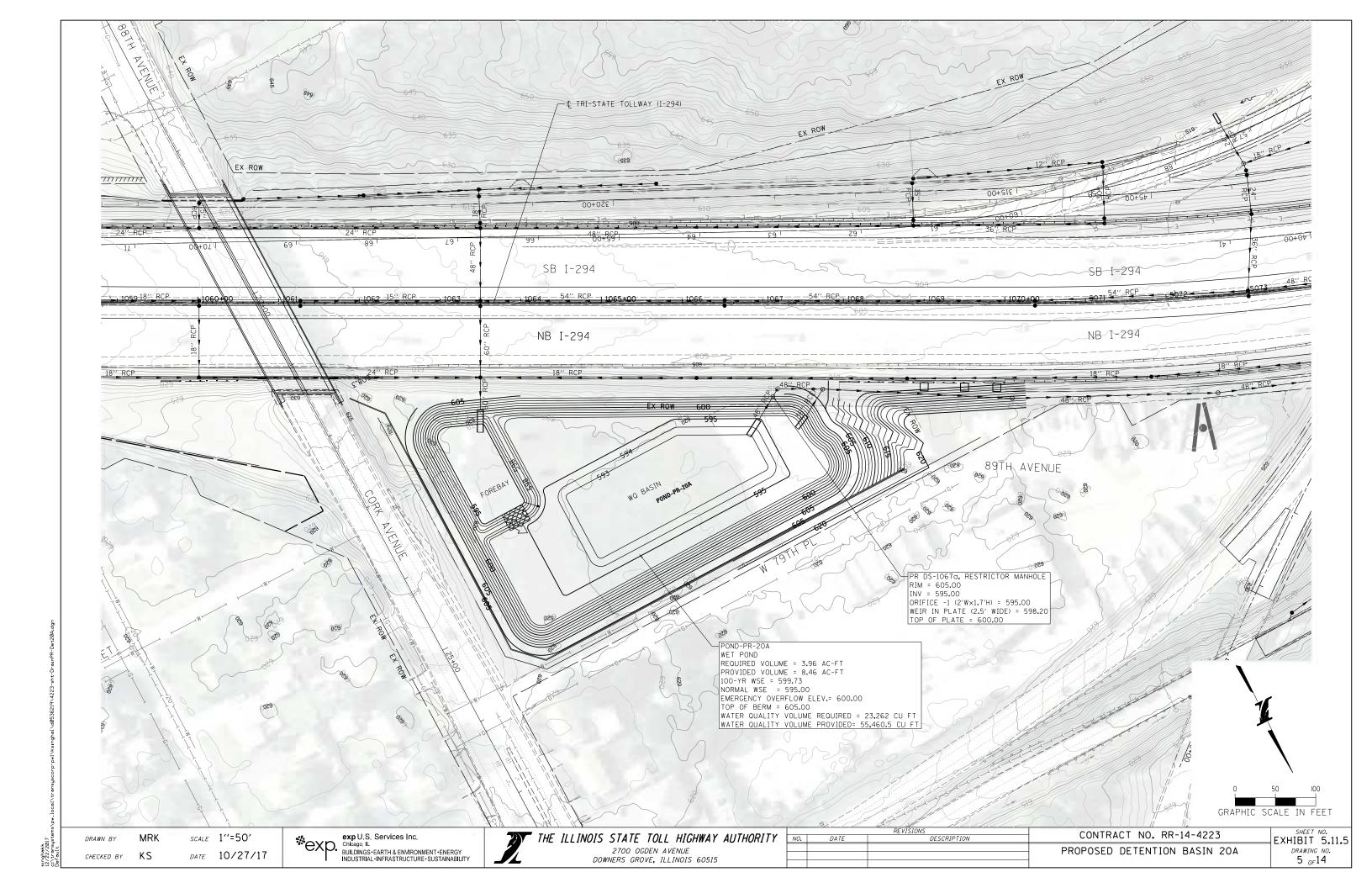
STREET 7TH AVENUE 91S7 È EX ROW-€_TRI-STATE TOLLWAY (I-294) SB I-294 953 948 1 950+0 955+0 NB I-294 48 _____ . . FYR POND-PR-17 PR DS-9511, RESTRICTOR MANHOLE RIM = 619.00 INV = 613.00 ORIFICE -1 (4 INCH DIA.) = 613.00 TOP OF PLATE = 616.00 POND-PR-17 WET POND REQUIRED VOLUME = 1.81 AC-FT PROVIDED VOLUME = 5.33 AC-FT 100-YR WSE = 616.00 NORMAL WSE = 613.00 NORMAL WSE = 613.00 EMERGENCY OVERFLOW ELEV.= 616.00 TOP OF BERM = 618.00 WATER QUALITY VOLUME REQUIRED = 12,543 CU FT WATER QUALITY VOLUME PROVIDED= 18,295 CU FT REVISIONS Sei THE ILLINOIS STATE TOLL HIGHWAY AUTHORITY SCALE 1''=50' SS DESCRIPTION DRAWN BY DATE 2700 OGDEN AVENUE DOWNERS GROVE, ILLINOIS 60515 CHECKED BY DW DATE 10/27/17 3041 WOODCREEK DRIVE, SUITE 211 - DOWNERS GROVE, IL 60515 (630) 641-9900

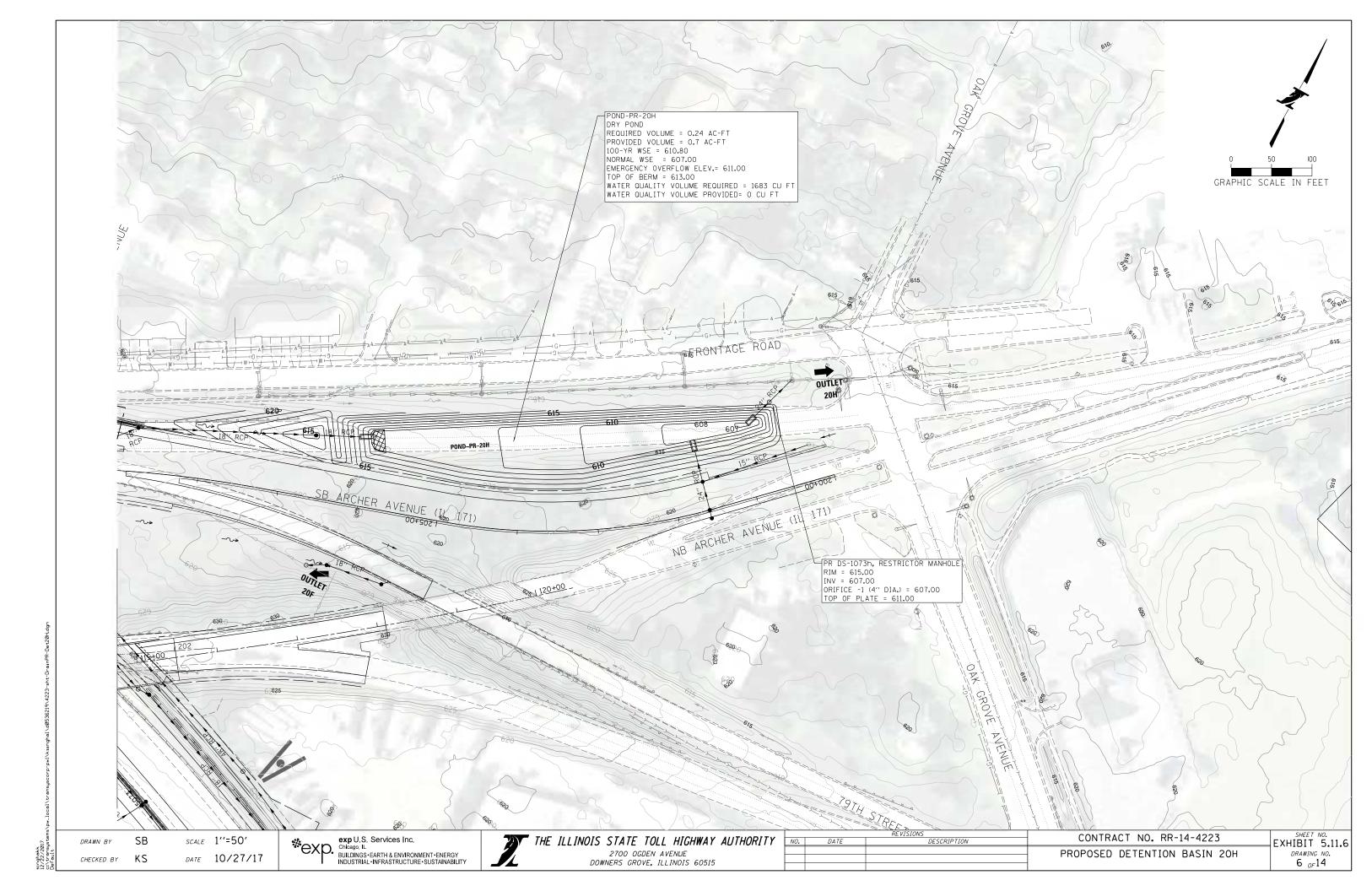


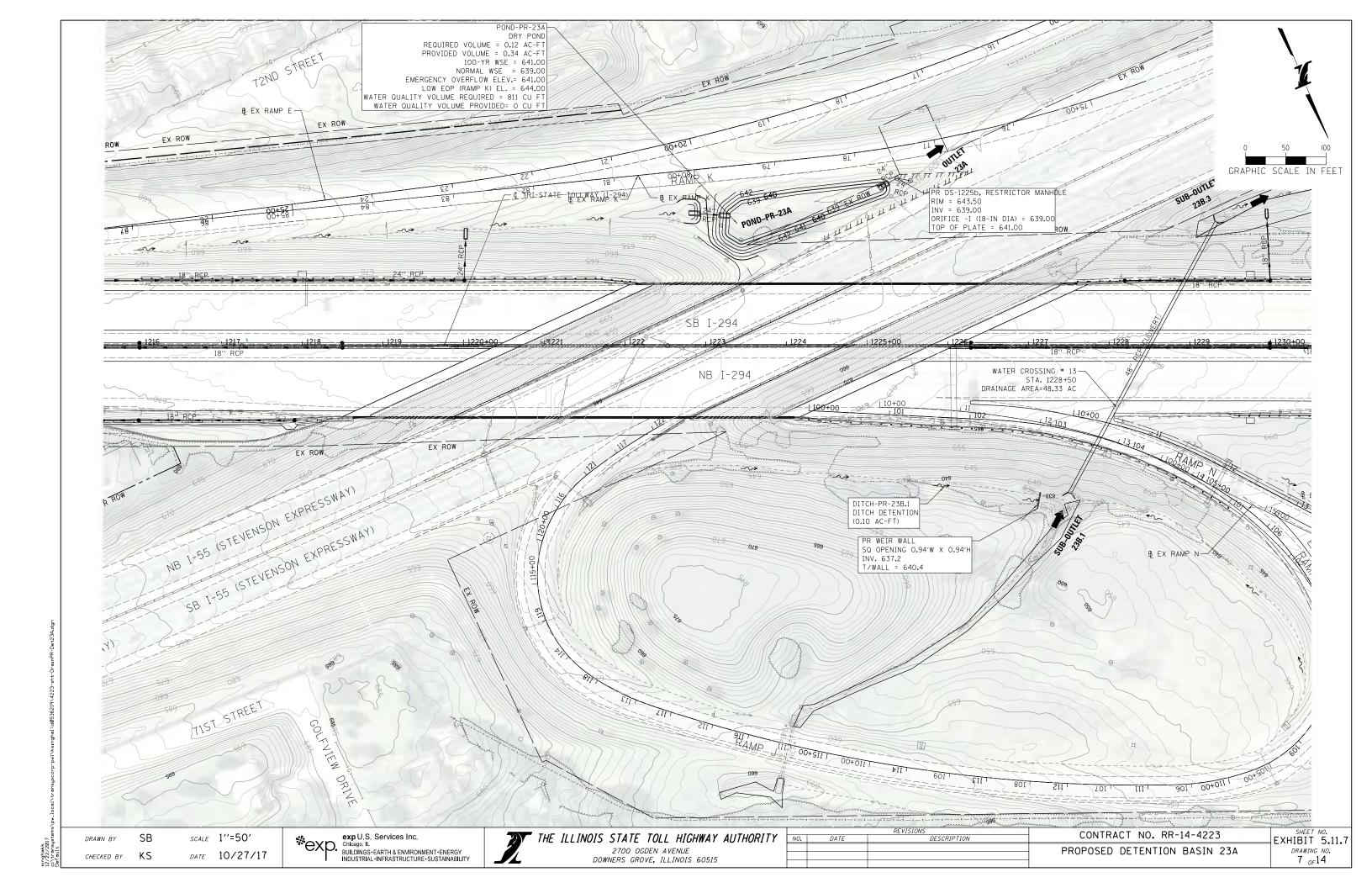


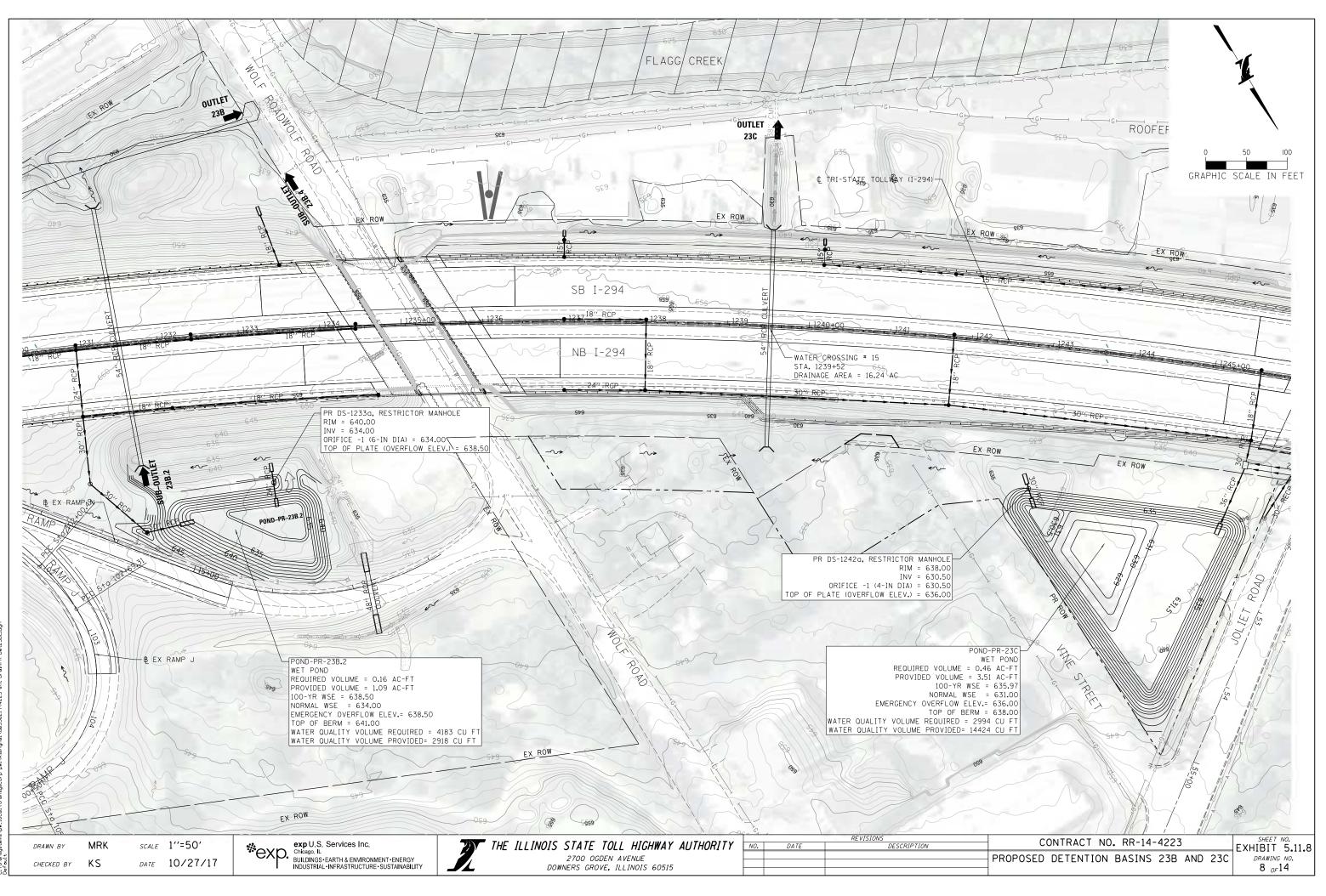


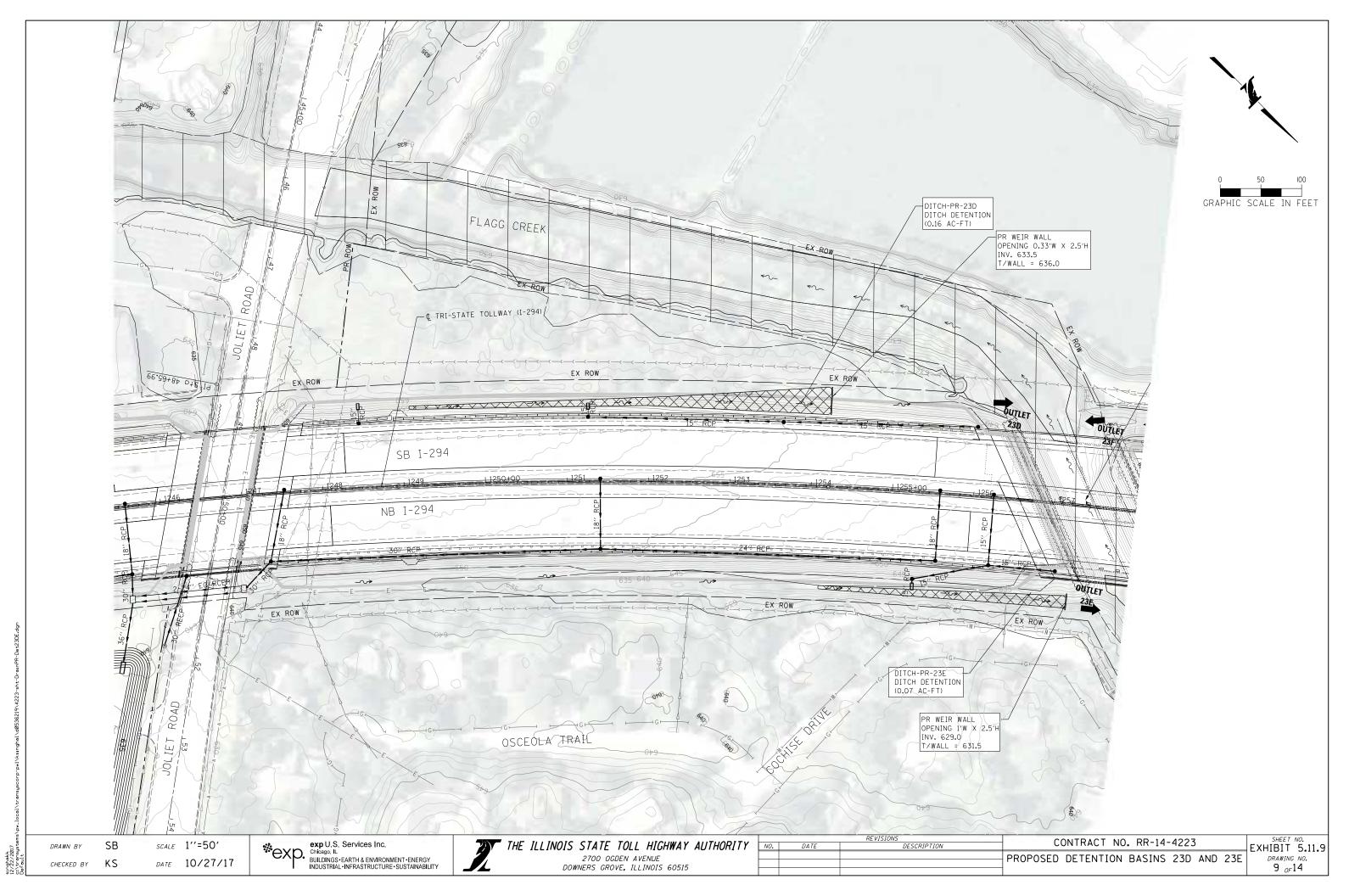


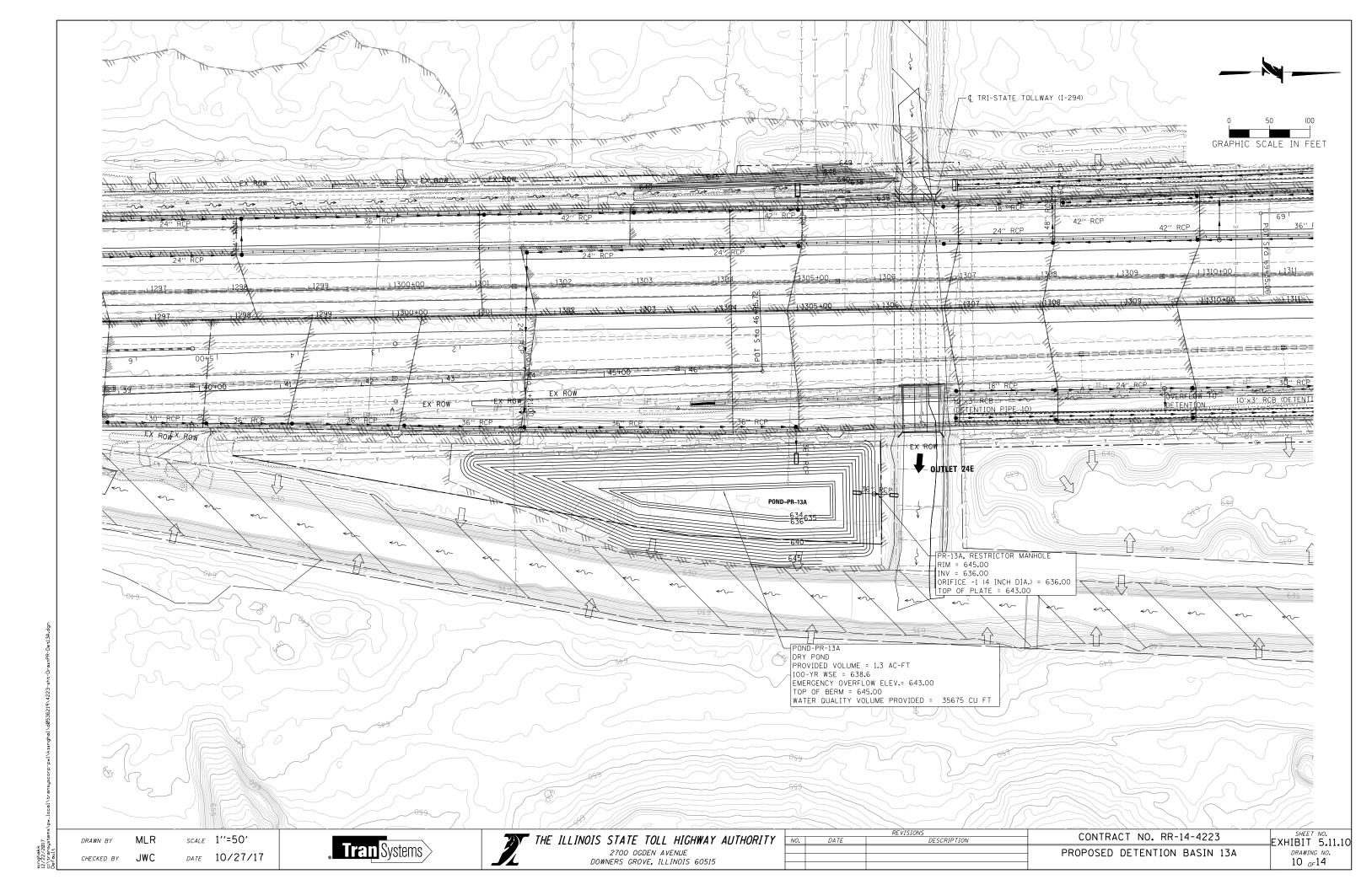


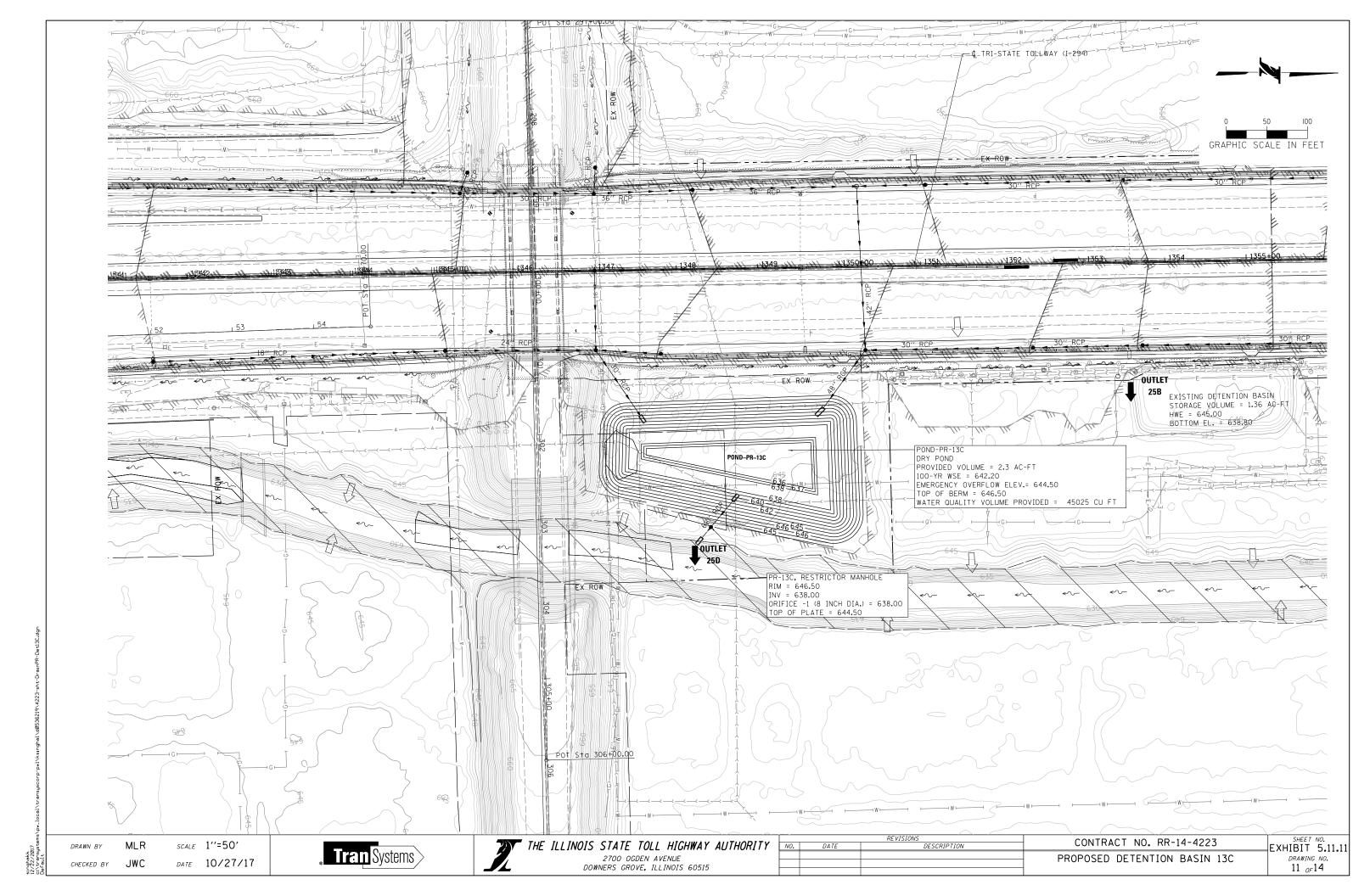


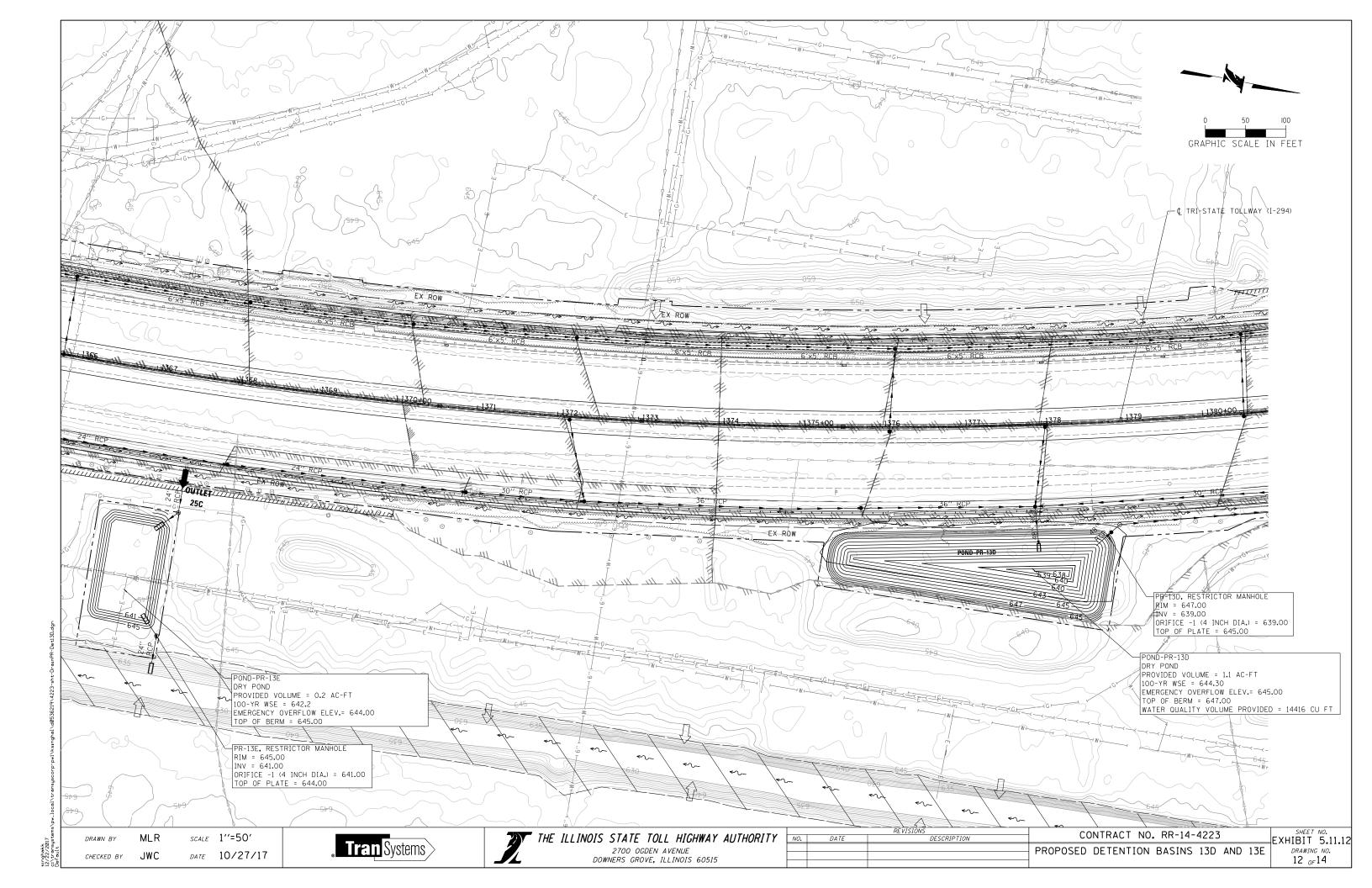


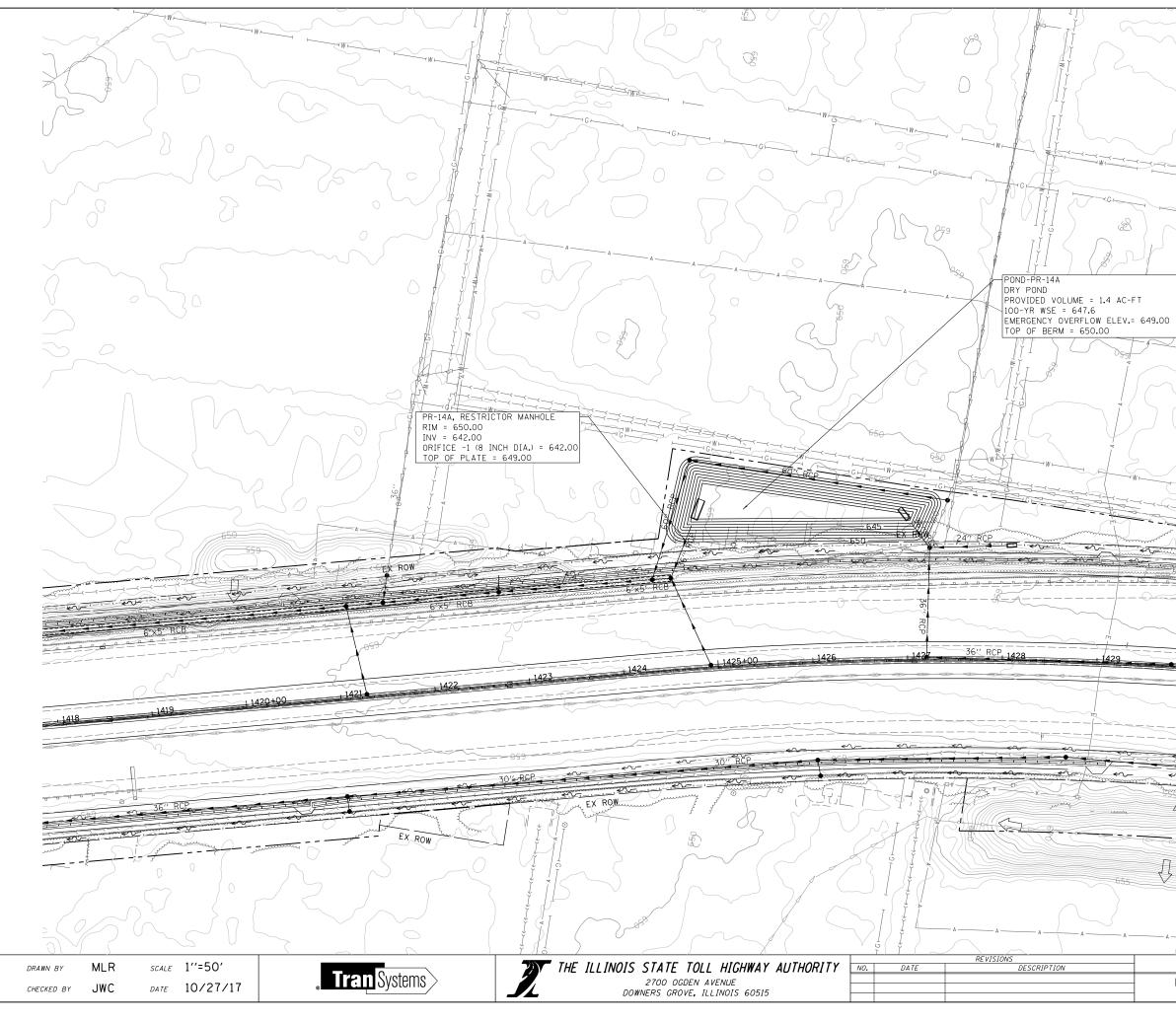




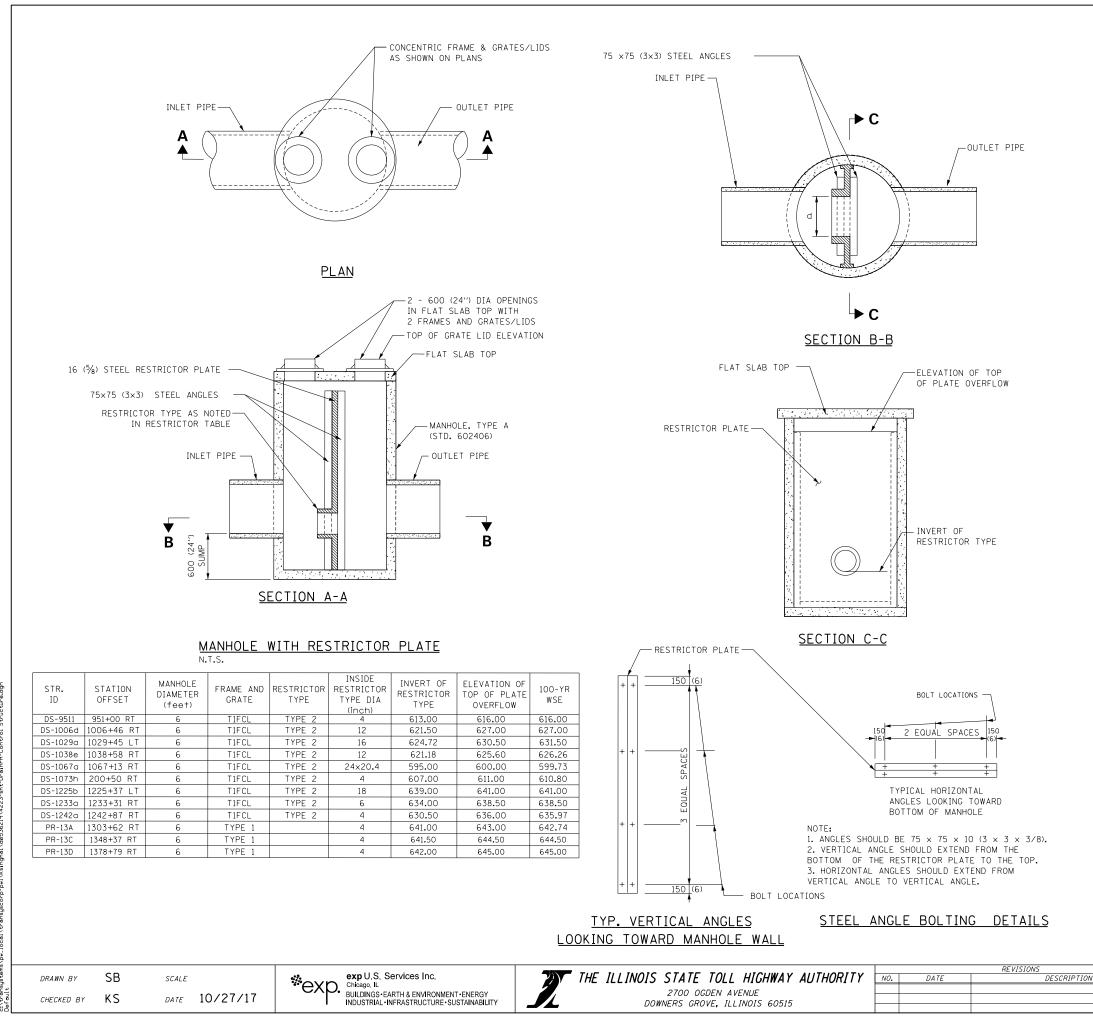


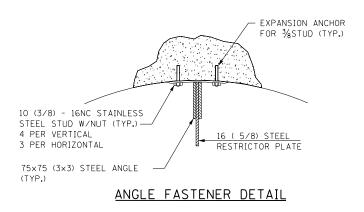






GRAPHIC SCALE IN FEET È INV= SHEET NO. EXHIBIT 5.11.13 DRAWING NO. CONTRACT NO. RR-14-4223 PROPOSED DETENTION BASIN 14A 13 _{OF}14



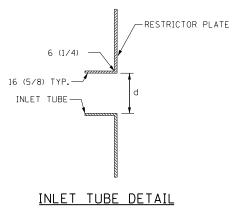


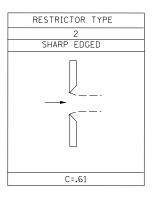
NOTES:

1. ALL STEEL ANGLES AND PLATES TO BE GALVANIZED AFTER FABRICATION.

2. ALL RESTRICTOR PLATES, ANGLES AND HARDWARE TO BE INCLUDED IN THE COST OF THE MANHOLE.

3. BASIS OF PAYMENT: "MANHOLES, TYPE A, 6'-DIAMETER, WITH 2 TYPE 1 FRAME, CLOSED LID, RESTRICTOR PLATE EACH.





ALL DIMENSIONS ARE IN MILLIMETERS (INCHES) UNLESS OTHERWISE SHOWN

CONTRACT NO. RR-14-4223	SHEET NO.	
CUNTRACT NU. RR-14-4225	EXHIBIT 5.11.14	
CONTROL STRUCTURE SCHEMATICS	DRAWING NO.	
	14 _{OF} 14	